



A Proposed Approach to Relay-Base Station Link Design for 5G Radio Access Network

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HIGHLIGHTS

- The Innovative Relay-Based 5G RAN design establishes DWDM-RoF relay-assisted architecture to build stable and scalable 5G Radio Access Network (RAN) deployment.
- The fiber-connected relay mesh topology provides stable bidirectional communication through high SNR and OSNR values exceeding 50 dB.
- The network performance benefits from DWDM-RoF through efficient wavelength reuse and strong channel isolation which makes it a reliable alternative to conventional 5G RAN designs.

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ABSTRACT

The fast expansion of 5G technology requires new innovative approaches to resolve challenges with extensive signal degradation and constrained coverage extent as well as interference in high-frequency bands. The proposed research designs a 5G Radio Access Network (RAN) station link using relay stations that combine Dense Wavelength Division Multiplexing (DWDM) and Radio-over-Fiber (RoF) technological frameworks. The proposed system uses a mesh architectural network with 32 fiber-connected relay stations to enable efficient, scalable data transfer as an alternative to conventional star configurations. An OptiSystem simulation demonstrates that signal integrity enhancement occurs through the establishment of a bidirectional transmission medium that combines Erbium-Doped Fiber Amplifiers (EDFAs) with high-stability Continuous Wave (CW) lasers. The communication functions between uplink and downlink depend on Wavelength Division Multiplexing (WDM) multiplexers and demultiplexers to operate smoothly. The design delivers remarkable Signal-to-Noise Ratio (SNR) and Optical Signal-to-Noise Ratio (OSNR) measurements greater than 50 dB, which ensures quality signals transmit with low degradation to demonstrate stable and bidirectional communication. The system optimizes wavelength reuse while ensuring channel isolation and achieves optimum bandwidth utilization, which makes it a potential choice for future mobile networks. The research findings prove that DWDM-RoF is an effective solution to tackle critical 5G network needs through efficient, high-speed, accurate networks, which opens new paths for relay-assisted 5G development while stabilizing networks across different geographic locations.

I. INTRODUCTION

The rapid advancement of technologies like virtual reality (VR), Industry 4.0, the Internet of Everything (IoE), and 8K video streaming is bringing society closer to full connectivity. So that causes telecommunications networks to experience a massive surge in data traffic. Global mobile data consumption is expected to exceed 5,036 exabytes per month, in parallel with increasing data usage from 5GB per month in 2020 to more than 250GB per month. Experts and industry pioneers are working to innovate next-generation mobile communication technologies to meet this unmatched demand. The optimal solution lies in deploying 5G networks that are designed to connect society through three essential applications: massive machine-type communications (mMTC), enhanced mobile broadband (eMBB), and ultra-reliable low-latency communications (URLLC). As a fundamental component, eMBB plays a critical role by ensuring faster data speeds and greater network capacity to handle growing traffic loads[1].

The effectiveness of 5G fundamentally relies on enhancements in Radio Access Network (RAN) design, which play a key role in managing escalating data traffic and fulfilling the requirements of present applications [2]. Cloud Radio Access Network (C-RAN) technology is a significant advancement in 5G RAN. It consolidates baseband tasks into Baseband Unit (BBU) pools or Central Units (CUs). This streamlined method cuts down on costs, makes the best use of resources, and effectively manages a large number of remote Radio Heads (RRHs) or Radio Units (RUs), offering a solution that can grow with the needs of 5G networks [3]. Relay systems play a vital role in enhancing coverage and signal quality, especially in hard-to-reach areas like urban canyons and rural zones [4]. With the advancement in 3GPP standards, fixed and mobile relays—such as IAB (release 16), conventional repeaters (release 17), and smart repeaters (release 18) hold substantial benefits for boosting 5G network performance [5], [6], [7], [8]. This study introduces an innovative relay-based station link concept for 5G Radio Access Networks, using fiber optic connections between relays. This approach uses a wired mesh topology, including Dense Wavelength Division Multiplexing (DWDM) and Radio-over-Fiber (RoF) technologies, deviating from conventional star topologies. The proposed architecture enhances flexibility, scalability, and network performance while ensuring high Signal-to-Noise Ratio (SNR) and Optical Signal-to-Noise Ratio (OSNR) for dependable communication. Difficulties like coverage restrictions and resource allocation in relay-based RAN topologies are highlighted in this study, establishing a basis for adaptive and efficient 5G communication systems that accommodate future applications.

