### A New Compact Dual Band GPS Patch Antenna Design Based on Minkowski-Like Pre-Fractal Geometry

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#### **Abstract**

A low profile compact microstrip antenna for GPS (L1/L2) application has been presented in this paper. The proposed antenna design is based on the 3rd iteration Minkowski-like pre-fractal geometry. The resulting antenna design offers a compact size, low profile and light weight making it suitable for use in handheld applications. Antenna performance has been evaluated using the EMSightTM from the Applied Wave Research. The proposed antenna has shown to possess two resonance bands (for return loss  $\leq$ -10 dB) covering the two GPS bands. Reasonable radiation characteristics have been achieved at the GPS frequencies (L1:1575.42  $\pm$  10.23 MHz, L2:1227.60  $\pm$  10.23 MHz) with good circular polarization characteristics. Realized circular polarization Bandwidths (for axial ratio  $\leq$  3 dB) are found to cover adequately those required for these GPS bands.

**Keywords:** GPS (L1/L2), Fractal Antenna, Dual Band Antenna, Circular Polarization, Axial Ratio.

# تصميم جديد لهوائي شرائط دقيقة مدمج ثنائي الحزمة بالاعتماد على شكل منكوفسكي ما قبل الجزئى لمحدد الموقع العالمي

### الخلاصة

هوائي الشرائط الدقيقة صغير الواجهة للـ GPS في تطبيقات (L1/L2) قدم في هذا البحث. التصميم المقترح للهوائي يعتمد على التكرار الثالث لشكل منكوفسكي الجزئي. التصميم الناتج يعطي حجم صغير، واجهة صغيرة ووزن قليل مما يجعله ملائما للتطبيقات اليدوية. الهوائي المقترح أظهر أن لديه حزمتي رنين (لخسائر رجوع  $\leq$ -GB10) تغطي حزمتي الـ GPS. تم انجاز ميزات إشعاع معقولة في ترددي الـ GPS (L1:1575.42  $\pm$  10.23 MHz, L2:1227.60  $\pm$  10.23 MHz) مع ميزات استقطاب دائري جيدة. وجد أن حزمتي الاستقطاب الدائري المتحققة (لنسبة محورية  $\leq$  GB3) تغطى بشكل مناسب الحزم المطلوبة للـ GPS.

### Introduction

Microstrip antennas offer many advantages such as low profile, the ease of fabrication, and the low cost. These make them very popular and attractive for the designers since the early days they appear. In many cases, where the antenna size is considered an important limitation, their large physical size, make them

improper to be used in many applications. Several methods have been considered to reduce the microstrip antenna size [1-5]. These methods include the use of shorting posts [1], material loading and geometry

optimization [2]. Use of slots with different shapes in microstrip patch antennas had proved to be satisfactory in producing miniaturized elements [3, 4, 5].

As a result, microstrip antennas are extensively used in the global positioning system (GPS). GPS antennas operating at L1 and L2 bands have been realized using two stacked patches and a small air-gap between the substrates with aperture-coupled multiple patch antennas fed through feed divider network [6,7]. Due to their promising application in microwave circuit and antenna design, much of

research work had been devoted to the use of periodic structures [8-10]. These periodic structures include the photonic crystals, electromagnetic bandgap (EBG) structures or metamaterials. The EBG structures have been applied to antennas with various polarizations to improve antenna gain

### II. The 3<sup>rd</sup> Minkowski-Like Pre-Fractal Antenna

and radiation patterns. Recently more research works have been devoted to make use of the space-filling and self similarity properties of some fractal objects to produce miniaturized multiband antenna elements [11, 12].

Dual band GPS antennas had been also achieved using two elliptical annular patches that are concentrically printed on two stacked substrates separated by an airgap. A central conducting wall shorts the two patches to the ground plane. The sizes of the patches have been chosen to make the upper and bottom patches resonating on the L1 and L2 frequencies [13,14].

In this paper, a compact multiband microstrip antenna based on 3<sup>rd</sup> iteration Minkowski-like pre-fractal structure has been designed and the antenna performance of many structures has been computed using a full-wave numerical method of moment (MoM). The proposed structures have been applied in dual-frequency GPS antennas at L2:1.2276 GHz and L1:1.57542 GHz.

Fractal geometry defines a structure with long lengths that fit in a compact area. Due to the

iterative generating process, the multiple scales of the recurring geometry resonate at different frequency bands. The iterative generation procedure of a Minkowski-like pre-fractal up to the 3<sup>rd</sup> iteration is demonstrated in Fig.1.

