Comparative Differential Thermal Analysis of Epoxy Resin blends with Amic Acid-Copper Complexes

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Abstract:

This work deals with the thermal behaviour of epoxy resin blended with eleven mono-and dibasic maleamic acids and their copper complexes. DTA thermograms of all blands show two distinct exotherms (T_2 and T_4) at high temperatures if compared with those of epoxy alone. Values of T_1 and T_4 in copper containing blends are

Key words: Epoxy resin; Maleamic acid complexes.

Introduction:

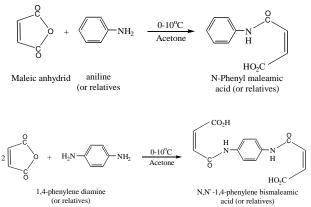
The use of metal salts in the production and formulation of epoxy resins for use in composite materials has been widely studied. A large body of work involving the use of metal complexes to enhance (e.g. electrical, thermal and chemical, etc.) epoxy properties were described [1]. Many types of ligands were used as a complexing agents with the metals. Ligands like acetylacetone [2,3], acrylates [4], imadizole [5], phthalocyanine [6] and Schiffs bases [7] are widely used in this field. Recently, thermal stability of epoxy resin blended with polyureametal complexes were discussed [8]. The present work deals with the preparation and investigation of epoxy blends with maleamic acids and their copper complexes. This metal was choosed as a complexing agent due to the high stability of its complexes with amic acid if compared with other metals [9].

Experimental: Chemicals:

Aniline, 2-chloroaniline, 3-chloroaniline, 2,6dichloroaniline, 2-bromoaniline, *o*-hydroxy aniline, *p*nitroaniline, *o*-toluidene, 1,2-phenylene diamine, 1,4phenylene diamine, 2,5-tolylene diamine, malic anhydride (BDH), copper acetate (Fluka). All chemicals were reagent grade. Common organic solvents commercially available were used without further purification.

Preparation of precursors:

Monobasic maleamic acids are prepared by the reaction of 1mole of aniline (or its relatives) with 1mole of maleic anhydride. While dibasic maleamic acids are synthesized by the reaction of 1 mole of diamine with 2moles of maleic anhydride [10]. higher than their isomers in mono amic acids, while the inverse was observed in copper-diamic acid blends. The presence of copper in the blend shifts the position of the oxidation exotherm (T_4) to relatively higher temperatures.



Copper complexes of amic acids are sunthesized by the reaction of the ligand (amic acid) with hydrated copper acetate $(CH_3CO_2)_2$.Cu.H₂O in methanol. The complex is treated and isolated as mentioned elsewhere [9].

Preparation of epoxy blends:

Epoxy blends with amic acids and their copper complexes are prepared by mixing liquid epoxy (Lyco-Pox 103, Lycochem. Ger.) with the second component (1:1 by weight). After homogenization, epoxy hardener was added. The mixture is left for 72 hrs to complete crosslinking.

Instrumentation:

Differential thermal analysis (DTA) thermograms were recorded using a home-made apparatus designed according to reference [11] and calibrated by standard PVC sample. IR spectra were recorded on Pye-Unicam SP-2000 spectrometer with KBr pellets.

Results and Discussion:

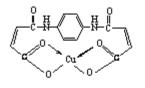
Table 1 shows the melting points and the important IR spectral bands of amic acids (ligands) and their copper complexes. Amic acids show characteristic bands around $3321-3250 \text{ cm}^{-1}$ (acidic –OH) and $1610-1640 \text{ cm}^{-1}$ (olifinic group) and $1710-1720 \text{ cm}^{-1}$ (carbonyl group).

