



Enhancement of an Iraqi Radial Distribution System Performance Using Multi-Object Particle Swarm Optimization

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HIGHLIGHTS

- MO-PSO algorithm for fast convergence and good-tuning feature.
- Adding DG and D-STATCOM simultaneously.
- IEEE 33-Bus and real 65-bus Iraqi RDS.
- enhancement voltage stability, improve voltage and minimize power losses by multi-objective function.
- Different cases and different load factor by using Newton Raphson load flow and MATLAB program.

ABSTRACT

This paper proposes a Multi Object Particle Swarm Optimization (MOPSO) to find the optimal location and capacity of Distributed Generation and D-STATCOM device. The objective function has adapted with a multi-objectives function to improve voltage profile, the voltage stability and reduce the total power loss of the Radial Distribution System (RDS). Basically, the voltage stability index (VSI) has been used to pre-determine the optimal location of DG and D-STATCOM. Then, a MOPSO applies to achieve the suitable size of DG and D-STATCOM units with different load models. The proposed method is compared with other existing methods and it was obtained losses reductions and enhancement voltage stability and average voltage when was tested on IEEE 33-bus and real Iraqi 65-bus radial distribution system through simulation using MATLAB. Furthermore, different cases were considered for using the (MOPSO) algorithm at different load factors.

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1. Introduction

The electrical distribution system is one of the main parts of the power system has a very high R/X ratio it causes high voltage drop and power losses which lead to voltage fluctuation, sag and instability.[1]. Different techniques have been suggested by planners for mitigating distribution systems loss and enhancement the voltage system stability issues.

Recently, small generators have been proposed that connected directly to distribution systems which are defined as Dispersed generators (DG) [2]. DG exhibits several features compared to conventional power generation such as, it can mitigate electrical losses, considers a clean technology, improves reliability, provides low-cost power and improves the power quality and the voltage profile. Furthermore, electrical system planners are applying DGs, to avoid the expansion of an existing electrical system which, become not practically feasible because of cost requirement, the complexity of protection system design, time requirements and environmental issues [1, 3, 4].

On the other hand, shunt capacitors have been used to compensate the reactive power in distribution grids to mitigate loss and improve power factor. However, these shunt capacitors are not capable to constantly produce a variable reactive power and exhibits some operational problems like resonance [2]. So, these restrictions on the construction of shunt capacitor have persuaded the power system designers to look for some alternative solutions to increase the power system stability and efficiently transmit power over the transmission lines.

In recent times, power system planners applying Distribution Flexible AC Transmission (D-FACT) controllers, which can absorb or inject reactive power in the system as an efficient shunt capacitors substitute. [2]. The distributed static synchronous compensator (D-STATCOM) is one of the most efficient shunt D-FACTS devices due to it features like zero resonance, less harmonic distortion, low power losses, low cost, compact size and high regulatory capability [3, 5].

The integration of DG and D-STATCOM has a significant role in enhancing the performance of the distribution systems. The optimal placement and the size of these devices have a great impact on the improvement of the distribution system performance such as minimizing of the distribution systems losses, enhancement the voltage stability and maintaining the voltage profile within acceptable limits [6].

The identification size and location of these devices have faced some challenges especially for large systems with a wide range of devices capacity. However, the researchers had suggested many techniques to solve the problem. The modification of the optimization techniques provides a good solution to overcoming these challenges. Generally, these optimization techniques refer to determine the optimal solution through maximizing /minimizing single or multiple objective functions [7].

Several studies have been presented under the name of meta heuristic techniques such as “,Whale Optimization Algorithm(WOA)[8], Improve Differential Search Algorithm (IDEA)[9], Genetic Algorithm (GA)[10],A combination of Genetic Algorithm and Particle Swarm Optimization (GA and PSO)[11]], Particle Swarm Optimization (PSO)[12], Grey Wolf Optimization Algorithm (GWOA)[13], Harmony Search Algorithm (HSA)[14],Gravitational Search Algorithm (GSA) [15] and Slap Swarm Algorithm (SSA)[16]” to find the optimal site problem of DG and D-STATCOM in power systems. A lot of studies mentioned above have been carried out to locate the optimal location and size problems of DG and D-STATCOM devices separately or simultaneously but did not add multiple DGs and D-STATCOMs in the real systems [12, 17].

Remarkably, in spite of the huge methods that have been suggested by researchers to find the proper allocation to insert the DG and the D-STATCOM in a radial distribution system they did not consider a real system application. In [18] the Multi Object-Modified flower pollination algorithm MO-MFPA had been applied to insert PV and DSTATCOM simultaneously at 33, 69, and 118-bus test systems. A Latin hypercube sampling (LHS) algorithm considered to determine the location of DSTATCOM in 69 bus test system [19].