The dimension of a fractal provides a description of how much a space it fills. A dimension contains much information

about the geometrical properties of a fractal. The generator used to develop the proposed Minkowski-like pre-fractal structure (Fig.1a) involves similarity transformations of more than one ratio;  $a_1$  and  $a_2$ , and thus its dimension can be obtained from the solution of the following equation [13]:

$$2(\frac{1}{2}(1-a_1))^D + 2a_2^D + a_1^D = 1$$
 (1)

where D, represents the fractal dimension,  $a_1$  is the ratio  $W_1/L_0$ , and  $a_2$  is the ratio  $W_2/L_0$ . The perimeter,  $P_n$ , of the n<sup>th</sup> iteration MLPF antenna is then calculated using [15]:

$$P_n = (1 + 2a_2)P_{n-1} (2)$$

In this paper, many  $3^{rd}$  iteration MLPF antenna structures, corresponding to different values of  $a_1$ , had been designed and modeled at the design frequency of the GPS (L2:1.2276 GHz).

## III. The Antenna Design and simulation

The geometry of the 3<sup>rd</sup> iteration MLPF microstrip antenna is shown in Fig.1*e*. It has been depicted with enlarged scale to show the smallest details. The proposed antenna design has been computed using an FR4 substrate with relative dielectric constant of 4.4 and a substrate height of 1.6 mm. The design frequency is the GPS L2:1227.60 MHz, since the multiresonance behavior of the MLPF antenna implies that the lowest resonance frequency takes place at the design frequency [15, 16].

The dimensions of the traditional half-wavelength patch antenna, (Fig.1*b*), have been calculated at the design frequency using the prescribed substrate parameters. The perimeter,  $P_{o}$ , of this patch is found to be of about 228 mm. The corresponding perimeter,  $P_{3}$ , of the 3<sup>rd</sup> iteration MLPF

antenna is then calculated using Equ.2. This results in an MLPF patch length of 26.3 mm.

The resulting dimension of the 3<sup>rd</sup> iteration MLPF microstrip antenna corresponds to a reduction in size of about 78% compared with the conventional microstrip antenna operating at the same frequency and using the same substrate.

The middle segment width ratio of the generator structure, (Fig.1a), has been adjusted to many different values. Best results had been obtained for a value of  $a_1$  = 0.2. The resulting antenna element has been excited with a two-port configuration having the same amplitude but in phase quadrature to enhance producing of circular polarization required for the GPS operation.

### **IV. Simulation Results**

Theoretical performance of each of the proposed antenna structure has been predicted using a full-wave numerical method of moment (MoM). EMSight<sup>TM</sup>, of the Applied Wave Research, includes a full-wave electromagnetic solver that uses a modified spectral-domain method of moments to accurately determine the multi-port scattering parameters for planar structures [17].

Fig.2 shows the computed return loss for the modeled antennas. It is clear that the simulated results show that two resonance bands exist: the first band is from 1.16 GHz to 1.26 GHz, and the second band is from 1.28 GHz to 1.71 GHz. The two bands include the GPS L1 band and L2 band frequencies.

Figs.3 and 4 show the E field radiation patterns for RHCP and LHCP at the GPS frequencies L2:1.2276 GHz and L1:1.57542 GHz. Respectively.

### V. Conclusion

A new 3<sup>rd</sup> iteration Minkowski-like pre-fractal dual band GPS patch antenna structure is presented, which possesses a compact size and low profile. The proposed low-profile dual-frequency GPS

antenna has good radiation patterns GPS L1 and L2 bands. The presented antenna offers a reduction percentage in size of 78% as compared with conventional rectangular Microstrip patch antenna designed at the same frequency and using substrate with similar parameters. Additional work has to be performed applying the same design idea for other dual-band communication systems.

#### References

- [1].G. Kumar and K. P. Ray, "Broadband Microstrip Antennas," *Artech House, Inc.*, 2003.
- [2]. A. K. Shrivervik, J. F. Zurcher, O. Staub and J. R. Mosig, "PCS Antenna Design: The Challenge of Miniaturization," *IEEE Antennas and Propagation Magazine*, vol. 43, pp. 12-27, Aug. 2001.
- [3]. G. Kosiavas, et al, "The C-Patch: A Small Microstrip Antenna Element," *Electronic Letters.*, vol. 25, pp. 253-254, 1989.
- [4]. V. Palaniswamy, and R. Crag, "Rectangular Ring and H-Shape Microstrip Antenna; Alternative Approach to Rectangular Microstrip Antenna," *Electronic Letters*, vol. 21, pp. 874-876, 1985.
- [5] W. S. Chen, "A Novel Broadband Design of a Printed Rectangular Slot Antenna for Wireless Applications," *Microwave Journal*, Vol. 49 No.1, Jan. 2006.
- [6]. D. M. Pozar and Sean M.Duffy "A Dual-Band Circularly Polarized Aperture-Coupled Stacked Microstrip Antenna for Global Positioning Satellite," *IEEE Transactions Antennas and Propagat.*, Vol. 45, No.11, pp. 1618-1625, Nov. 1997.
- [7]. Chih-Ming Su, and Kin-Lu Wong, "A dual GPS Microstrip Antenna," *Microwave and Optical Technology Letters*, Vol.33, No.4, pp.238-240. May 2002.

