# Adsorption Study for Chromium (VI) on Iraqi Bentonite

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# **Abstract**

The subject of this research involves studying adsorption to remove hexavalent chromium Cr(VI) from aqueous solutions.

Adsorption process on bentonite clay as adsorbent was used in the Cr(VI) concentration range (10-100) ppm at different temperatures (298, 303, 308 and 313)K, for different periods of time.

The adsorption isotherms were obtained by obeying Langmuir and Freundlich adsorption isotherm with R<sup>2</sup> (0.9921-0.9060) and (0.994-0.9998), respectively.

The thermodynamic parameters were calculated by using the adsorption process at four different temperatures the values of  $\Delta H$ ,  $\Delta G$  and  $\Delta S$  was [(+6.582 – +6.547) kJ.mol<sup>-1</sup>, (-284.560 – -343.070) kJ.mol<sup>-1</sup> and (+0.977 – +1.117) kJ.K<sup>-1</sup>.mol<sup>-1</sup>] respectively. This data indicates the spontaneous sorption process.

The kinetic study of adsorption process was studied depending on three kinetic equations:

- 1- Lagergren equation
- 2- Morris-Weber equation
- 3- Reichenberg equation

# **Keywords:**

# Introduction

Chromium can exist in several chemical forms, which have oxidation states ranging from 0-VI. However, only trivalent and hexavalent chromium are stable enough to occur in the environment[1,2].

Chromium is a naturally occurring element found in rocks, animals, plants, soil and in volcanic dust and gases[3]. Chromium (VI) in the form of CrO<sub>4</sub><sup>2-</sup> or Cr<sub>2</sub>O<sub>7</sub><sup>2-</sup> and HCrO<sub>4</sub><sup>-</sup>, is largely employed in the chemical industry for chrome plating, the manufacture of dyes and pigments, leather tanning, wood preserving, battery, rust and corrosion inhibitors, textiles, electroplating, metal processing, steel fabrication and canning industries[4-9]. Although chromium is used in many industries and is known to be essential trace, but it is found to be toxic an causing cancer at levels[10].

Toxicological studies are shown that the degree of toxicity of some elements depends on the chemical form in which the element presents, Cr(VI) is more toxicity; by contrast Cr(III) is negligible because it often forms insoluble hydroxides at neutral pH[11,12]. The USA EPA is require (0.05 and 0.1 mg/L) of Cr(VI) in drinking water and inland water, respectively[11,13].

Cr(VI) is known as carcinogens, mutagens, tetratogens in biological systems, beside that it can pose health risks such as liver damage, dermatitis, castro intestinal ulcers, diarrhea, vomiting and nausea[12,14].

The problem of removing pollutants from water are grown with rapid industrialization the discharge of toxic into water courses is a serious pollution problem.

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Adsorption is the tendency for accumulation of a substance to take place at a surface or at an interface the accummenence of adsorption is due to the atoms in any surface being subject to unbalanced forces of attraction perpendicular to the surface plane and these forces possessing a certain unsaturation[15-17].

Langmuir Isotherm is a good representation of chemisoprtion, and usually represents the low P portion of other isotherms[18].

Langmuir behavior assumes a rapid reversible adsorption, and interaction only between sorbate molecules and a surface site[19,20].

The Langmuir equation could be expressed as:

$$\left\lceil \frac{C_e}{Q} = \frac{1}{k} + \frac{a}{k} \cdot C_e \right\rceil \cdot \dots \cdot (1)$$

where Q is the amount of adsorbate (mg/g),  $C_e$  is the equilibrium concentration (mg/L), and a, k are constants related to adsorption capacity and energy of adsorption respectively or sometimes called Langmuir constants.

Freundlich Isotherm is one of the most important isotherms that deals with sorption at solid-liquid interface. Most of surface are heterogeneous, so the change in potential energy is regular, and the adsorption sites are not equivalent in energy[21,22], hence the multilayer formation is highly expected.

Freundlich equation could be written as follows[23,24]:

$$\begin{split} Q &= k_F \, C_e^{1/n} \quad ...............(2) \\ log \; Q &= log \; k_F + 1/n \; log \; C_e \quad .......(3) \end{split}$$

where Q is the adsorbate quantity (mg/g),  $C_e$  is the concentration of adsorbate at equilibrium (mg/L),  $k_F$ , and n is the sorption capacity and an empirical parameter, respectively and also called Freundlich constants.