Further research on using the (VSI) and Whale Optimization (WOA) was developed to select the proper location and best size of DG to enhancing the voltage stability and increase the load ability through injecting the appropriate active and reactive powers. However, the best DG place is allocating by using the VSI to find the most sensitive buses [20]

In this paper, it is assumed that DG placement is to compensate the only real power, whereas the DSTATCOM placement is to compensate only reactive power in the distribution system

The motivation of this study is to apply a multi-object Particle Swarm Optimization Algorithm (MOPSO) for optimal placement and sizing of DG and D-STATCOM device. The algorithm based on a multi-objective PSO to minimize the system power losses and voltage profile enhancement as well as increasing voltage stability system. Verification of the proposed algorithm has been achieved on standard IEEE 33-bus and Iraqi 65-bus radial distribution systems through simulation using MATLAB. The paper is organized as follows. Section 2 explains the system modeling. Section 3 presents the problem formulation. A multi object particle swarm optimization (MO-PSO) introduces in section 4. In section 5, simulations of a distribution system under a different case with the proposed algorithm is presented. Furthermore, a performance comparison of the system is then carried out over other existing algorithms in supporting voltage stability and loss reduction in distribution networks. Finally, section 6 gives concluding remarks on the current work.

2. System Modelling

2.1 D-Statcom Modelling

D-STATCOM is a power electronic device using to control power flow[21]. D-STATCOM is one of the third generation FACTS devices that injects or absorbs the desired reactive power at the point connecting with the system [22] .According to the V-I characteristic of DSTATCOM shows in the Figure. 1 [23]. It is clear that the D-STATCOM absorb reactive power, when the reference voltage (V_{REF}) higher than the voltage of the network and the D-STATCOM inject reactive power, when the reference voltage (V_{REF}) lower than the voltage of the network.

The reactive power of D-STATCOM evaluate by

$$Q_{D-STATCOM} = V_{rnew} (I_{D-STATCOM})^* \tag{1}$$

Where $I_{D-STATCOM} \angle ((\frac{\pi}{2}) + \theta_{new})$ is the injected current by DSTATCOM

$V_{Rnew} = V_{Rnew} \angle \theta_{new}$ is the voltage of bus ‘R’ after correction.

$$V_{Rnew} \angle \theta_{new} = V_S \angle \delta - (R_{SR} + jX_{SR}) I_L \angle \alpha - (R_{SR} + jX_{SR}) I_{D-STATCOM} \angle ((\frac{\pi}{2}) + \theta_{new}) \tag{2}$$

Figure.2(a) shows the single line diagram of two buses of a distribution system with D-STATCOM that is installed in bus ‘R’. The Voltage of bus ‘R’ changes from V_R to V_{Rnew} as shown in Figure.2 (b).

DSTATCOM has features like low power losses ,zero resonance, low cost, less harmonic distortion, high regulatory capability and compact size .These features made the D-STATCOM preferable to use at the distribution grids, improve the load ability ,enhance the voltage profile, minimize real power loss and enhance stability[6].However, choosing the correct place of D-STATCOM is important to minimize network power loss and is subjected to the following standard limits[24].

Voltage limit: $V_{R,min} \leq V_R \leq V_{R,max}$

Injected reactive power limit: $Q_{DSTATCOM(i)}^{min} \leq Q_{DSTATCOM(i)} \leq Q_{DSTATCOM(i)}^{max} \quad i=1, 2, 3, nb$

Where $V_{R,min}$ is the minimum Voltage limits of bus 'R' and $V_{R,max}$ is the maximum Voltage limits of bus 'R'?

$Q_{DSTATCOM(R)}^{min}$ is the minimum reactive power limit of compensated bus 'R' and $Q_{DSTATCOM(R)}^{max}$ is the maximum reactive power limit of the compensated bus 'R'

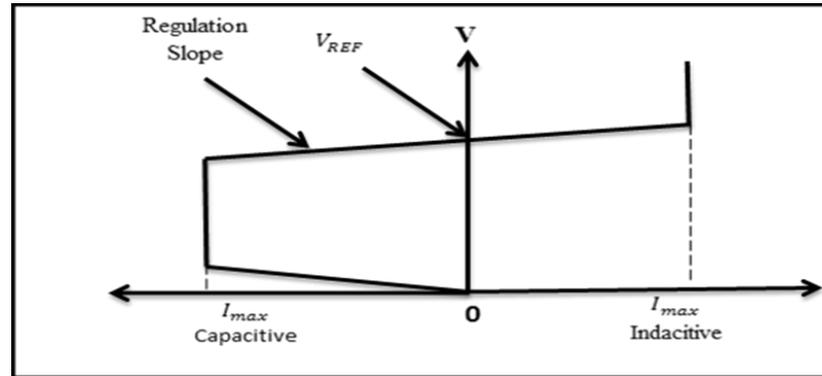


Figure 1 : V-I characteristic of DSTATCOM [23]