- [8]. J.S.Row, "Dual-frequency Circularly Polarized Annular-ring Microstrip Antenna," *Electronics Letters*, Vol. 40 No.3, pp.153-154, 2004.
- [9]. F. Yang, Y. Qian, and T. Itoh, "Low-Profile Cavity-Backed Slot Antenna Using UC-PBG Substrate," *IEEE AP-S*, Vol.1, pp.1796-1799, 2000.
- [10]. X. L. Bao and M. J. Ammann, "Dual-band GPS Patch Antenna based on Dual-band Fractal EBG Technique," *LAPC*, *Loughborough University*, pp.53-56, 11-12th April, 2006.
- [11]. S. E. El-Khamy, "New Trends in Wireless Multimedia Communications Based on Chaos and Fractals," 21<sup>st</sup> National Radio Science Conference (NRSC2004), pp. INV1 1 -25, 16-18 March 2004.
- [12]. N. Cohen, "Fractal's New Era in Military Antennas," *Journal of RF Design*, pp. 12-17, April 2005.
- [13]. L. Boccia, G. Amendola, G. Di Massa, "A Dual Frequency Microstrip Patch Antenna for High-Precision GPS Applications," *IEEE* Antennas and Wireless Propagation Letters, Vol. 3, pp.157-160, 2004.
- [14]. G. Amendola, L. Boccia, G. Di Massa, "Shorted Elliptical Patch Antennas with Reduced Surface Waves on Two Frequency Bands," *IEEE Transactions on Antennas and Propagation*, Vol. 53, No. 6, June 2005.
- [15]. J. K. Ali, "A New Reduced Size Multiband Patch Antenna Structure Based on Minkowski Pre-Fractal Geometry," *Journal of Engineering* and Applied Sciences, JEAS, Vol. 2, No. 7, pp. 1120-1124, 2007.
- [16]. J. K. Ali, and Ali S.A. Jalal "A Miniaturized Multiband Minkowski-Like Pre-Fractal Patch Antenna for GPS and 3G IMT-2000 Handsets," Asian Journal of Information

- *Technology* ,*AJIT*, Vol. 6, No. 5, pp.584-588, 2007.
- [17].Microwave Office and EMSight, Applied Wave Research, El Segundo, CA 2000

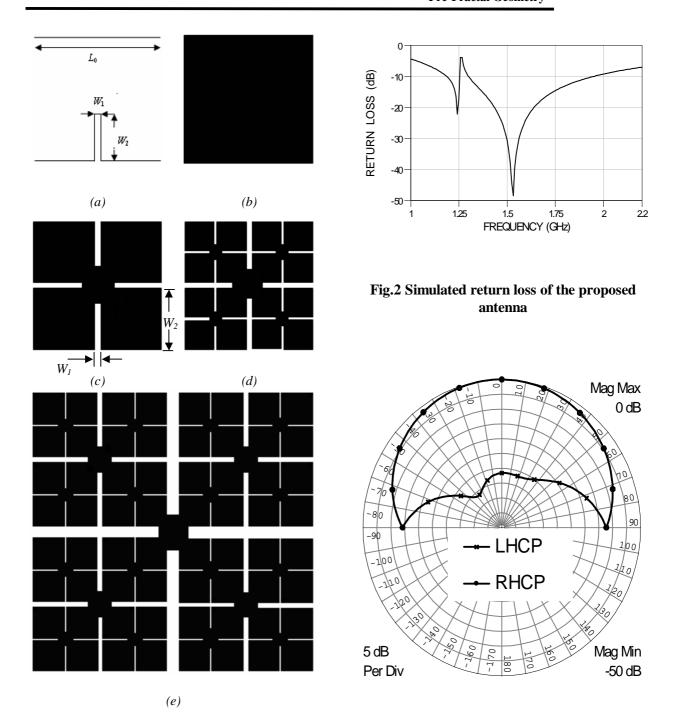


Fig.1 The iterative generation procedure of a Minkowski-like pre-fractal (MLPF); (a). The generator, (b). Square patch microstrip antenna, (the initiator), (c). The  $1^{\rm st}$  iteration (d). The  $2^{\rm nd}$  iteration and, (e).Enlarged scale of the proposed  $3^{\rm rd}$  iteration MLPF structure.

Fig.3 The RHCP and LHCP radiation patterns of the proposed antenna at 1.22760 GHz.

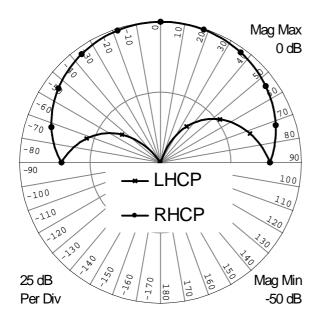


Fig.4 The RHCP and LHCP radiation patterns of the proposed antenna at 1.57542 GHz.