The major objective of this work is to minimize the concentration of Cr(VI) in aqueous solutions to the acceptable levels, by removing it via and an adsorption process is used and the optimum conditions for adsorption process have been found. The detailed kinetic and thermodynamics studies have been employed to investigate the mechanism, rate and order of the adsorption process.

# **Materials and Methods**

The bentonite clay was supplied from the state company for geological survey and mining-Iraq, the bentonite had the following composition with particle size less than 75µm.

Constituent								
Wt%	56.77	15.67	4.48	3.42	0.60	1.11	5.02	12.49

The molecular formula of bentonite could be written as:

$$Mg_2Al_{10}Si_{24}O_{60}(OH)_{12}[Na,Ca]$$

The spectrophotometer method uses the selective reaction of Cr(VI) with (1,5-DPC) in basic media to yield a red-violet diphenyl carbazone complex.

The general mechanism was illustrated for oxidation of DPC with Cr(VI) was shown in the following equation[2,3].

diphenylcarbazone-chromium(III) complex

The suggested final structure of the [Chromium-1,5-diphenylcarbazone] is as follows:

$$\begin{bmatrix} C_{6}H_{5} & C_{6}H_{5} & \\ & & & \\ & & & \\ N = N & N = N \\ & & & \\ N = N & N = N \\ & & & \\ & & & \\ C_{6}H_{5} & C_{6}H_{5} & \end{bmatrix}^{3+}$$

The complex was prepared using 2.5ml (1M) NaOH in volumetric flask 250 ml,

and 50ml of 100ppm Cr(VI) was added to it, 7.5ml of DPC was added (with stirring) to the Cr(VI) solution followed by 2.5ml (50%) H<sub>3</sub>PO<sub>4</sub> and then diluted to the mark by distilled water.

A sample of 5 ppm complex solution was taken and a spectrum scan was measured using UV-Vis Spectrophotometer and showed a  $\lambda_{max}$  at 543 nm

The quantity of adsorbate was calculated by using the following formula

$$Q_e = V_{sol} (C_o - C_e) / m$$
 ......(4)

Where:

 $Q_e = Quantity of adsorbate (mg/g).$ 

 $V_{sol}$  = Total volume of adsorbate solution (L).

 $C_o$  = Initial concentration of adsorbate solutions (mg.L<sup>-1</sup>).

 $C_e$  = Concentration of adsorbate solution at equilibrium (mg.L<sup>-1</sup>).

m=Weight of adsorbant (g).

While the adsorption percentage was calculated by using the following formula.

$$%Q = \frac{(C_o - C_e)}{C_o} *100$$
 ....(5)

Where:

%Q = Adsorption percentage.

And the adsorption coefficient was calculated by using the following formula[27]:

$$K_{ads} = \frac{Q_e}{C_o} \qquad (6)$$

Where:

 $K_{ads}$  = The adsorption coefficient.

# **Results and Discussion**

Table (1) and Figure (1) shows the variation of  $C_o$ - $C_e$  with the amount of adsorbent (bentonite).

Table -1- The values of  $(C_0-C_e)$  and M (quantity of sorbent)

Co-Ce /mg.L-1	M/g
40.18	0.050
40.27	0.075
40.38	0.100
40.30	0.150
40.25	0.200
40.22	0.300

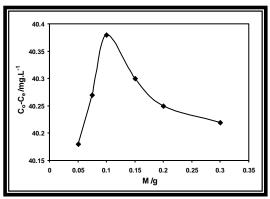


Fig. -1- The effect of clay dose on the adsorption process for 50~ppm~Cr(VI) solution on bentonite at 298K

Table (2) and Figure (2) show the variation of Q<sub>e</sub> with the contact time for 50 ppm Cr(VI) solution at 298 K to be in attachment with (0.1g) of bentonite clay.

Table -2- The values of  $Q_e$  and  $C_e$  at different time for 50 ppm Cr(VI) solution at 298K

C <sub>e</sub> /mg.L <sup>-1</sup>	Qe /mg.g-1	Time /min.
9.91	4.009	5
9.85	4.015	10
9.79	4.021	15
9.71	4.029	20
9.62	4.038	30
9.61	4.039	40
9.61	4.039	50
9.60	4.040	60

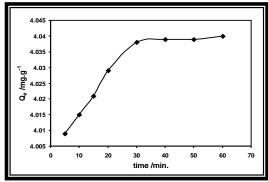


Fig. -2- The variation of  $Q_e$  with equilibrium time for 50 ppm Cr(VI) solution at 298K

The pH is an important factor that effected on the adsorption process, Table (3) and Figure (3) show the variation of %Q with different pH values for 50 ppm Cr(VI) solution at 298 K. It's clear that (pH=7) has the maxium Q% value, and this pH was chosen to all experiments of adsorption done subsequently.

