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# CORROSION of BOILER TUBES in SOUTH BAGHDAD ELECTRIC STATION

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### ABSTRACT

The corrosion of low carbon steel boiler tubes in demi water had been investigated. The purpose of this investigation was to determine the change produced in corrosion behavior of the carbon steel as a result of the specific presence of chloride and copper ions in the water under different temperatures.

For low carbon steel experiments, the temperature was taken in three levels (125, 175, and 215°C) under about 27 bar pressure and 1500 rpm in autoclave. Using weight loss technique, the corrosion rate ranges from (85 to 789 gmd) for low carbon steel boiler tubes.

### **INTRODUCTION**

Corrosion can cause serious problem to the safe and economic operation of a wide variety of industrial installations. However, in order to understand a corrosion problem or situation, it is very important to be able to recognize the type of problem one is dealing with [1].

Water is a naturally occurring substance; because except in rare cases it is not sufficiently pure, it cannot be used for human consumption or in industry without some form of treatment. The main use of water in industry is the transfer of heat and the production of steam. Cooling water is used extensively in every manufacturing process, in fossil and nuclear, fueled steam plant and attendant steam generation dominate the power generating field [1].

Water in the boiler section is heated to high temperature (260-315°C). The water is deaerated (usually by Na2SO3 addition) to reduce the O2 content less than (50 ppb) in a well operating boiler. Some boilers are operated with zero solid water. High-purity water was used in the boiler; deaeration is obtained by adding volatile hydrazine or hydrazine

Replacement which is called carbohydrazid: A to control the pH and also reduce the O2 content [2].

Carbon steel is widely used in chemical process plants for several important reasons. For one; it is low in cost, easy to fabricate, strong, and performance specifications are well defined. However, the general corrosion resistance of carbon steel is low in certain environment. Most iron occurs naturally as stable oxide, and iron that had been processed into steel tend to return to that form [3].

Iron and steel corrode in water to form various compounds depending upon the temperature and other environment conditions. Theoretically, iron should react with water in the absence of air to form ferrous hydroxide:

Fe + 2H2O or (H+, OH-)  $\Rightarrow$  Fe (OH) 2 + H2 $\uparrow$ 

However, even extremely small quantities of dissolved O2 in water will produce ferric ions which color the ferrous hydroxide to green.

The up normal chemical control (i.e., ammonia dosing) and up normal operating conditions (i.e., steam and water velocities) may lead to a leakage in the condenser tubes causing dissolution of Cu from the Cu-Ni alloy. Drops of raw water may enter from the cooling side (tubes) to steam side (shell) holding contaminants

 $(i.e., Cl^{-}, SO_{4}^{-2}, SiO_{2}, O_{2}, O_{2})$ 

organic mater in addition of Cu+2). So, this polluted water will enter the boiler where the corrosion problem will initiate because of high temperature (380 °C), and high pressure (60 bar).

In this investigation, the interest lies in corrosion behavior of iron a widely used in the steam power plant with demi water as corrosive media.

## EXPERIMENTAL WORK

Specimens Preparation

Specimens of low carbon steel with dimensions of about  $(3 \text{ cm } \times 1.5 \text{ cm})$  and (0.51 cm) thickness rectangular in shape were used exposing about 4.5 cm2 surface area to the corrosion media

## **Cleaning procedure**

Specimens were cleaned by washing with detergent and flushed with tap water followed by deionized water, degreased by analar benzene and acetone, then annealed in vacuum at 600°C for 1 hour and cooled under vacuum to room temperature. Finally, they were stored in a desicator over a silica gel to be used.

## Specific treatment

Specimens carbon-steel were abraded in sequence using emery paper of grade number 220, 320, 400, and 600 then washed with running tap water followed by deionized water, then dried with clean tissue, degreased with benzene, dried, degreased with acetone, dried, and finally left to dry for one hour in a desicator over silica gel. Weighing the specimens were carried out using 4 decimals digital balance and its dimensions were measured with a vernier.

## **Experimental procedure**

The tests were carried out using a standard reactor (autoclave) as shown in Fig. (1) Made of stainless steel and consist of pressure gauge and thermocouple which are sealed in stainless steel probe, internal agitator with stirring shaft hanged on it a specimen, safety pressure discs which protect the operator and the equipment from accidental destructive pressure. Also consists of fitting for nitrogen feed. The carbon steel rectangular shape specimens were placed in taflon frame as shown in Fig. (1) Hanged on rotating shaft at constant speed of 1500 rpm in a reactor pressure vessel (autoclave) containing 250 ml of corrosive solution.