| Maleamic acid | m.p. (°C) | -ОН | -NH | -COO | C=C olefinic | aromatic |
|------------------|-----------|------|------|--------------|-----------------|----------|
| PMA(*) | 198 | 3314 | 3325 | 1705 | 1610 | 1432 |
| 2CMA | 123 | 3321 | 3278 | 1713 | 1610 | 1439 |
| 3CMA | 195 | 3316 | 3270 | 1708 | 1615 | 1420 |
| 2,6DCMA | 157 | 3250 | 3260 | 1710 | 1623 | 1414 |
| 2BMA | 112 | 3305 | 3268 | 1715 | 1626 | 1475 |
| 4NMA | 216 | 3300 | 3265 | 1716 | 1618 | 1428 |
| 2HMA | 185 | 3318 | 3260 | 1717 | 1621 | 1421 |
| 2MMA | 216 | 3311 | 3267 | 1714 | 1620 | 1430 |
| 1,2PBMA | 193 | 3277 | 3271 | 1718 | 1636 | 1452 |
| 1,4PBMA | 227 | 3280 | 3205 | 1718 | 1635 | 1450 |
| 2,5TBMA | 203 | 3287 | 3210 | 1720 | 1637 | 1451 |
| Copper complexes | m.p. (°C) | -NH | -COO | C=O amide | C=C | aromatic |
| PMCu(*) | 155 | 3225 | 1690 | 1440 | 1624 | 1450 |
| 2CMCu | 175 | 3235 | 1629 | 1436 | 1640 | 1456 |
| 3CMCu | 173 | 3230 | 1685 | 1400 | 1644 | 1468 |
| 2,6DCMCu | 188 | 3140 | 1671 | 1422 | 1644 | 1465 |
| 2BMCu | 178 | 3150 | 1650 | 1425 | 1643 | 1480 |
| 4NMCu | 243 | 3197 | 1666 | 1369 | 1647 | 1479 |
| 2HMCu | 370 | 3200 | 1657 | 1375 | 1629 | 1479 |
| 2MMCu | 234 | 3190 | 1685 | 1442 | 1648 | 1480 |
| 1,2PBMCu | 302 | 3215 | 1680 | 1490 | 1650 | 1470 |
| 1,4PBMCu | 325 | 3210 | 1642 | 1450 | 1640 | 1476 |
| 2,5TBMCu | 272 | 3220 | 1675 | 1488 | 1645 | 1487 |

Table 1: Important IR absorptions (cm⁻¹) and melting points of amic acid and their copper complexes.

(*) Abbreviations: PMA=N-phenyl maleamic acid, PMCu= Cu complex of PMA, and so for the other compounds.

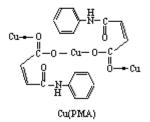
Complexation of amic acids with copper through the carbonyl groups makes the –OH absorption to disappear and shifts the other absorption bands to a near positions. Previous work shows that bisamic acids behave as tetradentate ligands leading to square planer complexes, while monobasic acids behave as a bidentate ligands [9] as shown below:



Cu \mathbf{Cr}

Cu(1,4-FBMA)

OJ(1,2-PBMA)



Curing behaviour of epoxy resins:

Figure 1 shows a representative DTA thermogram of epoxy resin alone (a), epoxy-PMA (b) and epoxy-PMCu (c) blends. Analysis of these thermograms reveals that polymers in general transverse through different thermal phases [12]. T1, T2, from the figure, represent the first energy release and the maximum degree of orientation or cyclodehydration. The termination of arrangement or crosslinking are represented by T3. T4 is the temperature of phase changes like oxidation, degradation etc. which appeared at high temperatures [12, 13]. These representative temperatures for epoxy and its blends with eleven amic acids and their copper complexes are obtained from similar DTA thermograms and listed in tables 2 and 3.

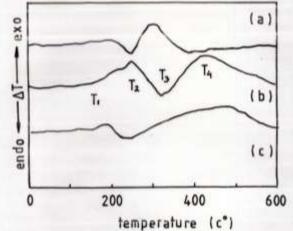




 Table 2: Representative DTA temperatures for Epoxy-Amic acid blends

| Blend | $T_1(^{\circ}C)$ | T ₂ (exo) | T ₁ | T ₄ (exo) |
|-----------|------------------|-----------------------------|-----------------------|-----------------------------|
| Epoxy (E) | 120 | 220 | 250 | 310 |
| E-PMA | 115 | 260 | 320 | 450 |
| E-2CMA | 140 | 300 | 325 | 450 |
| E-3CMA | 120 | 190 | 330 | 450 |
| E-2,6DCMA | 120 | 350 | 375 | 450 |
| E-2BMA | 120 | 180 | 330 | 420 |
| E-4NMA | 105 | 180 | 250 | 420 |
| E-2HMA | 100 | 125 | 300 | 430 |
| E-2MMA | 100 | 150 | 200 | 450 |
| E-1,2PBMA | 110 | 200 | 270 | 475 |
| E-1,4PBMA | 110 | 180 | 350 | 510 |
| E-2,5TBMA | 100 | 130 | 315 | 440 |

