

STUDYING PROPERTIES OF AL-12WT%SI ALLOY REINFORCED WITH CeO₂ NANO POWDERS PREPARED BY POWDER METALLURGY

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ABSTRACT:

In this paper, Aluminum – 12wt% Silicon alloys reinforced by cerium oxide (CeO₂) nano powder with a different percentage (1, 2, and 3 wt.%) were prepared by powder technology method. Wear, porosity, apparent density tests were conducted for composite materials and reference alloy. The results showed that there is a slight change in the density and increases in the porosity of nanocomposite materials compared to reference alloy. The wear rate decreases with the increase in the proportion of the reinforced particles for the reference alloy as well as the wear rate increases with increased applied load.

KEYWORDS : Al-Si Alloy, Cerium Oxide, Powder Technology, Wear test.

 CeO_2 دراسة خواص سبيكة Al-12%Si المقواة بمسحوق نانوي من والمحضرة بطريقة ميتالورجيا المساحيق

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الخلاصة

في هذا البحث تم تحضير مواد متراكبة ذات اساس من سبيكة المنيوم – 12% سليكون ومقواة بمسحوق نانوي من مادة سير اميكية اوكسيد السيريوم (CeO₂) بنسب مختلفة (1، 2، 3%) بطريقة تكنولوجيا المساحيق. تم اجراء اختبارات البلى، المسامية وكذلك الكثافة الظاهرية على المواد المتراكبة والسبيكة الاساس. اظهرت النتائج ان هنالك تغيير طفيف في الكثافة وزيادة في المسامية لمواد المتراكبة النانوية مقارنة بالسبيكة غير المقواة . اما معدل البلى فيقل مع زيادة نسبة الدقائق المقارة بالنسبة المتراكبة النانوية مقارنة بالسبيكة غير المقواة . اما معدل البلى فيقل مع زيادة نسبة الدقائق المقواة بالنسبة الى

INTRODUCTION:

Metal Matrix Composites are being increasingly used in aerospace and automobile industries owing to their enhanced properties such as tensile strength, elastic modulus, hardness at room and elevated temperatures and wear resistance (Veeresh2011 and Dwivedi2011). Composite materials based on light metals like Aluminium, Magnesium and Zinc find applications in many industries due to their low density (Shabani2012, Srivastava2011 and Cavaliere2006). Different reinforcing materials like SiC, TiB₂, Al₂O₃, B₄C, zircon sand, SiCrFe and CrFeC, and cerium oxide have been used to reinforce the metal-based matrices in an attempt to improve their mechanical and wear properties (Poddar2009 and Hamid2008). Aluminium alloy-based particulate-reinforced composites with adequate strength and wear resistance have a large potential for a number of engineering applications (Madhu2012 and Son2003). Powder metallurgy is an important processing technique for MMCs, which can eliminate the segregation of the reinforcement that is typical of the ingot metallurgy process (Smagorinski1998 and O'donell2001). Wear is the progressive loss of material due to relative motion between a surface and the contacting substance or substances (Peter1997). The wear damage may be in the form of micro-cracks or localized plastic deformation (Sanchez2006) .

Many studies were concentrated on improvement of Al-Si alloy properties (Haitham2010), studied the mechanical properties of modifier Al-12% Si with different wt% Sb, reinforced by ceramic particles (Y_2O_3) with different wt% using vortex technique. He showed that the addition of Antimony leads to the microstructure refinement and change the silicon shape in the alloy from the flake – like or lamellar – like to fibrous – like In addition to the increasing the hardness when Sb is up to 0.3%, after that the hardness will decrease, as well as the addition of ceramic particles increase the hardness and decrease the wear rate. While (Prabhu2010) studied the effect of heat treatment on strength and abrasive wear behavior of Al 6061/SiC composite. He showed that with using composites better micro hardness, tensile strength and good wear resistance were obtained compared with Al matrix alloy. (Lee1992) Characterized wear behavior of aluminum matrix composites by the dry spindle wear test under various conditions (volume fractions of reinforcements, sliding distances and speeds). They found that wear resistance of composites was improved due to the presence of reinforcements, but with no noticeable improvements observed in the wear resistance with more than 20% addition of reinforcements.