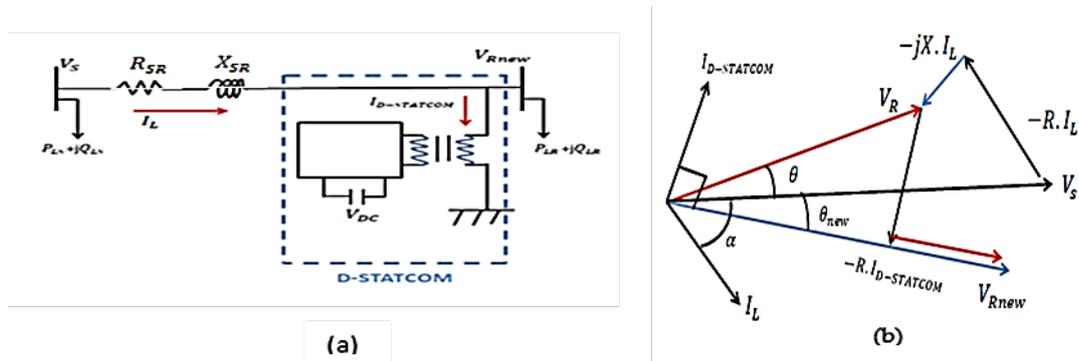


Figure 2: (a)Single line diagram of two buses with D-STATCOM[12]. (b)The phasor diagram of two buses with D-STATCOM [12]

2.2 Distributed Generation (Dg)

Distributed Generation (DG) is effective local power source supply power from a few watts (W) to ten megawatts (MW) which is commonly powered by renewable energy, DG exhibits several features compared to conventional power generation. It is able to inject the different value of active and reactive power and connected directly to the distribution system. [1,25]. There are many types of DG which are included as renewable and non-renewable power sources such as, induction generators, micro turbines, synchronous generators, fuel cells, solar photovoltaic, wind turbines, combustion gas turbines and other small power generation sources DGs also are divided into the following four types according to the supplying power of DG[2] :

1. DG type one: DG injects real power (P) only.
2. DG type two: DG injects both real and reactive power (P&Q).
3. DG type three: DG injects real (P) power but absorbs reactive power.
4. DG type four: DG injects reactive power (Q) only.

The main features of DGs are mitigating from the greenhouse effect and using of fossil fuel, improving the voltage profile, energy security, reliability, stability and power quality as well as reduces the power losses[1]. However, the optimal locations of DGs are also important to improve the system operation characteristics and subjected to the following standard limits [9].

Voltage limit: $V_{R,min} \leq V_s \leq V_{R,max}$

Injected real power limits: $P_{R,min(i)} \leq P_{R(i)} \leq P_{R,max(i)}$ $i = 1,2,3 , nb$

Where $P_{R,min(R)}$ is the minimum real power limit of compensated bus 'R' and $P_{R,max(R)}$ is the maximum real power limit of compensated bus 'R'

3. Problem Formulation

3.1 Load Flow Analysis

The power flow study is necessary for analyzing, designing and planning expansion of the power system and obtaining real and reactive power reading at each line and voltage magnitudes and their angles at each bus. Newton-Rap son method with balance condition is considered in this paper where the power-flow equation is derived in polar form and written in term of admittance matrix Y, The relation between the bus voltages V and the current I injected at the network buses is described in equation(3) according to the Kirchoff's Current Law [26]

$$I_i = \sum_{j=1}^n Y_{ij} V_j \tag{3}$$

The total loss of the system evaluated by summing the losses of all the branch by Equation (4) below[3]

$$S_{total\ loss} = \sum_{S=1}^{no.branch} P_{loss}(S, R) + j \sum_{S=1}^{no.branch} Q_{loss}(S, R) \tag{4}$$

Where the loss in a branch between buses 'S' and 'R' of two buses network illustrated in figure 3 is calculate by using Equation (5) and (6) for real and reactive losses respectively.

$$P_{loss}(S, R) = \left(\frac{P_S^2 + Q_S^2}{|V_S|^2} \right) * R_{SR} \tag{5}$$

$$Q_{loss}(S, R) = \left(\frac{P_S^2 + Q_S^2}{|V_S|^2} \right) * X_{SR} \tag{6}$$

3.2 Objective Function

The radial distribution networks often expose to voltage collapse due to the low level of the voltage stability index. Therefore, the voltage stability index should be considered in the objective function to avoid the voltage collapse problem occurrence. As power losses have a greater effect on utilities and represent the major concern in the power system network [3]. Hence, to avoid conflicting between the VSI and the voltage collapse, the multi objective function has been modeled in this paper. The objective function of the optimization algorithm is adapted a number of functions to be optimized simultaneously included the maximize voltage stability index, enhance the bus voltage profile and mitigate the power loss with a weighting factor. Equations (7) illustrate the objective function that is considered in this work.

$$\text{Minimize (Fitness)} = \min \left(\beta_1 \left(\Delta P_{TL}^{DG/DST} \right) + \beta_2 \left(\frac{1}{AV(x)} \right) + \beta_3 \left(\frac{1}{\Delta VSI^{DG/DST}} \right) \right) \tag{7}$$