The organization of this paper is presented as follows: Section II literature review related to the work. Section III describes the system-based methodologies employed. Section IV explains the proposed DWDM-RoF relay-base station system. Section V gives a detailed discussion of the results and a complete analysis. Section VI provides a conclusion with key findings and recommendations for future research. Finally, documents the references consulted in this study.

II. RELATED WORK

Recently, a renewed focus has been placed on relaying technology as a fundamental pillar block for the future evolution of 5G RAN. In [9], it is highlighted that UAV-based relays contribute to improving throughput by optimizing trajectory as well as power allocation in dynamic wireless networks. Another investigation [10] focused solely on RIS-assisted relay mesh networks, noting throughput gains in densely deployed urban canyons by reducing routing interference; the report also

did not examine hybrid fiber-wireless systems or latency gains. Additionally, reinforcement learning has been used to optimize relay selection in wireless sensor networks under an impulsive noise model [11]; yet, no efforts have been made to utilize it in fiber-based systems.

A follow-up study assessed wireless relay configurations in 5G networks [12], revealing improvements in capacity and latency; however, the challenges of integrating these systems with fiber optic connections remain unexamined. A Network Digital Twin framework [13] was implemented for the virtual optimization of relay systems, emphasizing wireless situations without consideration of fiber integration. Standardization initiatives [14] incorporated wireless relays with 3GPP standards, while network-controlled repeaters [15] effectively enhanced coverage and capacity; likewise, hybrid relay technologies that integrate fiber and wireless components were not considered. Research on user equipment relaying [16] explored post-5G but maintained a focus persisted on wireless relays.

Hybrid relay systems, which integrate fiber and wireless technology, have garnered little attention. A review on relay-assisted optical wireless communications [17] emphasized the benefits of hybrid designs for low latency and higher reliability. Although Cooperative relaying in Rayleigh fading channels [18] demonstrated promise for 5G networks in urban regions. Nevertheless, the key aspects, such as enhancing Service quality and smooth transitions in hybrid relaying situations remain unexplored.

III. SYSTEM BASED METHODOLOGY

A. Optical Fiber Communication System

RoF is a system that works by integrating fiber optic networks for transmitting radio frequency (RF) signals from a central hub to distant antenna units. This technology combines optical and microwave systems to provide a dependable solution that enhances network capabilities and mobility features at cost-effective rates [19]. As shown In *Fig. 1*, the RoF system requires three essential elements that perform unique functions, starting with the central station (CS) and continuing with the optical fiber network and finishing with the base station (BS). The central station acts as the transmitter, monitoring signal formation and modulation; the base station operates as the receiver, receiving and processing signals from the fiber optic network. The data source working with the laser operates at the CS as a transmitter to transform electrical signals into optical signals. The base station collects signals through fiber optic transmission. The fiber optic network employs remote nodes to enhance and disseminate

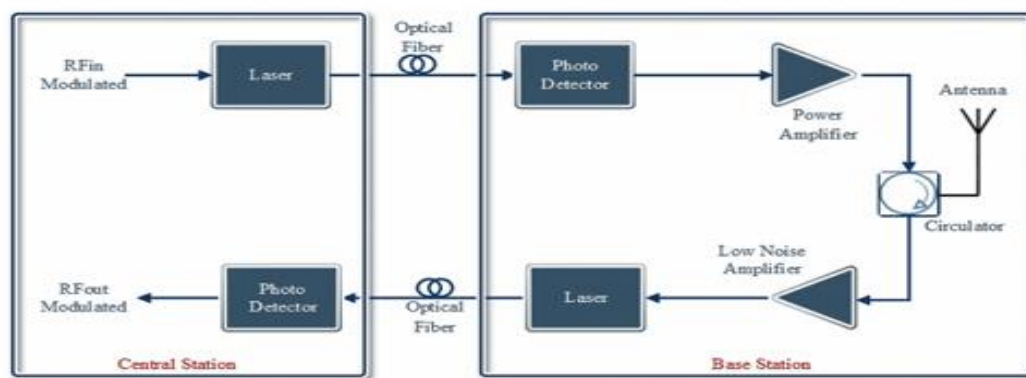


FIG. 1. GENERAL STRUCTURE OF FIBER OPTIC COMMUNICATION SYSTEM [19].