The present work focused on evaluating and prediction the effects of the addition of various amounts of cerium oxide nano powder on wear properties of Al-Si alloy. Density and porosity are also determined in this work.

EXPERIMENTAL WORK:

Powders Preparation

The materials used for preparation the metal matrix nanocomposites (MMNCs) are Aluminum with average particle size 50 μ m and purity 99.99%, Silicon with average particle size 75 μ m and purity 99.98% (supplied by METCO Co. Ltd), and 75-125nm of CeO₂ (supplied by MTI Co. Ltd) depended on using sieving vibration to determine the practical size of powders. The powders were mixed with a percent (Al-12wt%Si) as shown in Fig. (1). Nano powder (CeO₂) has been added as listed in Table (1). Electric rolling mixer (ball mill) with velocity rotation 750 rpm and 15 mm diameter of alumina balls was used for mixing these powders together in order to obtain good particles distribution for 30 min (dry mixing), the percent weight of alumina ball to powders was 1:20. After that, they used manual mixing for 15min at room temperature to ensure the quality and volume homogenous of powders mixing.

Compact Powders

After mixing process, the powders were compacted in a cylindrical die made from tool steel (diameter =1 cm and height = 6 cm), by using a manual hydraulic press. The powders compacted by using cold press method (uniaxial) with compact pressure (175 MPa) for 30 seconds to obtained good bonding between its powders.

Sintering of Compacts

The sintering process for green compacts was carried out by put the compacts in a container and inserts then into the electrical furnace (0 to 1200 °C \pm 2°C). The furnace contacted to digital numeric and also a gas regulator. Argon inert gas is used to prevent powder oxidation during the sintering process, and therefore, to get good diffusion bonding between powder particles. The furnace was heated to 473 °C at heating rate 15 °C/min, with pumped of gas at flow rate (1 milliliter/min), this temperature calculated according to the equation (Jartych1995):

$$Ts (K) = (Tm+273) (0.7 to 0.9)$$

(1)

Where:

Ts: sintering temperature.

Tm: melting temperature of Aluminum = $660 \degree C$.

After the temperature of furnace reached to 473 °C, the samples were kept it in the furnace for 60 min, to ensure that all samples reached to the required temperature. After that, the temperature of the furnace was reduced to 150 °C at cooling rate 20 °C/min and argon gas were closed, then the furnace was switch off and the samples kept it in the furnace at room temperature. Fig. (2) show the steps of the sintering process.

Tests of Samples:

Density& Porosity Testing

Apparent density and porosity were calculated after the sintering process for samples according to ASTM B962-15 standard which is based on Archimedes principle. The Apparent density of material is given by equation (1) (Singer1979), and the porosity is given by equation (2) respectively (ASTM1986):

 $\rho = [w_1 / (w_1 - w_2)] * \rho_{\text{Ethanol}}$ (2) $P = [(w_3 - w_1) / (w_3 - w_2) * \rho_{\text{Ethanol}}]$ (3)

Where:

p: apparent density (gm/cm³).
w₁: weight of dry sample (gm)
w₂: weight of suspension sample in ethanol (gm)
w₃: weight of wet sample (gm)

P: porosity %

Wear Test:

(Pin-On-Disk) wear apparatus under dry conditions was used in this work. The samples were prepared with dimension (diameter 1 cm and length 2 cm). Wear test carried out under the constant parameters in which rotational speed of the disk (500 rpm), the distance from the center of the sample to the center of the disk (r = 7cm) and the hardness of the steel disk (35 HRC). Applied load using in the wear test are a static load 10 N, 15 N respectively. Wear rate was calculated by the following relationship (Eyre1976):

Wear rate
$$(Wr) = \frac{\Delta w}{2\pi rnt}$$

Where:

Wr : wear rate (gm/cm).

 Δw : weight loss (gram).

r: The distance from the center of the sample to the center of the disk: r: =7 cm.

n: Number of cycles steel disk (500 rpm).

t: Time of test = 10 min.