Table -3- The adsorption percentage at different pH values, using bentonite at 298K for 50 ppm Cr(VI) solution

Q%	pН
79.62	3
79.85	5
80.76	7
79.54	9
79.37	11

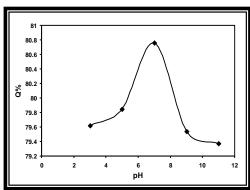


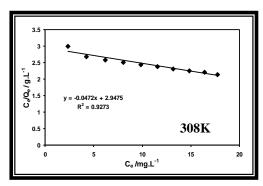
Fig. -3- The adsorption percentage vs. pH, using bentonite at 298K for 50 ppm Cr(VI) solution

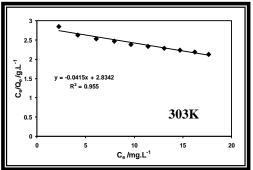
The equilibrium adsorption isotherms are of fundamental importance in the design of adsorption systems [(22]. Table (4) and Figure (4) show the Langmiur data and Linear relationship between  $C_e/Q_e$  and  $C_e$  of a series Cr(VI) solutions at (298, 303, 308 and 313)K.

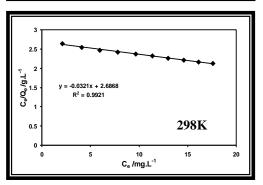
Table -4- The values of  $C_o$ ,  $C_e$  and  $C_e/Q_e$  for the adsorption of series Cr(VI) solutions at different temperatures

	298K			303K		
C <sub>o/</sub> mg.L <sup>-1</sup>	C <sub>e</sub> / mg.L <sup>-1</sup>	C <sub>e</sub> /Q <sub>e</sub> / g.L <sup>-1</sup>	C <sub>o</sub> /mg.L <sup>-1</sup>	C <sub>e</sub> / mg.L <sup>-1</sup>	C <sub>e</sub> /Q <sub>e</sub> / g.L <sup>-1</sup>	
10	2.10	2.65	10	2.22	2.85	
20	4.08	2.55	20	4.17	2.63	
30	5.95	2.47	30	6.08	2.54	
40	7.80	2.42	40	7.93	2.47	
50	9.62	2.38	50	9.65	2.39	
60	11.35	2.33	60	11.41	2.34	
70	12.96	2.27	70	13.05	2.29	
80	14.58	2.22	80	14.67	2.24	
90	16.10	2.17	90	16.22	2.19	
100	17.56	2.13	100	17.61	2.13	

	308K			313K	
C <sub>o</sub> /	C <sub>e</sub> /	C <sub>e</sub> /Q <sub>e</sub> /	Co	Ce	C <sub>e</sub> /Q <sub>e</sub> /
mg.L <sup>-1</sup>	mg.L <sup>-1</sup>	g.L <sup>-1</sup>	mg.L <sup>-1</sup>	mg.L <sup>-1</sup>	g.L <sup>-1</sup>
10	2.31	3.00	10	2.40	3.15
20	4.25	2.69	20	4.36	2.78
30	6.17	2.59	30	6.27	2.64
40	8.03	2.51	40	8.11	2.54
50	9.84	2.45	50	9.92	2.49
60	11.55	2.38	60	11.64	2.40
70	13.14	2.31	70	13.25	2.33
80	14.80	2.26	80	14.86	2.28
90	16.37	2.22	90	16.43	2.23
100	17.70	2.15	100	17.84	2.17







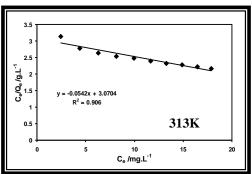


Fig. -4- The plot of  $C_e/Q_e$  against  $C_e$  for the adsorption of series Cr(VI) solutions at different temperatures

Table (5) Show the Langmuir constant at different temperatures

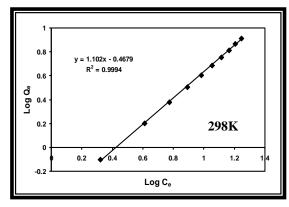
Table -5- The values of Langmuir constant at temperature range (298-313)K