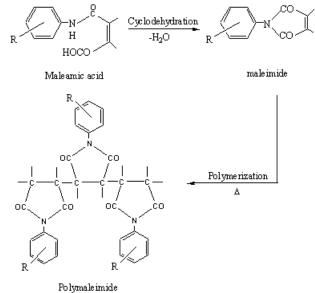
 Table 3: Representative DTA temperatures for Epoxy-Copper/Amic acid complex blends

| Blend | $T_1(^{\circ}C)$ | T ₂ (exo) | T ₃ | T ₄ (exo) |
|------------|------------------|-----------------------------|----------------|-----------------------------|
| E-PMCu | 135 | 180 | 260 | 480 |
| E-2CMCu | 170 | 310 | 320 | 480 |
| E-3CMCu | 140 | 250 | 320 | 450 |
| E-2,6DCMCu | 130 | 230 | 360 | 460 |
| E-2BMCu | 130 | 150 | 250 | 420 |
| E-4NMCu | 110 | 170 | 380 | 420 |
| E-2HMCu | 130 | 160 | 390 | 490 |
| E-2MMCu | 110 | 140 | 200 | 490 |
| E-1,2PBMCu | 110 | 150 | 245 | 400 |
| E-1,4PBMCu | 110 | 155 | 270 | 420 |
| E-2,5TBMCu | 115 | 150 | 300 | 400 |

DTA of Epoxy- Maleamic acid blends:

Analysis of DTA thermogram of epoxy resin alone (fig 1a) reveals 2 exotherms at 220 and 310°C. the first belongs to partial orientation of molecules, the second to polymer oxidation [12]. The comparison of Epoxy-amic acid values with that of epoxy alone (Table 2) reveals the following conclusions:

1. Expansion of the distance between T_1 and T_3 which appeared as a wide band as shown in PMA, 2MMA, 2CMA, 3CMA and 2BMA belnds. The reason may be due to the interference of three effects (cyclodegydration of amic acids, polymerization through the olinific bond and orientation of the formed molecules:



2. The lower values of oxidation peak (T_4) noticed in the blends containing Br, NO₂ and OH. On the contrary, the maximum values of T_4 is observed in

bisamic acid-epoxy blends as follows: 1,4PBMA > 1,2PBMA > PMA ~ 2MMA ~ 2CMA ~ 3CMA > 2,5TBMA > 2,6DCMA > 2HMA > 4MMA ~ 2BMA

DTA of Epoxy-Cu/amic acid blends

The comparison of DTA values of copper containing blends (Table 3) with their isomers without copper (Table 2) shows the following notes:

- 1. Advancing of T_1 to higher values in the blends containing monobasic acids while those containing dibasic acids are not affected.
- 2. T_2 and T_3 show small intensities and shifted, in general, to lower values.
- 3. Creep of T₄ to higher values for most monoacid copper blends and to lower positions for diacid once as shown:
- 2MMCu ~ 2HMCu > PMCu ~ 2,6DCMCu > 3CMCu ~ 2BMCu ~ 4NMCu ~ 1,4PBMCu > 1,2PBMCu ~ 2,5TBMCu

To investigate the prementioned results, we have to note that all blends composed of two polymers. The first is the fixed epoxy resin while the second is a changeable polymer (11 maleamic acids and their copper complexes). Such blends are synthesised by interpentrating of the second component through the epoxy network. The new structure changes the thermal properties of epoxy resin and causes its (T) values to change their positions. The exotherm (T₄) has a special importance because it represents the beginning of oxidation and degradation of the resin. Higher values of T₄ reflect high thermal stability of this polymer. The minimum T₄ values are observed in the blends containing Br and NO₂. Such result may be related to electronwithdrawing nature of these substituents. On the contrary, the presence of OH and Me substituents

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enhances T_4 to high values. As well as, the presence of metal (Cu) in the blend show the same effect especially when complexed with monobasic acids. While lower T_4 values observed in bisamic acid/Cu complexes may be due to the bulky complex which causes a depression in network density. The decrease in polymer density lower its packing and affects its thermal and mechanical properties negatively [14].

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التحليل الحراري التفاضلي المقارن لسبائك راتنج الايبوكسي مع حوامض الاميك ومعقداتها النحاسية

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الملخص:

 $T_1 \ e$ $T_4 \ e$ $T_4 \ e$ $T_1 \ e$ T_1

يشتمل البحث على دراسة حرارية تغاضلية مقارنة لمجموعة من سبائك راتتج الايبوكسي مع أحد عشر نوعاً من حوامض الاميك الأحادية والثنائية المجموعة الكاربوكسيلية وكذلك مع معقداتها مع النحاس. أشارت الدراسة أن معظم السبائك أعطت انبعاثين حراريين كبيرين T₂ و T₄ في درجات حرارية أعلى مما هي في حالة راتنج الايبوكسي منفرداً. كما لوحظ أن قيم