In this test, the flat end of specimen 10 mm in diameter and 20 mm length was fixed in chuck jaws to prevent specimens from rotation during the test. Axial load was applied to the pins against the plane surface of the rotating disc. The specimen's ends were polished with (800, 100) SiC emery paper and cleaned with acetone. The wear test was carried out at room temperatures. Each specimen was weighed before the experiment and after it by a digital balance (type Denver with max 210 gm. management system ISO 9001) having a sensitivity of 0.0001 gm. The duration of the experiment was controlled by a digital timer.

Scanning Electron Microscope Test.

Microstructural characterization studies were done to observe the microstructure of sample surface test. This is done by using scanning electron microscope. Characterization is done in etched conditions. Etching was done using the Keller's reagent (1 volume part of hydrofluoric acid (48%), 1.5 volume part of hydrochloric acid, 2.5 volume parts of nitric acid and 95 volume parts of water). The samples were characterized by (Angstrom) Scanning Electron Microscope (SEM) in Nanotechnology and advanced materials research center / University of Technology.

Microstructure Examination Test

The microstructure of Al -12wt%Si and Al-12wt%Si reinforced with CeO_2 nano powder were examined by an optical microscope (100W Carl Zeiss Jane, Germany, EP. Type 2) connected to a digital camera. One surface of all specimens was initially grinding using a series of (500, 800, and 1000) waterproof SiC papers with increasing fineness. Finally, polishing was carried out on a disc polisher using diamond pastes of 1 µm particle size with polishing liquid as a cooling lubricant. Polished samples were cleaned with distilled water and alcohol. The prepared samples were etched using Keller's solution for about 30-50s in order to reveal the

(4)

microstructure with grain boundaries and finally, the polished specimens were taken for optical microscopy .

RESULTS & DISCUSSION :-

Apparent Density and Porosity

Table (2) shows the apparent density, porosity results of Al-12wt% Si with and without wt% CeO_2 nano powder additives. Alloy 1 represented the Al-12wt% Si alloy without any additives, apparent density is 2.7260, while the porosity of this alloy is 18%. The results show the addition of wt% CeO₂ nano powder to Al-12wt% Si alloy will decrease the apparent density with increased the nano CeO_2 addition; conversely, the porosity increased with increases the wt% CeO_2 nano powder addition. Fig. (3 and 4) shows the relationship between densities, porosity with alloy Al-12wt%Si (in different additives of wt.% CeO₂ nano powder). It is clear that the apparent density of the alloy samples decrease with increased addition of wt.% CeO₂ nano powder, while the porosity increased with increases addition of wt.% CeO₂ nano powder to matrix alloy (Osama2010 and Fadhil2010), the decreases in density due to pores expansion from the sintering process (different thermal expansion in compacted samples) which leads to the expansion of porous gaseous inside the compacted samples. As a result of these changes will increase the size of the pores in the compacted samples (this will lead to the expansion of most compacted) after sintering process, and this is due to the of diffusion grain, and most gaps gaseous (pores) transformed from closed gaps into open gaps and appeared as a semi-spherical form.

Wear Rate Results:

From Table (3) and Fig. (5) shows the relationship between wear rates for the Al-12wt%Si alloy (in different additives of CeO_2 nano powder). It was clear that the wear rate of all the Al-12wt%Si reinforced by CeO₂ nano powder (1, 2, and 3% wt) were been less than the wear rate of without additives with the alloy at least the increase in the fraction volumetric of particles and this is due to the hardness increase with increasing volumetric fraction. Wear rate increase with increase applied load and decrease with increase the CeO₂ nanoparticles (Madhu2012 and Haitham2010. The increase in the wear rate with increase the applied load is due to increase the amount of small separate from the material (debris) particles sample (composite material) as a result of increased friction and pressure with a hard disk device and these particles increase the wear of the sample surface because it works stress center on the sample in the areas of presence [21, 22]. It is noted that the increase in load leads to increase the wear rate where the wear of shifting mild wear to wear transition and to the wear severe and this is due to plastic deformation quotient to the tops of bumps surface of the sample, leading to Increase the density of dislocations and thus a strain hardening.