Where $\Delta P_{TL}^{DG/DST}$ is the ratio of total power loss after and before adding DG/D-STATCOM in RDS which given by[3]

$$\Delta P_{TL}^{DG/DST} = \frac{P_{TL}^{DG/DST}}{P_{TL}} \tag{8}$$

$\Delta VSI^{DG/DST}$ is the ratio of voltage stability index of weaken bus after and before adding DG/D-STATCOM in RDS which is given by [3]

$$\Delta VSI^{DG/DST} = \frac{VSI_{after}^{DG/DST}}{VSI_{before}} \tag{9}$$

$AV(x)$ is the average of buses voltages which is given by[18]

$$AV(x) = \left(\frac{\sum_{i=1}^n V_i(x)}{n} \right) \tag{10}$$

β_1, β_2 and β_3 are the weighting factors of minimization power loss and maximization AV and VSI respectively which considered (0.7), (0.3) and (0.3) respectively

3.3 Voltage Stability Index

It is important to consider the VSI in the objective function to avoid the voltage collapse problem. Whereas, the voltage stability was defined in[3] as "the ability of a system to maintain voltages in acceptable range so that when system nominal load is improved, the real power that delivered to the load by the system will rise and both voltage and power are controllable".

In this part, the weak buses of the system are found by applying (VSI) to mitigate the search range of the optimization algorithm. Thus, DGs and D-STATCOM will be adding in the optimal locations. Then, the multi object particle swarm optimization (MOPSO) algorithm will be utilized to determine the optimal size of both DG and D-STATCOM. The simultaneous voltage stability index value can be determined by the below relation [1]

$$VSI_R = |V_S|^4 - 4(P_R X_{SR} - Q_R R_{SR})^2 - |V_S|^4 (P_R R_{SR} + Q_R X_{SR}) \tag{11}$$

Where VSI_R is voltage stability index of node 'R' of two buses distribution system which was showed in Figure 3?

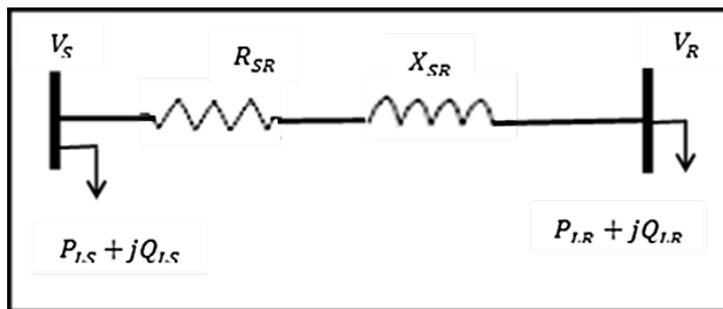


Figure 3: Single line diagram of two buses network [12]

4. Particle Swarm Optimization (PSO)

A particle swarm optimization (PSO) is used in this work to determine the optimal location and size of DG/ D-STATCOM. A particle swarm optimization algorithm PSO is introduced by [27] to solve the optimization problem. The performance of the PSO algorithm is preferred due to its fast convergence feature. Figure 4 shows the flowchart of the proposed PSO. To illustrate the PSO algorithm, the steps of the algorithm are below:

Step1: adjusted the counter $t = 0$

$X_i(0)$, particles location stochastically generated where $[i=1, 2, 3, n]$

$V_i(0)$ particles speed generated stochastically

$W(0)$ adjusted to be 0.8.

$F(0)$ Run load flow program to evaluate fitness value.

Step 2: update counter $t = t + 1$.

Step 3: update weight inertia factor according to equation 1.

Step4: update particles speed to change the particle speed according to equation 12.

$$V_i(t + 1) = wV_i(t) + c_1t_1(pbest_i(t) - x_i(t)) + c_2t_2(gbest_i(t) - x_i(t)) \quad (12)$$

Where, $V_i(t)$ and $V_i(t + 1)$ are previous and new speed of the current particle

C_1 And C_2 are acceleration coefficients that introduce in [28] as below:

$$C_1 = C_{a1} + \left(\frac{C_{b1} - C_{a1}}{t_{max}}\right) * t, \quad C_2 = C_{a2} + \left(\frac{C_{b2} - C_{a2}}{t_{max}}\right) * t$$

Where $C_{a1} = 2.5$, $C_{b1} = 0.5$, $C_{a2} = 0.5$, $c2f = 2.5$

r_1 And r_2 are random numbers.

Step 5: update particles location according to equation 13 without violates the limits.

$$x_i(t + 1) = x_i(t) + V_i(t + 1) \quad (13)$$

Where, $x_i(t)$ and $x_i(t + 1)$ are previous and new position of Current particle

Step 6: Run load flow program to update fitness for the updated location every new iteration.

Step 7: search for the best value of fitness, if the new fitness better than the previous fitness set it as the global best fitness

Step 8: if the iteration reach the maximum iteration then stop, else return to step 2.[11]

5. Results and Discussions

To prove the effectiveness of the MO-PSO method, the bus voltage and losses for a standard IEEE 33-bus RDS and 65-bus Iraqi RDS have been calculated by using the Newton Rap son load flow program. Then, the proposed algorithm MO-PSO is used effectively to determine the optimal place and capacity of DG and D-STATCOM by MATLAB program. Three different cases have been considered for adding DG and D-STATCOM as presents below. The results have been compared with the results of the Bacterial Foraging Optimization Algorithm(BFOA)[29]

Case 1. System without DG and D-STATCOM.

