Buildup factor calculation for high density poly ethylene, and high density poly ethylene with lead

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حساب عامل التراكم للبولي أيثيلين عالي الكثافة والبولي أيثيلين عالي الكثافة مع الرصاص محمد قاسم الفخار, حارث إبر اهيم ز هير سالم خميس قسم الفيزياء, كلية العلوم, جامعة و اسط المستخلص

دراسة عامل التراكم لعينات اسطوانية (دروع) من البولي أيثيلين علي الكثافة البولي أيثيلين عالي الكثافة مع الرصاص. حيث حسب عامل التراكم باستخدام اسماك من(0-3) معدل مسار حر ومصدر سيزوم- 137. (Lagore MeV) حيث استخدم الكاشف ألوميضي يوديد الصوديوم المطعم بالليثيوم ,NaI(TI) تظهر الحسابات هذه ان نتائج البولي أيثيلين عالي الكثافة مع الرصاص تعطي عامل تراكم اقل من ذلك للبولي أيثيلين كما الحسابات هذه ان نتائج البولي أيثيلين عالي الكثافة مع الرصاص مدر معدل مسار حر ومصدر الميزوم- 137. (Ev ومصدر معد معرف معام التراكم باستخدام اسماك من(0-3) معدل مسار حر ومصدر الميزوم- 137 (Ev ومحد الحكافي المعام الحمابات هذه ان نتائج البولي أيثيلين عالي الكثافة مع الرصاص تعطي عامل تراكم اقل من ذلك للبولي أيثيلين كما هو متوقع بسبب إضافة الرصاص. المعام ورعوا معام ورعوا معام التراكم ورعام ورعام التراكم ورعام ورعام ورعام المعام ورعوا معام المعام التراكم ورعام وروم ورعام وريام ورعام و

Abstract

The buildup factor of cylindrical samples (shields) for High Density Poly Ethylene, High Density Poly Ethylene with lead (HDPE+ Pb) was studied, where the buildup factor calculated using thickness between (0-3) m.f.p. Cs^{137} sources (E γ =0.662 MeV) have been used together with scintillation detector NaI(T ℓ) (2.5 x 2.5).These calculations show that the results of (HDPE +Pb) give buildup factor lower than that of (HDPE) as expected due to the addition of lead.

Key words: Buildup factor, gamma ray, shield, radiations.

1. Introduction

Shielding is the using of materials to lower the effects of incident radiation to any expectable level by reducing the intensity of radiation. Today the design and construction of radiation shielding used to protect people, equipment, and structures from the harmful effects of radiation of the most important problems innuclear engineering. Radiation shields required some facilities to determine and calculate x-ray radiation, gamma ray, and neutron. x-ray and gamma ray facilities for the detection of defects in materials, radiation facilities in food and plastics industries, The purpose of a radiationshieldisto protect from external radiation and in this context does not include the prevention of internal biological radiation hazards due to eating, drinking or breathing radioactive material (1). The buildup factor is defined as the ratio of the total photon beam(collided and un collided) response (e.g., flux, dose or exposure) to the response of the unclouded photon beam fraction. The gamma ray radioactive source have been used is¹³⁷Cs. The radioactive sources ¹³⁷Cs are considered to be point isotropic source because of their small dimension. As it will be evidently shown later, the effect of the solid angle in the present work is negligible, thus the source have been consider as point source. (2)

The shielding idea using a point source, narrow beam, and broad beam attenuations are used to explain "buildup factor" concept. Different values of buildup factors are presented and their behaviors in several materials are considered.

2. Theoretical concept

2.1 Gamma ray interaction with matter

Photons are classified according to their mode of origin, not to their energy. The term γ -ray is normally reserved for radiation emitted by nuclei, while the xray terms refer to radiation originating due to the transitions of atomic electrons andbremsstrahlung. There is, no fundamental difference between the two radiations.

There are number of processes which cancausey-raytobe scattered or absorbed (interact) by matter. However, only three processes are usually taken into account in nuclear physics or nuclear engineering problems. These processes are:

1. Photoelectric effect,

2. Compton effect (Compton scattering),

3.Pairproductionand inhala-tion. The photoelectric effect predomina-tes at low energies and high Z-value, pair production predominates at high energies and high Z-value. Whereas, the Compton effect is the main interaction at moderate energies ($\approx 1 \text{ MeV}$) for all Z and significant even at low energies for small Z. (3).

2.2 Types of buildup factors

The buildup factor may be expressed in terms of different quantities. These are the "number", the "energy" and the "dose" buildup factor and shown by the following equations (4).