Before starting the experiment, the pressure was raised to 32 bar in the reactor for leakage checking by using pure nitrogen (98.0%), after that the pressure was reduced to the desired value of (i.e., 27 bar). After they were exposed for one hour to the desired temperature of (125, 175, 215) °C and pressure of (27) bar. The specimens were cleaned with running tap water using a brush, followed by deionized water, dried with clean tissue, then degreased with benzene, dried, degreased with acetone, dried, left for one hour, then the weight loss was measured and the corrosion rate was obtained.



Fig (1) Auto-clave system for corrosion rate measurement under high temperature and pressure

#### **RESULTS AND DISCUSSION**

#### Corrosion Behavior of Low Carbon Steel Pipes Used in Boiler

The influence of temperature (125, 175, and  $215^{\circ}$ C), chloride concentration as NaCl (0.5, 50.25, and 100 ppm) beside copper concentration Cu+2 (0.005, 0.0125, and 0.02 ppm), were studied using weight loss technique. The experiments were designed according to factorial method and 27 runs have been achieved as shown in Table (1).

It is important to mention here that the rotational mixer speed during the experiment was fixed at (1500 rpm) and the pressure at  $(27\pm1)$  bar.

#### **Effect of Temperature**

The rate of metallic corrosion is dependent on temperature like most chemical reactions. Experiment at different temperatures and fixed flow velocity solution containing different concentration of  $\Omega^$ and Cu+2 ions as NaCl and CuSO4.5H2O respectively, were carried on flow velocity was expressed as rotational mixer speed at 1500 rpm. Fig. (2) shows the result of activation energies of low carbon steel obtained as log corrosion rates versus temperature reciprocal using Arrhenius form, a linear relationship was obtained giving different activation energies (7.75, 4.58, 3.935, and 2.89 kcal/mol) depending on the  $\Omega^-$  and Cu+2 ions concentration in the solution.

The values of activation energy (7.75 kcal/mol) indicates that at 0.5 ppm chloride and 0.005 ppm copper, the reaction is to some extent slow while when the copper concentration was increased to 0.02 ppm in the same time fixing the chloride concentration at 0.5 ppm, the reaction become faster (i.e. activation energy= 4.58 kcal/mole < 7.75 kcal/mole).

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Fig. 2 Arrhenius plot for the corrosion rate of low carbon steel at different concentration of chloride and copper ions

Table (1) Corrosion rate results of factorial experimental runs for the boiler. Low carbon steel Pipes achieved in the autoclave

| Run | Temperature | Chloride | Copper | C.R.* |
|-----|-------------|----------|--------|-------|
| No. | (°C)        | (ppm)    | (ppm)  | (gmd) |
| 1   | 125         | 0.5      | 0.0050 | 85    |
| 2   | 125         | 0.5      | 0.0125 | 142   |
| 3   | 125         | 0.5      | 0.0200 | 213   |
| 4   | 125         | 50.25    | 0.0050 | 172   |
| 5   | 125         | 50.25    | 0.0125 | 230   |
| 6   | 125         | 50.25    | 0.0200 | 307   |
| 7   | 125         | 100      | 0.0050 | 266   |
| 8   | 125         | 100      | 0.0125 | 349   |
| 9   | 125         | 100      | 0.0200 | 401   |
| 10  | 175         | 0.5      | 0.0050 | 293   |
| 11  | 175         | 0.5      | 0.0125 | 341   |
| 12  | 175         | 0.5      | 0.0200 | 454   |
| 13  | 175         | 50.25    | 0.0050 | 382   |
| 14  | 175         | 50.25    | 0.0125 | 451   |
| 15  | 175         | 50.25    | 0.0200 | 513   |
| 16  | 175         | 100      | 0.0050 | 457   |
| 17  | 175         | 100      | 0.0125 | 524   |
| 18  | 175         | 100      | 0.0200 | 591   |
| 19  | 215         | 0.5      | 0.0050 | 506   |
| 20  | 215         | 0.5      | 0.125  | 595   |
| 21  | 215         | 0.5      | 0.0200 | 609   |
| 22  | 215         | 50.25    | 0.0050 | 591   |
| 23  | 215         | 50.25    | 0.0125 | 641   |
| 24  | 215         | 50.25    | 0.0200 | 721   |
| 25  | 215         | 100      | 0.0050 | 667   |
| 26  | 215         | 100      | 0.0125 | 739   |
| 27  | 215         | 100      | 0.02   | 789   |