At the base station, a compact antenna device, commonly known as a remote antenna, converts the optical signal back into an electrical signal for the end user. Through the base station, radio signals received from end users get converted into optical signals before transmission to the central station through the fiber optic network [19].

B. Wavelength Division Multiplexing

The 5G networking element WDM plays a vital role by combining optical signals through separate wavelengths for extended data transmission. The signals reach separate channels upon reception which results in substantial capacity growth for the system. DWDM emerges as the most efficient WDM technology because it enables increased transmission capacity together with extended distances and extensive wavelength spectrum use.

The combination of RoF technologies with DWDM in 5G communication networks enables faster data rates and improved bandwidth performance, which establishes them as the optimal solution for next-generation networks [20]. *Fig. 2*, illustrates the fundamental concept of WDM technology, showing its ability to manage several signals simultaneously.

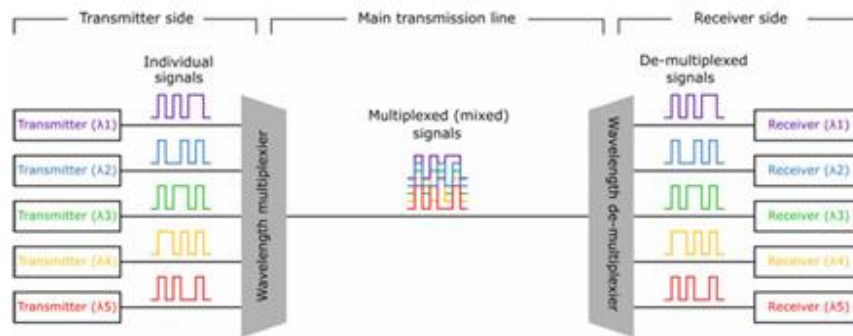


FIG. 2. WDM-BASED TECHNOLOGY BASIC DIAGRAM [20].

IV. PROPOSED DWDM-RoF RELAY-BASE STATION SYSTEM

The system design employs 32 channels of 32 relay stations connected through WDM fiber optics to 32 remote stations at the receiving end, as shown in *Fig. 3*, for 7 relays. The proposed configuration was simulated using OptiSystem software V22, a well-established tool renowned for its efficacy in designing, testing, and modelling diverse fiber optic systems. The software system delivers precise performance evaluation capabilities for system testing under various circumstances. *Fig. 4* displays the 32-channel DWDM system, demonstrating the relay-based fiber link architecture. This design

facilitates seamless communication between relay stations and distant stations, leveraging the efficacy of WDM technology for fast and low-loss data transmission over several channels.

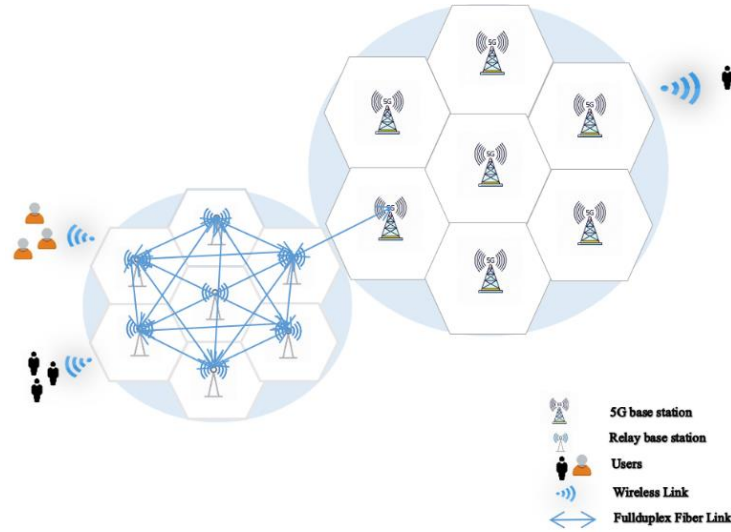


FIG. 3. RELAY BASE STATION SCENARIO.