The ''number'' buildup factor B _n =1+	$I=I_{e}e^{-\mu\times}$	(1.4)	
Scattered photon flux reaching the detect	OF it is important at this point to	discuss	
Unscattered photon flux	what is so called Narrow beam ge	eometry	
(1.1)	(NBG) and Broad beam geometry (
	BBG).		
The "energy" buildup factor:	The NBG, as shown in figure 1.	1, is the	
	geometry where only the und	collided	
$\mathbf{B}_{\mathbf{a}} = 1$	photons may reach the detector.	. While	
+	the BBG, as shown in figure 1. 2	2, is the	
Scattered energy flux reaching the det e	geometry where both the uncloud	ded and	
Unscattered energy flux reaching the det	some of the scattered photon	is may	
(1 2)	reach the detector (5). The "	buildup	
(1.2)	factor" is defined as the ratio	of the	
	actual gamma flux encountered	by the	
The dose bundup factor:	detector according to the ge	eometry	
D 1.	shown in figure 1.1 with	simple	
$B_{D}=1+$	exponential attenuation that for	llowing	
Absorbed dose from scattered photons	the geometry shown in figure 1	2 It is	
Absorbed dose from Unscattered photons	important to mention here th	hat the	
(1.3)	geometry represented in figure	1.5 will	
	not follow equation 1.7. This is b	ecause,	
The dose buildup factor is related to the	according to this equation,	each	
number buildup factor, in the following	scattered photon will be remove	ed from	
inner:	the path between the source a	and the	
Dose intensity = number flux \times	detector and never reach the d	etector.	
energy per number × absorption	Thus, there will be more gamm	na flux	
coefficient	encountered by the detector a	ind the	
	result of calculation will be	larger.	
2.3 Narrow Beam (NB) and	Therefore, equation 1.8 should b	be corr-	
Broad Beam (BB) geometries	ected to match the actual experi	m-ental	
	results as shown in the equation ((1.5).	

If each scattered photon will be removed from the path between the source and the detector, and never reach the detector, then applying equation(1.4) in suitable manner the experimental and theoretical results will be the same. But unfortunately some of the scattered photons will be scattered back toward the detector and recorded as un collided photons.

$$\mathbf{I}=\mathbf{B}\mathbf{I}_{o}\mathbf{e}^{-\mu\mathbf{x}} \tag{1.5}$$

where **B** is the buildup factor.



Figure (1.1): The narrow beam geometry (NBG) where only the un collided photons may reach the detector.



Figure (1.2): The broad beam geometry (BBG) where both the unclouded and some of the scattered photons may reach the detector.

3. Photon attenuation

The probability of a photon intera-cting in a particular way with a given material, per unit path length, is usually called 'linear attenuation coefficient' μ (cm⁻¹). This coefficient is of great importance in matters concerning radiation shielding.Consideringa point source of gamma rays separated from a detector by a dist-ance "X", with a material shield of thickness "x" and radius "r" located between them as shown in figure 1.3. (4). If the dimensions are such that :

X- x » 0 and x >> r (1.6)

Then every photon collision with the used material produces a scattered photon. Each one of these scattered photons will be removed from the path between the source and the detector, and never reaches the detector.



Figure (1.3): Point source of gamma rays separated from a detector by a distance "X", with a material shield of thickness "x" and radius "r".

The flux-level reduction rate is proportional to the flux-level itself. Mathematically,

$$-\frac{\mathrm{d}I}{\mathrm{d}x} = \mu I \tag{1.7}$$

or

$$\mathbf{I}=\mathbf{I}_{o} e^{-\mu \times}$$
(1.8)

where:

"Io" is the collimated flux in the direction of the detector.

" μ " is a coefficient representing the macroscopic probability density for a collision between the gamma photons

and an atom of the material at a depth "dx" (linear attenuation coefficient). The magnitude of the linear attenuation coefficient " μ " depends upon the energy of gamma and shielding material.

4. Experimental arrangement for buildup factor calculation

The top views of the experimental arrangements are shown in figures 1.4 and 1.5. Figure 1.4 shows the NB arrangement. However, figure 1.5 shows the BB arrangement (with detector shield). The radioactive source is well shielded with lead block from all sides. The NaI(Tl) detector is also well shielded with lead blocks from all sides except its front face to reduce the background radiation that may reach the crystal. The source, detector and the two collimators are arranged and aligned in a straight line on a wooden stage especially built for this experimental work. (6).



Figure (1.4): Top view of the narrow beam (NB) experimental arrangement.





5. Collimators

the NB In measurements. two collimators are used. Each collimator is a lead block of 5 cm radius and 8.4 cm width, with a central hole of 1.45 cm radius. The collimator near the radioactive source is usually used to obtain a narrow and collimated beam of gamma photons from a point source. While, the collimator near the detector is used to prevent scattered photons and allow those emitted straight forward by the radioactive source to reach the front face of the NaI(Tl) detector.