Case 2. System with only DG.

Case 3. System with one DG and one D-STATCOM

5.1 IEEE 33-Bus System

An IEEE 33-bus radial distribution system is considered in this work. To demonstrate the effectiveness of the MO-PSO algorithm the total active and reactive load of the system is 3715 kW and 2300 kVar respectively. The base voltage of the system is 12.66kV with 100MVA as a base apparent power. The data of the system considered in this paper presented in [31].

The three different cases simulation results of the MO-PSO algorithm are present in Table 1. Firstly, the system simulated without DG and D-STATCOM as a base case and the result of active power losses, the minimum voltage and the minimum VSI were 210.77 kW, 0.66734p.u and 0.90383p.u, respectively as shown in Table 1.

In case2, the total active power loss mitigated to 112.9kW and the minimum VSI of the IEEE 33-bus radial distribution system improved to 0.7824p.u. In addition, to increase the minimum voltage to 0.9422 p.u. The above enhancement comes from the impact of adding one DG (Type one PV generator) with 2460 kW as an optimal capacity in 26th as an optimal place that determines by the proposed method. Obviously in case adding DG as a second case has a good impact on the performance of the system and better than other method as shown in Table1. Finally, in case3, three DG and one D-STATCOM are placed in the system at optimal places to minimize the active power losses and to improve the minimum voltage and minimum VSI of this system. The evaluated results have been illustrated in Table 1. It is clear, in the third case, the total active power loss has been minimized to 62.5 kW and the minimum VSI and minimum voltage are improved to 0.8537 p.u and 0.9612 respectively. However, the third case better than the first two cases, the MO-PSO gives a good minimization in losses and the voltage profile of the system and the minimum VSI is improved more than the other algorithms. A comparison of the voltage profile, stability voltage index and the total power losses for the three different cases are shown in Figure 5(a), 5(b) and 5(c) respectively

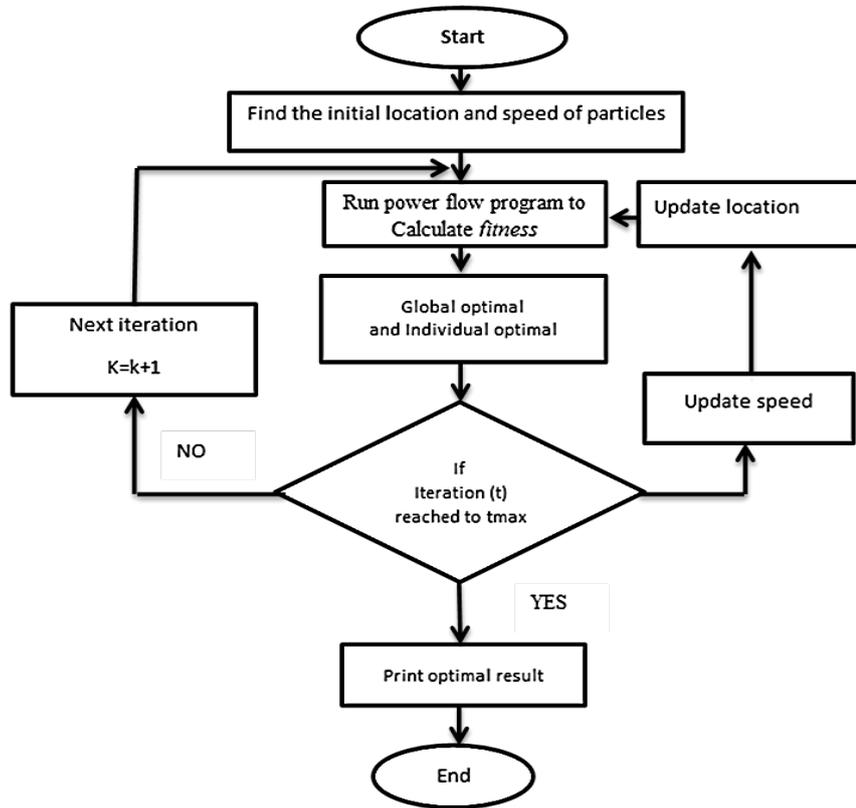


Figure 4: Flowchart of PSO Algorithm [30]

Table 1: The comparative results

	Variable	MOPSO	BFOA[29]
Case 1	P_{loss} (kW)	210.77	210.98
	VSI _{min} (p.u.)	0.66734	0.6610
	V_{min} (p.u.)	0.90383	
Case 2	Size in kw(location)	2460(26)	2200 (6)
	P_{loss} (kW)	112.90	113.14
	VSI _{min} (p.u.)	0.7824	0.7640
Case 3	V_{min} (p.u.)	0.9422	0.9368
	Size in kvar (location)	1180(30)	1094.6(30)
	Size in kW (location)	2880(7)	1239.8(10)
	P_{loss} (kW)	62.5	70.87
	VSI _{min} (p.u.)	0.8537	0.8465
	V_{min} (p.u.)	0.9612	0.9615

5.2 Numerical Results of Iraqi 65-Bus System

The radial distribution system is shown in Figure (6) is an Iraqi real 65-bus RDS considered in this paper as a second test system. The system is one feeder of Sadat Al-Hindiya district secondary power station which supply the Al-Zahraa neighborhood, one of the neighborhoods of Sadat Al-Hindiya district is located south of Al-Musayyib city in Babil Governorate, Iraq.