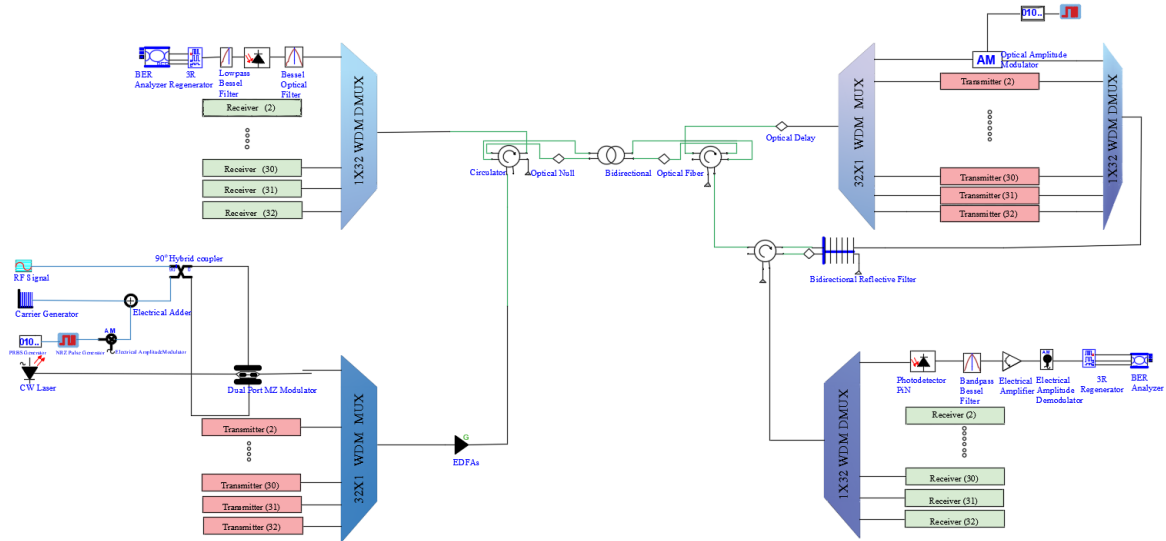


FIG. 4. SYSTEM DESIGN BLOCK DIAGRAM.

A. Transmitter Part

The system integrates electrical and optical components to facilitate efficient digital data transfer via an optical fiber link, which consists of 32 channels. Every wavelength-operated channel connects to an associated relay device. The initial channel operates at 193.1 THz with a 1 MHz linewidth, but other channels maintain a 0.8 nm separation for low-loss transmission and higher user density and increased data rates. Each channel sustains an input power of 6 dBm. The baseband signal emerges through non-return-to-zero (NRZ) pulses, which result from processing binary data by a pseudo-random bit generator. An electrical adder subsequently combines the signal with a carrier signal from a carrier

generator, and an electrical amplitude modulator (AM) operating at a frequency of 3.5 GHz adjusts the signal amplitude according to the input data.

The modulated signal is fed into a Continuous Wave (CW) laser to generate an optical carrier wave. A 90° hybrid coupler applies a phase shift, enabling subcarrier multiplexing. The output proceeds to a dual-port lithium niobate (LiNbO₂) Mach-Zehnder modulator (MZM) for additional processing that transforms electrical signals into optical signals. A WDM multiplexer with an 80 GHz bandwidth integrates the optical signals from all 32 channels into a unified transmission. This setup facilitates rapid, high-density, and low-loss communication across the optical fiber link, as shown in Fig. 5 below.

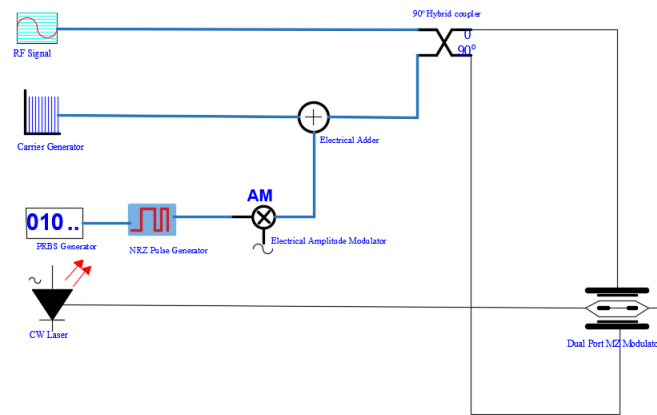


FIG. 5. INTERNAL STRUCTURE OF TRANSMITTER.