\* All corrosion rate valued in the last column are recorded from putting the sample in the corrosive media waiting until reaches the required temperature then 1 hr exposure time

Similarly, when the chloride concentration was increased to its maximum value. Fixing the copper concentration at its minimum value, the reaction goes faster (i.e. 3.94 and 2.89 kcal/mol) indicating that chloride concentration leads the reaction to be under diffusion control. In the closed system as in this study no oxygen is permitted to escape. As a result of the rise in temperature, the corrosion rate increases steadily with the temperature. Figs. (3 - 5) show the effect of increasing temperature on the corrosion rate of carbon steel pipes at different concentrations of

- $Cl^-$  and Cu+2 ions. It is clear that:
  - Generally, the corrosion rate is higher as the <sup>CI<sup>-</sup></sup> ions increases at different Cu+2 ions concentration.
  - 2. At all concentrations of  $Cl^-$  ions where the Cu+2 increases the corrosion rate increase with the temperature. This can be attributed to Cu+2 ions acting as cathode with respect to the carbon steel which act as anode. So, increasing Cu+2 ions cause an increase in the corrosion rate.

Finally, the results indicate that the corrosion attack proceeds by linear kinetics throughout the temperature range (125-215°C) studied in presence of  $Cl^-$  ions range (0.5-100 ppm) and Cu+2 ion range (0.005-0.02 ppm).

Accordingly, it is evident that since the experimental results show that corrosion process follows linear rate law, it's the chemical surface reaction which controls the kinetics in this case.

The same results was found by Kameswari[4] in his study of the relative corrosion resistance of different boiler steels in presence of sugar can, phosphates, sulfate, and chloride of sodium as the ash contains. He found that the weight loss data as function of temperature and time follows linear kinetics.









#### **Effect of Chloride**

Figures (6 - 8) show the effect of increasing the  $\square^-$  ions concentration on the corrosion rate of low carbon steel pipe at different concentrations of Cu+2 ions for elevated temperature. In the sodium chloride solution, the conductivity is greater hence additional anodes and cathodes can operate. It can be stated that:

1. Generally the corrosion rate increases with increasing  $Cl^-$  ions

concentration at all Cu+2 concentration for all temperatures.

2. At certain temperature, corrosion rate increase with increasing  $\Omega^-$  and Cu+2 ions concentrations.

The effect of  $Cl^-$  ions on the corrosion rate can be explained as follows: Chloride ions are able to destroy passive films formed on metals such as iron, and increase the corrosion rate of attack.

This behavior result from the conflicting effect of rising solution conductivity. Higher solution conductivity faster or greater physical separation between the anodi and permits the formation of cathodic product Fe (OH)2 at a distance from the steel surface. Because Fe (OH)2 formed in this way cannot provide a protective layer, the corrosion is not inhibited, so, a change in concentration of a salt can influence the corrosion rate.



Fig. 5 The effects of temperature on the corrosion rate of carbon steel at different copper concentration and chloride









### **Effect of Copper**

Figures (9 - 11) show the relationship between the corrosion rate of low carbon steel and the concentration of Cu+2 ppm in the solution with different  $Cl^-$  ion concentration at various temperature levels. It can be stated that:

1. The corrosion rate increase with increasing Cu+2 ion concentration at

all  $\mathbf{Q}^{-}$  ion concentration for all temperatures.

2. At a given temperature, corrosion rate increase with increasing Cu+2 and  $Cl^-$  ions concentration.

As the result of up normal operation i.e., the presence of high concentration of ammonia in aerated water which leads to corrode the copper alloy followed by forming oxide layers, transferred to the boiler and

deposited their causing increasing the corrosion rates of carbon steel.

Iron dissolves by displacing another metal which is already in solution in the electrolyte. This may be noted by submerging iron in copper solution. When this is done, the iron goes into solution in the electrolyte and the copper is deposited upon the iron [5].



Fig. 8 The effects of chloride ion on the corrosion rate of carbon steel at different temperature and copper concentration of (0.02 ppm)



Fig. 9 The effects of copper ion on the corrosion rate of carbon steel at different chloride concentration and Temperature (125°C)



Fig. 10 The effects of copper ion on the corrosion rate of carbon steel at different



Fig. 11 The effects of copper ion on the corrosion rate of carbon steel at different

### CONCLUSIONS

On the basis of the results presentedThe corrosion rate of boiler carbon steel tubes in water showed no minimum value in all experiments, (i.e. the higher the value of one variable when the second variable was fixed led to higher corrosion rate.

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