The system data present in Table 2 is identified after determining the length of line and location of buses by Geographic Position System (GPS) and plot the real system by Geographic Information System (GIS) [32] as shown in Figure (7) incorporate with the Iraqi ministry of electricity. The Iraqi system tested under three different cases and three different load factors with base voltage and base apparent power are 11kV and 100MVA respectively. The total active and reactive load of this RDS is 5669.1 kW and 3560.6 kVar respectively. In the first case before adding DG and DSTATCOM the active power losses, the minimum voltage and the minimum VSI were 446.2 kW, 0.8962p.u and 0.645p.u respectively for 1 load factor as illustrated in Table 3. In case2, the total active power loss mitigated to 125.9kW and the minimum VSI of Iraqi 65-bus radial distribution system is improved to 0.8333p.u .In addition, to increase the minimum voltage to 0.9555p.u. The above enhancement comes from the impact of adding one DG (Type one) with 4940 kW as an optimal capacity in 51th bus as an

optimal place that determine by the proposed method for 1 load factor. Obviously in the case of adding DG as a second case gives a good impact on the performance of the system as shown in Table 3.

In case3, both one D-STATCOM and three DG are installed at the optimal bus to minimize the power losses and to enhance the minimum VSI of the system. The obtained results are presented in Table 3.

The evaluated results have been illustrated in Table 3. It is clear, in the third case, the total active power loss has been minimized to 26.3kW and the minimum VSI and minimum voltage are improved to 0.9503p.u and 0.9873 respectively. However, the third case better than the first two cases, the MO-PSO gives a good minimization in losses and an improvement in voltage profiles of the system and in the minimum VSI in all three cases.

Remarkably, it is able noticed that as load factor increases the total losses increase for each three cases but the minimum voltage and VSI reduce at the same time. A comparison of the voltage profile, stability voltage index and the total power losses for the three different cases are shown in Figure 8(a), 8(b) and 8(c) respectively.

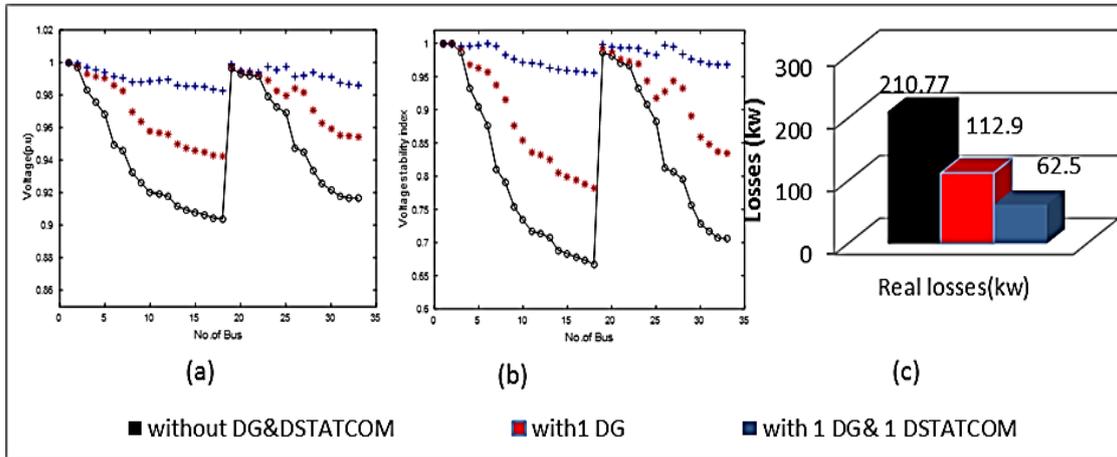


Figure 5: (a) voltage profiles comparison of 33-bus system for different cases (b) VSI comparison of 33-bus system for different cases and (c) power losses comparison of 33-bus system for different cases.