B. Transmission Medium Part

Erbium-Doped Fiber Amplifiers (EDFAs), as essential components of optical communication systems, enhance signal strength across multiple channels simultaneously, function to amplify signals effectively within the 1550 nm wavelength range, optimal for optical signal amplification, and also optical interference of the system between downlink and uplink signals minimized by utilizing a bidirectional circulator, ensuring smooth and continuous data transmission. Furthermore, the signal transmission reliability and system performance can be improved by using a 1-kilometer-long optical fiber to simulate relay distances allows for dependable and continuous signal transmission, enhancing the system's resilience and efficiency as shown in Fig. 6 below.

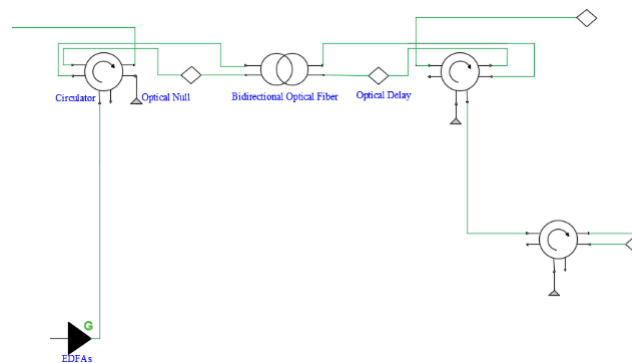


FIG. 6. FIBER LINK WITH MEDIUM COMPONENTS.

TABLE I. THE EDFAs SELECTED PARAMETERS.

EDFAs Parameters	Parameter Value
Gain	20 dB
Noise Figure	4 dB
Operation Mode	Power control
Power	15 dBm
Saturation Power	10 dBm
Include Noise	Yes

TABLE II. THE FIBER LINK PARAMETERS.

Bidirectional Optical Fiber Parameters	Parameter Value
Length	1km
Reference Wavelength	1550nm
Dispersion	17 Ps/nm/km
Dispersion Slop	0.07 Ps/nm ² /km

C. Reseiver Part

The WDM demultiplexer equipped with 80 GHz bandwidth splits the received signal before it directs the data to receivers at the endpoint. The bidirectional reflective filter functions as the main component of this operation by letting some signal pass through as it reflects the rest of the data-carrying signal for continued demodulation. The PIN photodiode converts the reflected signal which moves through a band-pass filter before the signal reaches the signal analyzer at downlink.

The portion of the signal sent via the bidirectional reflective filter is re-modulated by an amplitude modulator driven by a 20 Gbps baseband signal. A WDM MUX with an 80 GHz bandwidth merges the modulated signals from all channels and is retransmitted as an uplink signal to the transmitter side. At the transmitter, a WDM de-multiplexer with a bandwidth of approximately 80 GHz demultiplexes the uplink signal, and then the demultiplexed signal is subsequently converted to electrical signal using a PIN photodiode and refined through a Bessel filter for conclusive analysis, as shown in Fig. 7 below and indicated in Table III.

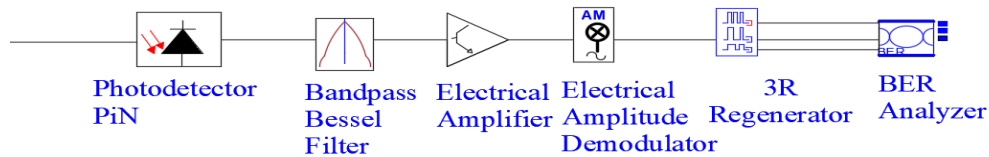


FIG. 7. SYSTEM DOWNLINK RECEIVER PART.

TABLE III. RECEIVER PART PARAMETERS VALUE FOR BOTH UPLINK AND DOWNLINK.

Downlink Receiver		Uplink Receiver	
Photodetector	values	Bandpass Bessel filter	values
Responsivity	1A/W	Frequency*	193.1 THz
Dark current	10nA	Bandwidth	12 GHz
Bandpass Bessel filter	values	Photodetector	values
Frequency	3.5 GHz	Responsivity	1A/W
Bandwidth	1 GHz	Dark current	10nA
Electrical amplifier	value	Lowpass Bessel filter	value
Gain	20dB	Cut off frequency	0.72*Bit rate
AM demodulator	values	3R Regenerator	value
Frequency	3.5GHz	Reference Bit rate	20Gbps
Cut off frequency	0.72*Bit rate		

* This frequency changes according to each channel.