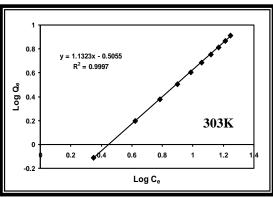
<b>T</b> ( <b>K</b> )	$K_L/L/mg$	a	$\mathbb{R}^2$
298	0.3721	0.0119	0.9921
303	0.3528	0.0146	0.9550
308	0.3392	0.0160	0.9273
313	0.3256	0.0170	0.9060

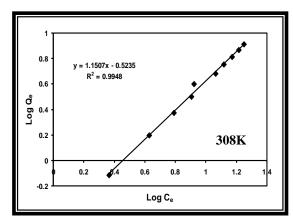
Table (6) and Figure (5) show the data and linear relationship of Freundlich isotherm between Log Q and Log  $C_{\rm e}$  for the adsorption of Cr(VI) solutions at the temperature range (298-313)K.

Table -6- The values of C<sub>e</sub>, Log C<sub>e</sub> and Log Q for the adsorption of series Cr(VI) solutions at different temperatures

different temperatures					
	298K		303K		
C <sub>o</sub> / mg.L <sup>-1</sup>	Log Ce	Log Qe	C <sub>o</sub> / mg.L <sup>-1</sup>	Log Ce	Log Q <sub>e</sub>
10	0.322	-0.102	10	0.346	-0.109
20	0.610	0.201	20	0.620	0.199
30	0.774	0.381	30	0.783	0.378
40	0.892	0.507	40	0.899	0.506
50	0.983	0.606	50	0.984	0.605
60	1.054	0.687	60	1.057	0.686
70	1.112	0.756	70	1.115	0.755
80	1.163	0.815	80	1.166	0.815
90	1.206	0.868	90	1.210	0.867
100	1.244	0.916	100	1.245	0.915
	308K		313K		
C <sub>o</sub> / mg.L <sup>-1</sup>	Log C <sub>e</sub>	Log Qe	C <sub>o</sub> / mg.L <sup>-1</sup>	Log C <sub>e</sub>	Log Q <sub>e</sub>
10	0.363	-0.114	10	0.380	-0.119
20	0.628	0.197	20	0.639	0.194
30	0.790	0.377	30	0.797	0.375
40	0.904	0.504	40	0.909	0.503
50	0.922	0.603	50	0.996	0.602
60	1.062	0.685	60	1.065	0.684
70	1.118	0.754	70	1.122	0.753
80	1.170	0.814	80	1.172	0.813
90	1.214	0.867	90	1.215	0.866
100	1.247	0.915	100	1.251	0.914







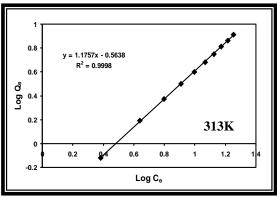


Fig. -5- Freundlich linear relationship between Log  $Q_e$  vs. Log  $C_e$  for a series Cr(VI) solutions at different temperature

Table (7) Show the Freundlich constants at different temperatures

Table -7- The values of Freundlich constants at different temperatures

T (K)	Log k <sub>f</sub>	$\frac{k_{\rm f}/}{mg/g/(mg/L)^{\rm n}}$	1/n	n	$\mathbb{R}^2$
298	- 0.4679	0.3404	1.1020	0.9074	0.9994
303	- 0.5055	0.3122	1.1323	0.8831	0.9997
308	0.5331	0.2930	1.1523	0.8678	0.9997
313	- 0.5638	0.2730	1.1757	0.8505	0.9998

Table (8) and Figure (6) show that the adsorption percentage of Cr(VI) decrease as temperature increase, where as the adsorption process is an exothermic process, so absorption was involved with adsorption and all processes and all processes increase with temperature increase.