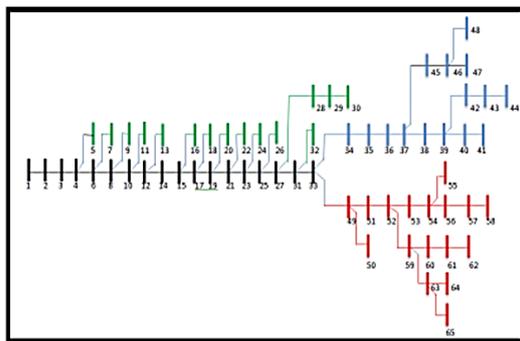


Figure 6: Iraqi real 65-bus configuration

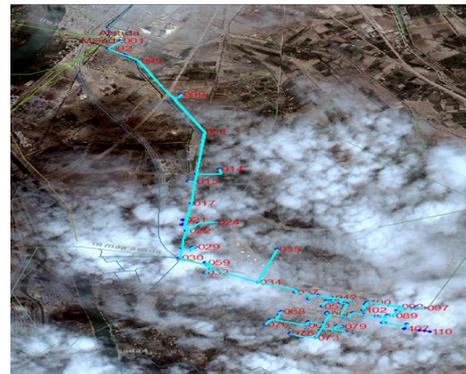


Figure 7: Data of Iraqi 65 bus system

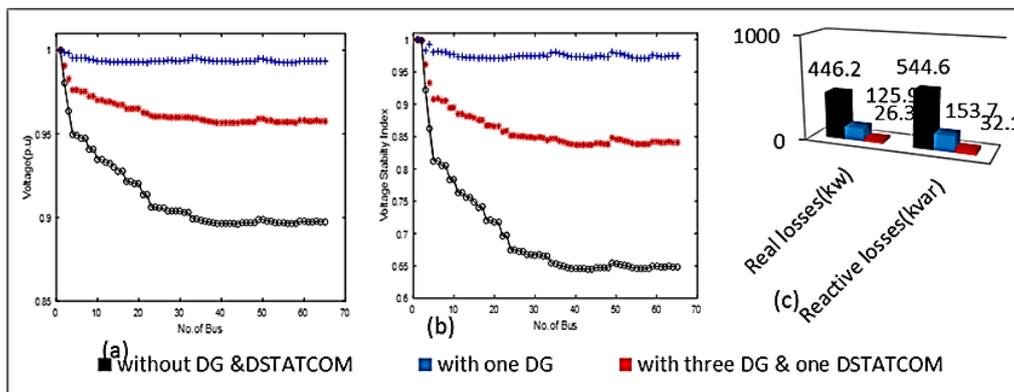


Figure 8: (a) Comparison of voltage profiles for different cases in Iraqi 65-bus system, (b) Comparison of VSI for different cases in Iraqi 65-bus system and (c) Comparison of line losses for different cases in Iraqi 65-bus system

Table 2: Data of Iraqi 65 bus system

	From	To	R(p.u)	X (p.u)	P_L (MW)	Q_L (MVA R)	From	To	R (p.u)	X (p.u)	P_L (MW)	Q_L (MVA R)
1	1	2	0.216363	0.264099	0.1063	0.0659	3	3	0.006175	0.007538	0.1700	0.1054
2	2	3	0.18478	0.225542	0.1063	0.0659	3	3	0.045125	0.055081	0.1063	0.0659
3	3	4	0.159363	0.194523	0.0	0.000	3	3	0.032063	0.039137	0.1063	0.0659
4	4	5	0.06318	0.077113	0.1700	0.1054	3	3	0.03086	0.037675	0.0	0.000
5	4	6	0.025650	0.031309	0	0	3	3	0.046550	0.056820	0.1063	0.0659
6	6	7	0.011400	0.013915	0.1063	0.0659	3	3	0.015200	0.018554	0.0	0.0
7	6	8	0.077663	0.094797	0.0	0.000	3	3	0.056763	0.069286	0.1700	0.1054
8	8	9	0.004750	0.005798	0.1063	0.0659	4	3	0.018763	0.022902	0.0	0.0
9	8	1	0.073625	0.089869	0.0	0.000	4	4	0.02111	0.025801	0.1063	0.0659
10	1	1	0.022325	0.027251	0.1063	0.0659	4	3	0.045600	0.055661	0.1700	0.1054
11	1	1	0.024938	0.03044	0.0	0.000	4	4	0.022088	0.026961	0.1063	0.0659
12	1	1	0.066025	0.080592	0.1700	0.1054	4	4	0.026363	0.032179	0.1700	0.1054
13	2	3	0.032300	0.039426	0.1700	0.1054	4	3	0.037525	0.045804	0.0	0.000
14	1	1	0.030875	0.037687	0.0	0.0	4	4	0.055813	0.068127	0.1063	0.0659
15	1	1	0.031588	0.038557	0.1700	0.1054	4	4	0.007600	0.009277	0.1063	0.0659
16	1	1	0.089538	0.109292	0.0	0.0	4	4	0.021375	0.026091	0.0	0.000
17	1	1	0.017100	0.020873	0.1063	0.0659	4	3	0.009975	0.012176	0.1063	0.0659
18	1	1	0.014725	0.017974	0.0	0.000	5	4	0.029688	0.036238	0.1700	0.1054
19	1	2	0.015675	0.019133	0.1063	0.0659	5	4	0.006413	0.007827	0.0	0.000
20	2	1	0.095238	0.11625	0.0	0.0	5	5	0.081225	0.099146	0.1700	0.1054
21	2	2	0.121838	0.148718	0.1700	0.1054	5	5	0.016150	0.019713	0.0	0.000
22	1	1	0.11302	0.137992	0.0	0.0	5	5	0.018525	0.022612	0.1700	0.1054
23	2	2	0.016350	0.020003	0.1700	0.1054	5	5	0.018725	0.022912	0.1700	0.1054
24	3	3	0.088				5	4	0.063	0.02	0.0	
25	2	2	0.011400	0.013915	0.0	0.0	5	5	0.002850	0.003479	0.1063	0.0659
26	4	3	0.001663	0.002029	0.1063	0.0659	5	5	0.01357	0.016538	0.1063	0.0659
27	5	5	0.027550	0.033628	0.0	0.0	5	5	0.01258	0.015365	0.0	0.000
28	2	2	0.008550	0.010436	0.1063	0.0659	5	5	0.00956	0.011596	0.1063	0.0659
29	7	7	0.011638	0.014205	0.1700	0.1054	6	5	0.05010	0.061169	0.1700	0.1054
30	8	8	0.020900	0.025511	0.1700	0.1054	6	6	0.026113	0.031869	0.1063	0.0659
31	9	9	0.015675	0.019133	0.0	0.0	1	1	0.022825	0.027889	0.0	0.000
32	0	7	0.021675	0.026381	0.1700	0.1054	2	9	0.021100	0.025830	0.1700	0.1054
33	1	1	0.069113	0.084361	0.0	0.0	3	3	0.024938	0.030401	0.1700	0.1054
34	3	3	0.069113	0.084361	0.0	0.0	6	6	0.024938	0.030439	0.1700	0.1054
35	2	1	0.069113	0.084361	0.0	0.0	4	3	0.024938	0.030439	0.1700	0.1054