6. Method Buildup factor Calculation This method can be summarized as

For a narrow beam (with collimation):

I=I_°
$$e^{-\mu \times}$$

follows:

$$\therefore \frac{\mathbf{I}}{\mathbf{I}_{o}} = \boldsymbol{e}^{-\boldsymbol{\mu}\times} \quad \text{or} \quad \ln\left(\frac{\mathbf{I}}{\mathbf{I}_{o}}\right) = -\boldsymbol{\mu}\boldsymbol{x}$$
(1.9)

Because (**I** < **Io**) always, then, **ln**(**I** / **Io**) is a negative value and hence

- (ve) value = - μx or + (ve) value = μx (1.10)

Forabroad beam (without collimation)-

I=BI_o $e^{-\mu \times}$ ln(I / I_o)= ln B - μx (1.11)

Then, in the same manner:

+ (ve) value = x - ln B (1.12)

Atypical plotting **ln** (**I/Io**) as a function of **x** for the two cases (**NB** and **BB**) is shown in **figure 1.7**, from which, the buildup factor **B** at each thickness can be calculated (7,8).



Figure (1.7): ln(I/Io) as a function of absorber thickness x (mfp)

7. Experimental results and discussion:

7.1 Effects of lead addition to standard polymer

In order to determine the effects of lead additive to polymer, its attenuation coefficient and buildup factor are examined. of course, it is desired to increase the attenuation coefficient and decrease its buildup factor in order for it to be a suitable shielding material or at least make good optimization between them. For this reason the two different kinds of polymer [(High Density Poly Ethylene), and High Density Poly Ethylene withlead)],have been examined and compared witheachother. Figure 1.6 shows a comparison of attenuation coefficients for these different kinds of polymer. It is clear from this figure that the attenuation coefficients increase with using Pb additive



Figure (1.6): $ln(I/I_0)$ as a function of absorber thickness used to compare the attenuation coefficients for [(High Density Poly Ethylene)and(High Density Poly Ethylene with lead)] . for¹³⁷Cs gamma source, (E γ =0.662 MeV).



Figure (1.8): The experimental buildup factor curves for [(High Density Poly Ethylene)and(High Density Poly Eth-ylene with lead)]. for¹³⁷Cs gamma source, (E γ =0.662 Mev).

Tables and graphs of the experimental results to determine the buildup factor for each material.

Table (1.1): The experimental buildup factors for (High Density Polyethylene + lead) a using 137 Cs gamma source, E γ =0.662MeV.

Thickness	ln B	Buildup factor (B)	Previous Study
			(B)(9)
0.5	0.024	1.0249	1.02634
1	0.047	1.04812	1.05337
1.5	0.69	1.07143	1.08220
2	0.091	1.09526	1.11182
2.5	0.10	1.1162	1.1411
3	0.133	1.1422	1.1735

Table (1.2): The experimental buildup factors for (High Density Poly Ethylene) a using ¹³⁷Cs gamma source, $E\gamma$ =0.662MeV.

Thickness	ln B	Buildup factor (B)	Previous Study
			(B)(9)
0.5	0.032	1.0328	1.0376
1	0.062	1.0639	1.0757
1.5	0.092	1.0963	1.1151
2	0.124	1.1320	1.1583
2.5	0.144	1.1548	1.2008
3	0.189	1.2020	1.2460



Figure (1.9): $In(I/I_0)$ as function of absorber thickness(mfp) used determine the Buildup factor HDPE +Pb using ¹³⁷Cs gamma source (E_y=0.662MeV).



Figure (1.10): $\ln(I/I_0)$ as a function of absorber thickness x(mfp) used determine the Buildup factor HDPE using ¹³⁷Cs gamma source (E_y=0.662MeV).

References

1-Kaplan, M. F. (**1989**). Concrete radiation shielding,. Longman Group UK Limited.

2-Lamarsh,J. R. (1975). Introduction to nuclear engineering. Ddison-Wesley Co., N. Y.

3-ProfioA. (1979). Dadiation shielding and dosimerty,. John Wiley and Sons.

4-Glower, D. D. (1965). Experimental reactor analysis and radiation measurements. McGraw-Hill Book company.

5-Dresner, **L.** (1965). Principles of radiation protection engineering. McGraw-Hill Book company.

6-Hubbell ,J. H. (1982). Values of the absorption coefficients for different materials using Co-60 and Sc-137 gamma radioactive source. Appl. Radiat. Isot., 33(269).

7-Chilton , A. B. (1968). Broad beam attenuation sec.4.3 in Engineering compendium on radiation shielding. (Springer-Verlag,).

8-Chilton ,A. B. shultis, J. K. , and Faw, R. E. (1984). Principles of radiation shielding. Prentice-Hall, INC.

9-Ali ,A. I. (2009) . Fabricating and using some polymers as single and multi-layers (with other materials) nuclear gamma ray shield, Master Thesis, Omar Al- Mukhtar University.