Table -8- The adsorption percentage and  $Q_e$  values at different temperature

T/K	Q <sub>e</sub> / mg.g <sup>-1</sup>	Q%		
298	4.038	80.76		
303	4.035	80.70		
308	4.016	80.30		
313	4.008	80.16		

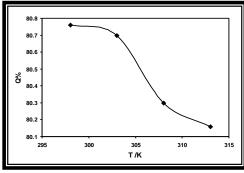


Fig. -6- The effect of temperature on the adsorption percentage

The thermodynamic functions,  $\Delta H$ ,  $\Delta G$  and  $\Delta S$  were calculated using the following formulas [28,29].

b = a · exp(-
$$\Delta$$
H/RT) ......(7)  
ln b = ln a - ( $\Delta$ H/R) · 1/T ......(8)  
ln a =  $\Delta$ S/R .....(9)  
 $\Delta$ G =  $\Delta$ H - T $\Delta$ S......(10)

Where b is the maximum adsorption quantity for series Cr(VI) solutions at different temperature and could be obtained from the plot of C<sub>e</sub>/Q<sub>e</sub> vs. C<sub>e</sub> (Fig.(4)).

The equation (8) was used to calculate the  $\Delta H$ , by plotting ln b vs. 1/T. Table (9) and Figure (7) showed a linear relationship and the slope represents -  $\Delta H/R$ , where R is the gas constant (8.314J.mol<sup>-1</sup>.K<sup>-1</sup>) , and  $\Delta H_{ads}$  were calculated.

Table -9- The values of the reciprocal of temperature and ln b

T(K)	1/T * 10 <sup>-3</sup>	b	ln b
298	3.35	2.68	0.98
303	3.30	2.83	1.04
308	3.24	2.94	1.08
313	3.19	3.07	1.12

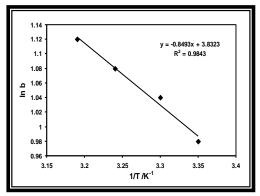


Fig. -7- The plot of ln b vs. the reciprocal of temperature

Table -10- Show the thermodynamic functions of the adsorption process

or the a	of the ausorption process				
T(K)	ΔH*10 <sup>-3</sup> (kJ.mol <sup>-1</sup> )	ΔG (kJ.mol <sup>-1</sup> )	ΔS*10 <sup>-3</sup> (J.mol <sup>-1</sup> .K <sup>-1</sup> )		
298		- 284.560	+ 977		
303	6.55225	- 307.680	+ 1037		
308		- 325.167	+ 1077		
313		- 343.070	+ 1117		

From the Table (10), It's clear that  $\Delta H$  has the positive values, which indicate the ideal and the maximum value of a physic-sorption process. All values of  $\Delta G$  were negative so the adsorption of Cr(VI) on the bentonite was considered a spontaneous process, also  $\Delta S$  was had the positive values, and it was increased with the temperature increase, the disorder of

the system increase, i.e. the system becomes more disordered, which due to the absorption process and diffusion of Cr(VI) ions in the bentonite pores.

The kinetic of the adsorption process was studied via introducing three models, also the rate constant was calculated.

# 1- Lagergren Model

The rate constant  $k_{ads}$  was determined from the following pseudo- $1^{st}$ -order rate expression, which could be expressed as follows[30]:

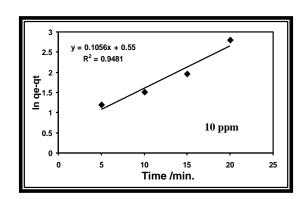
$$\ln q_e - q_t = \ln q_e - k_{ads} t \dots (11)$$

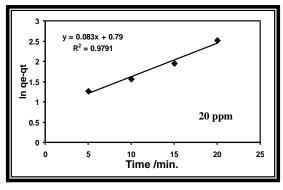
where  $q_t$  and  $q_e$  are the amount of Cr(VI) adsorbed at time t /min., and at equilibrium time respectively,  $k_{ads}$  /min.<sup>-1</sup> is the rate constant and values are given in Table (11) at 298K.

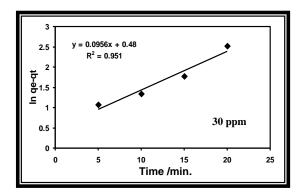
The linear relationship was obtained via plotting ln  $q_e$ - $q_t$  vs. t /min., as shown in Figure (8).