Table 3: Numerical results of Iraqi 65-bus system

	Case1			Case2			Case3		
	0.7	1	1.2	0.7	1	1.2	0.7	1	1.2
Load factor	0.7	1	1.2	0.7	1	1.2	0.7	1	1.2
Size in kVAr (location)							1950(53)	2830(38)	2770(29)
Size in kW (location)				3450 (59)	4940 (51)	5520 (59)	900(11) 290(12) 2050(52)	20(48) 1390(30) 3000(38)	610(2) 3110(29) 2510(46)
Ploss (kW)	204.8	446.2	673.5	61.1	125.9	190.3	12.4	26.3	35.2
Qloss(kvar)	250	544.6	822	74.6	153.7	232.2	15.2	32.1	43
VSImin (p.u.)	0.7474	0.645	0.578	0.882	0.833	0.784	0.9519	0.9503	0.9141
Vmin (p.u.)	0.9298	0.8962	0.872	0.969	0.955	0.941	0.9878	0.9873	0.9778

6. CONCLUSION

In this paper, a multi object particle swarm algorithms (MO-PSO) has been proposed to enhance the system stability of smart Distribution Grids. The MO-PSO is employed to solve a multi-objective function including enhancement the average voltage and voltage stability and minimizing the total power loss by finding the optimal locations and sizes of DG and D-STATCOM in the power distribution system. Actually, simulation results demonstrated that the MO-PSO algorithm improves the average voltage and voltage stability and minimizing the total power loss of distribution networks when compared with other optimization algorithms under a different cases. Generally, it can be concluded that the MO-PSO can be simply used as an intelligent real-time tool with any large distribution system.

Nomenclatures

$AV(x)$	Average of buses voltage
c_2, c_1	Acceleration coefficient
$gbest^{t-1}$	Global best location
$I_{D-STATCOM}$	Injected current of D-STATCOM
I_L	Current pass between two buses
n	Total number of buses in the network
$pbest_i$	Partiel best location
$P_{R(R)}$	Real power of DG at bus 'R'
P_{TL}	Total Loss before insert device
$P_{R,min(R)}$	Minimum active power
$P_{R,max(R)}$	Maximum active power
$P_{loss}(S, R)$	Active losses of branch between buses R and S
$Q_{loss}(S, R)$	Reactive losses of branch betweenBus R and S
$Q_{DSTATCOM(R)}^{min}$	Minimum limit of compensated Power
$Q_{DSTATCOM(R)}^{max}$	Maximum limit of compensated Power
$R_{SR} + jX_{SR}$	Impedance of branch between buses R and S
$S_{total loss}$	Total power losses
t	Number of iterations
V_R	Voltage at receiving end bus
V_S	Voltage at receiving end bus
V_{Rnew}	Voltage at receiving end bus after Compensated
$V_{R,min}$	Minimum Voltage limits of bus R
$V_{R,max}$	Maximum $V_{R,max}$ Voltage limits of Bus R
VSI_R	Voltage stability index of node 'R'
$V_i(t)$	Velocities of the particles
$v_i(t + 1)$	Updated velocities of the particles

W	weight inertia
$x_i(t)$	Position of the particles
$x_i(t + 1)$	Updated position of the particles
θ_{new}	Phase angle between V_{Rnew} and V_S
δ	Phase angle of sending end voltage
α	Phase angle of Current pass between Two buses
β_1, β_2 and β_3	weighting factors

Author contribution

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Data availability statement

The data that support the findings of this study are available on request from the corresponding author.

Conflicts of interest

The authors declare that there is no conflict of interest.

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