MICROSTRUCTURE :

Microstructural characterization studies were done to observe the microstructure of sample surface test. This is done by using an optical microscope and SEM. Characterization is done in etched conditions. Figs. from (6-9) show the microstructure of Al-12wt%Si alloy without and with additives CeO_2 nanoparticles after the sintering process. It is noticed clear that different in microstructure in shape and size of Si-phase and eutectic Al-Si between nanocomposites (MMNC) reinforced with nano powder CeO_2 . The microstructures of Al-12wt%Si alloy consist

of Al matrix and Si phase and different pores dispersed in the matrix. A little agglomeration was occurred leading to a formation of large particles; this is due to insufficient mixing time for powders. Figs. from (10-12) show the scanning electron microscope of nanocomposite materials. It is clear that nanoparticles are dispersion and distributed uniformly in the Al-12%Si matrix. The microstructure evaluation also shows that, for a given series of composites, the size of the particles in the nanocomposites increases as the content increases. A small agglomeration of particles in the Al matrix has been noticed and this is mainly due to non-homogeneity involved in mixing process carried out before sintering as shown in Fig. (11).

CONCLUSIONS :-

- 1. The addition of Cerium oxide as a nanoparticles reinforcement to the Al-12wt%Si alloy was contributed to decreasing the wear rate for all additions percentage of CeO_2 nanoparticles.
- 2. Wear rate of the base alloy and nanocomposites increases with increasing applied load.
- 3. Apparent density decreases slightly with increasing the CeO_2 nanoparticles reinforcement that added to the Al-12wt%Si alloy.
- 4. Increasing the weight percentage of Cerium oxide nanoparticles led to increasing the porosity for nanocomposites as compared to the base alloy.

No. of sample	Al%	Si%	CeO ₂ %
1	88	12	-
2	87	12	1
3	86	12	2
4	85	12	3

Table (1) The weight percent of composition samples.

Table (2) The apparent density, porosity of samples.

Samples	Apparent Density gm./cm ³	Porosity %	
A1-12%Si	2.726012	18	
Al-12%Si-1%Ce ₂ O	2.720406	22.4	
Al-12%Si-2%Ce ₂ O	2.710619	24.2	

	Al-12%Si-3%Ce ₂ O	2.694933		26.5		
	Samples	Wr (10 ⁻⁷) (gm/cm) at P=10N	Wi (gi at]	r (10 ⁻⁷) m/cm) P=15N		
	Al-12%Si	5.82		7.16		
Table (3) The wear P=10N, P=15N.	Al-12%Si-1%CeO ₂	4.45		6.17	- rate	
	Al-12%Si-2% CeO ₂	3.59		5.53		
	Al-12%Si-3% CeO ₂	3.17		5.06		

rate of samples, at



Fig. (1) The electric rolling mixers.



Time

Fig. (2) The procedure of sintering process.



Fig. (3) Effect of the wt%CeO₂ nano powder additions on the apparent density of the Al-12wt%Si alloy



Fig. (4) Effect of the wt%CeO₂ nano powder additions on the porosity of the Al-12wt%Si alloy



Fig. (5) Effect of the wt%CeO₂ nano powder additions on the wear rate of the Al-12wt%Si alloy





Figure (7) Microstructure of Al-12wt%Si reinforced by 1wt% CeO₂ nanoparticles.





Figure (8) Microstructure of Al-12wt%Si reinforced by 2wt% CeO₂ nanoparticles.

Figure (9) Microstructure of Al-12wt%Si reinforced by 3wt% CeO₂ nanoparticles.



Figure (10) SEM of MMNC with 1wt% CeO₂ nanoparticles.





Figure (12) SEM of MMNC with 3wt% CeO₂ nanoparticles.

REFERENCES :-

A. Hamid, P. Ghosh, S. Jain, S. Ray: The influence of porosity and particles content on dry sliding wear of cast in situ Al (Ti)–Al₂O₃(TiO₂) composite, Wear, Vol. 265, No. 1&2, pp.14-26, 2008.

ASTM part 15.02 (C 373 – 72) water absorption Bulk density, apparent porosity of fired white ware products (1986).

E. Jartych, D. Oleszak, J. Zeng, B. von Gromann, C. Haberling, and H.G. Haldenwanger: Conf. on Aluminum Alloys and Their Application, K.U. Kainer, Wolfsburg, Germany ,62-67, 1995.