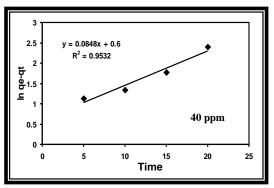
Table -11- The rate constants of adsorption process for a series Cr(VI) solutions at 298K

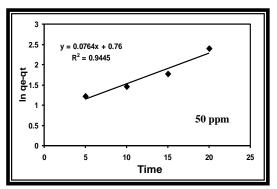
C <sub>0</sub> (mg.L <sup>-1</sup> )	k <sub>ad</sub> (min1)	$C_0$ (mg.L <sup>-1</sup> )	k <sub>ad</sub> (min1)
10	0.1056	60	0.0890
20	0.0830	70	0.0934
30	0.0956	80	0.1198
40	0.0848	90	0.0756
50	0.0784	100	0.1192

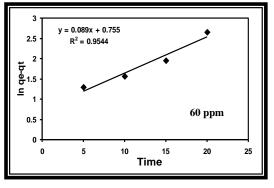


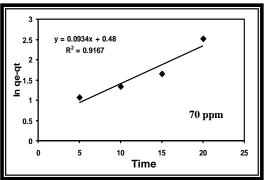


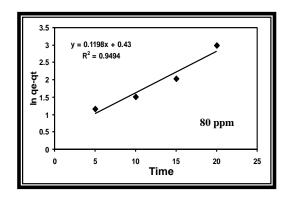


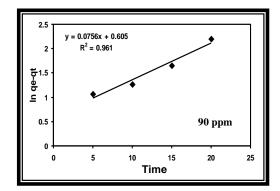












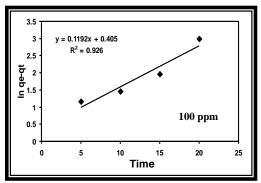


Fig. -8- The Lagergren model for a series Cr(VI) solutions at 298K

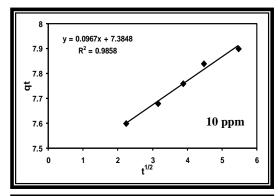
#### 2- Morris-Weber Model

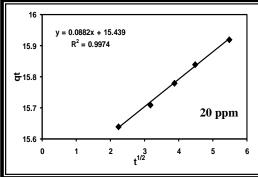
12)

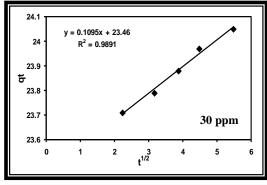
This kinetic model was used to estimate the rate limiting step of any adsorption process, the equation of this model could be expressed as follows<sup>(31,32)</sup>.

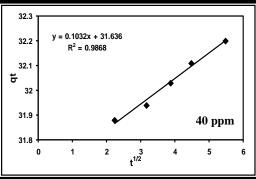
$$q_t = k_d \sqrt{t}$$
 (

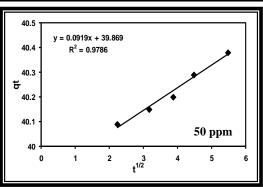
Where  $q_t$  is the quantity of adsorbed material at any time /mg.g<sup>-1</sup>,  $k_d$  is the diffusion constant, and t is the time of diffusion /min., the plotting of  $q_t$  vs.  $\sqrt{t}$  was accomplished at 298K. Figure (9) shows the plot of  $q_t$  vs.  $\sqrt{t}$  for different Cr(VI) concentrations at 298K.

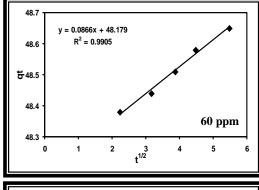


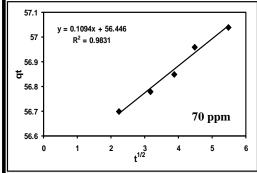


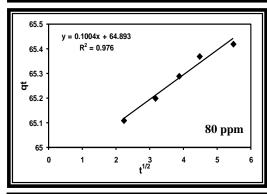


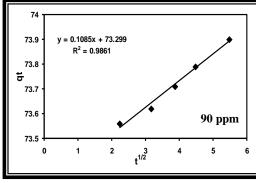












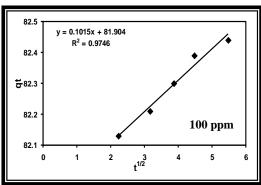


Fig. -9- The plot of  $q_t$  vs.  $\sqrt{t}$  for a series Cr(VI) solutions at 298K

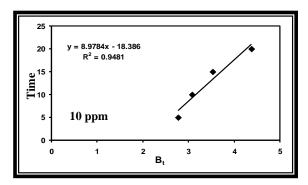
# 3- Reichenberg Model

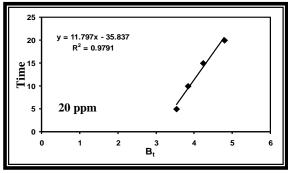
This kinetic model was proposed to discuss the behavior of many adsorption process in solution and Reichenberg had introduced following formula<sup>(33)</sup>:

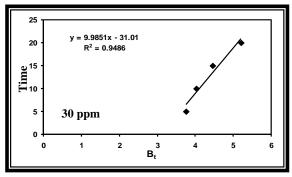
$$\begin{split} F &= [1\text{-}6/\pi^2] \; e^{\text{-Bt}} \; \dots \dots (13) \\ B_t &= \text{-}0.4977 \; \text{-} \; \ln \; (1\text{-}F) \; \dots \dots (14) \\ F &= q_t \; / \; q_e \; \dots \dots \dots (15) \end{split}$$

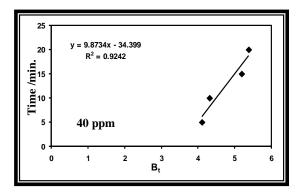
Plotting of time (min.) vs.  $B_t$  revealed a linear relationship with relatively acceptable  $R^2$  values. Figure (10) shows the variation of  $B_t$  with time for different concentration of Cr(VI) at 298K.

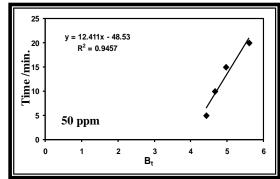
According to this model, it characterized the rate determining mechanisms which was diffusion process for Cr(VI) ions from the bulk solution to the absorbent surface and absorption occurred.

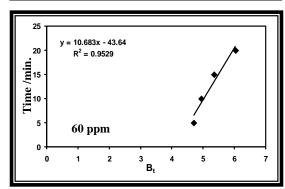


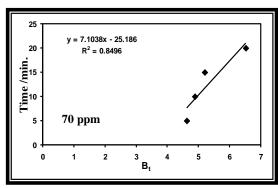


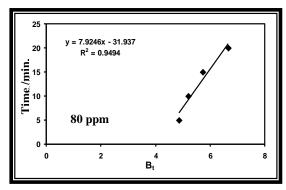


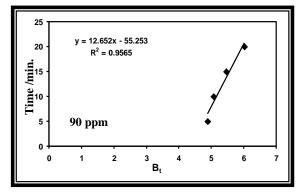












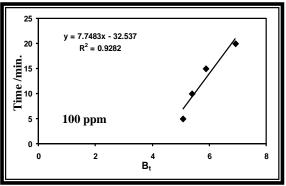


Fig. -10- The variation of Bt with time for a series of Cr(VI) solutions at 298K

# **Conclusion**

The adsorption of Cr(VI) on bentonite was of Langmuir type at Cr(VI) concentration range (10-1000) ppm. Langmuir type indicates to the monolayer formation of Cr(VI) on the bentonite surface. The isotherms of Cr(VI) was followed both Langmuir and Ferundlich models.

The adsorption of Cr(VI) on bentonite reched to the largest value (83.54) at pH = 7.

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# دراسة امتزاز الكروم السداسي على طين البنتونايت العراقي خلوب عبد صالح السعدى\*

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#### الخلاصة

يتضمن موضوع البحث دراسة امتزاز الكروم السداسي لازالته من المحاليل المائية. عملية الامتزاز على طين البنتونايت (كمادة مازة) لازلة تراكيز مختلفة من الكروم السداسي تراوحت بين (10-1000) ملغم/لتر بمدى من درجات الحرارة (298-313) كلفن وعند الازمان المختلفة.

تم الحصُول على أيزوثرمات الامتزاز بتطبيق معادلتي لنكماير وفرندلش بنسبة خطية - $(R^2=0.9921-1.09921-1.$ 

تم حُساب القيم الثرموديناميكية باربع درجات حرارية وكانت قيم الانثالبي محصورة بين (6.547 – 6.582) كيلوجول مول وقيم الانتروبي الخاقة الحرة لكبس بين (284.56 – 343.07 – كيلوجول مول وقيم الانتروبي بين (977 – 1117) جول مول  $^{-1}$  بين (977 – 1117) جول مول ول مول ولي منافقة الخاتية عملية الامتزاز.

تمت دراسة حركيات الامتزاز اعتماداً على ثلاث معادلات حركية هي 1- معادلة لنكماير 2- معادلة موريس-ويبر 3- معادلة ريجمبرغ.