Eyre T.S., "Wear characteristic of Metals", Tribology International pp 203-212, (1976).

G. B. Veeresh Kumarı, C. S. P. Rao, N. Selvaraj. "Mechanical and Tribological Behavior of Particulate Reinforced Aluminum Metal Matrix Composites", Journal of Minerals & Materials Characterization & Engineering, Vol. 10, No.1, pp.59-91, 2011.

G. O'Donell, L. Looney, Mater. Sci. Eng. A 303, 292, 2001.

H.T. Son, T.S. Kim, C. Suryanarayana, B.S. Chun, "Homogeneous dispersion of graphite in a 6061 aluminum alloy by ball milling" Materials Science and Engineering A348 pp.163_169, 2003.

Haitham Razouqi Saleh, "Mechanical Properties of the Modified Al-12%Si Alloy Reinforced by Ceramic Particles" Eng. & Tech. Journal, Vol.28, No.2, 2010.

Lee, C. S., Y. H. Kim, K. S. Han and T. Lim., "Wear behavior of aluminum matrix composite materials", Journal of Materials Science Volume 27, Number 3 1992. M.E. Smagorinski, P.G. Tzantrizos, S. Grenier, A. Cavasin, T. Brezenski, G. Kim, Mater. Sci. Eng. A 244, 86, 1998.

M.O. Shabani, A. Mazahery "The performance of various artificial neurons interconnections in the modelling and experimental manufacturing of the composits", Materials and technology, Vol. 46, No. 2, pp. 109–113, 2012.

Madhu Kumar YC, Uma Shankar, "Evaluation of Mechanical Properties of Aluminum Alloy 6061-Glass Particulates reinforced Metal Matrix Composites", International Journal of Modern Engineering Research (IJMER), Vol.2, Issue.5, pp.3207-3209. Sep.-Oct. 2012

P. Cavaliere, E. Evangelista: Isothermal Forging of Metal Matrix Composites: Recrystallization Behaviour by Means of Deformation Efficiency, Composite science and technoogy, Vol. 66, pp. 357–362, 2006.

P. Poddar, S. Mukherjee, K.L. Sahoo: The Microstructure and Mechanical Properties of SiC Reinforced Magnesium Based Composites by Rheocasting Process, Journal of materials engineering and performance, Vol. 18, pp. 849–855, 2009.

Peter J, Blau, "Fifty years of research on the wear of metals", Tribology International Vol. 30, No. 5, pp. 321-331, 1997.

Prabhu Swamy, N.R., C.S. Ramesh and T. Chandrashekar, "Effect of Heat Treatment on Strength and Abrasive Wear Behavior of Al 6061-SiCp Composites", Bull. Mater. Sci., Vol.33, No.1, pp49-54, 2010.

R. Dwivedi, "Performance of MMC Rotors in Dynamometer Testing", SAE Technical Paper Series, 940848, Warrendale, PA, USA, 2011.

S. Srivastava, S. Mohan "Study of Wear and Friction of Al-Fe Metal Matrix Composite Produced by Liquid Metallurgical Method", Tribology in Industry, Vol. 33, No. 3, pp. 128-134, 2011.

Singer, F. & Singer, S., "Industrial Ceramic", Chapman and Hall LTD, Published, 1979.

U. Sanchez-Santana, C. Rubio-Gonzalez, G. Gomez-Rosas, J.L. Ocana, C. Molpeceres, J. Porro, M. Morales, "Wear and friction of 6061-T6 aluminum alloy treated by laser shock processing", Wear 260 pp 847–854, 2006.

اسامة سلطان محمد، "البنية المجهرية ومعدل البلى للمواد المتراكبة ذات اساس من سبيكة الالمنيوم – سليكون والمقواة بدقائق الايتريا"، مجلة الهندسة والتكنولوجيا، المجلد 28 ، العدد 23، 2010.

فاضل عطية جياد، احمد حسين علي و رونق صلاح الدين مهدي، " در اسة الخواص الفيزيائية لمادة متر اكبة من نظام الالمنيوم _كاربيد البورون (B₄C) " ، مجلة الهندسة والتكنولوجيا،المجلد 28 ،العدد 1، 2010.