V. RESULTS AND DISCUSSION

Table IV outlines the wavelengths assigned to each of the 32 WDM channels, ranging from 193.1 THz to 196.2 THz. Each channel is allocated a distinct frequency.

TABLE IV. THE UTILIZED WAVELENGTHS.

Channel Number	Wavelength	Channel Number	Wavelength
Ch 1	193.1 THz	Ch 17	194.7 THz
Ch 2	193.2 THz	Ch 18	194.8 THz
Ch 3	193.3 THz	Ch 19	194.9 THz
Ch 4	193.4 THz	Ch 20	195.0 THz
Ch 5	193.5 THz	Ch 21	195.1 THz
Ch 6	193.6 THz	Ch 22	195.2 THz
Ch 7	193.7 THz	Ch 23	195.3 THz
Ch 8	193.8 THz	Ch 24	195.4 THz
Ch 9	193.9 THz	Ch 25	195.5 THz
Ch 10	194.0 THz	Ch 26	195.6 THz
Ch 11	194.1 THz	Ch 27	195.7 THz
Ch 12	194.2THz	Ch 28	195.8 THz
Ch 13	194.3 THz	Ch 29	195.9 THz
Ch 14	194.4 THz	Ch 30	196.0 THz
Ch 15	194.5 THz	Ch 31	196.1 THz
Ch 16	194.6 THz	Ch 32	196.2 THz

The RF signal generated by the sine wave generator, as demonstrated in *Fig. 8 (A)*, features a pure single-frequency spectrum, offering exceptional spectral clarity that ensures minimal disruption and facilitates effective subcarrier modulation. The hybrid coupler applies a 90° phase shift, producing orthogonal signals necessary for subcarrier multiplexing, as illustrated in *Fig. 8 (B)*. Amplitude variations indicate strengthened modulation.

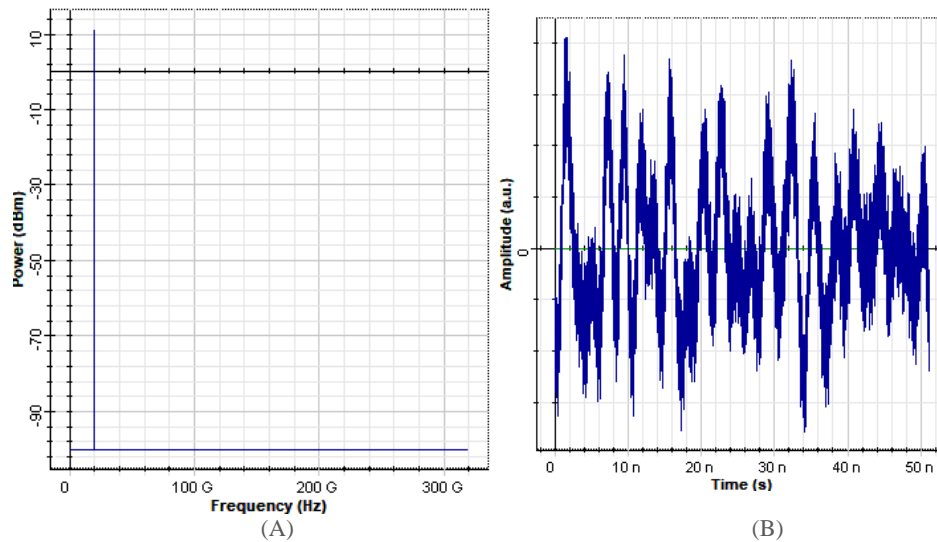


FIG. 8. (A) RADIO FREQUENCY SIGNAL, (B) RADIO FREQUENCY AFTER 90-DEGREE PHASE SHIFT.

Fig. 9 (A) ,illustrates the binary signal from the NRZ pulse generator, preserving data integrity, and then, as shown in Fig. 9 (B), the NRZ data integrates with a carrier signal of amplitude modulation, ensuring compatibility for optical conversion and reliable transmission.

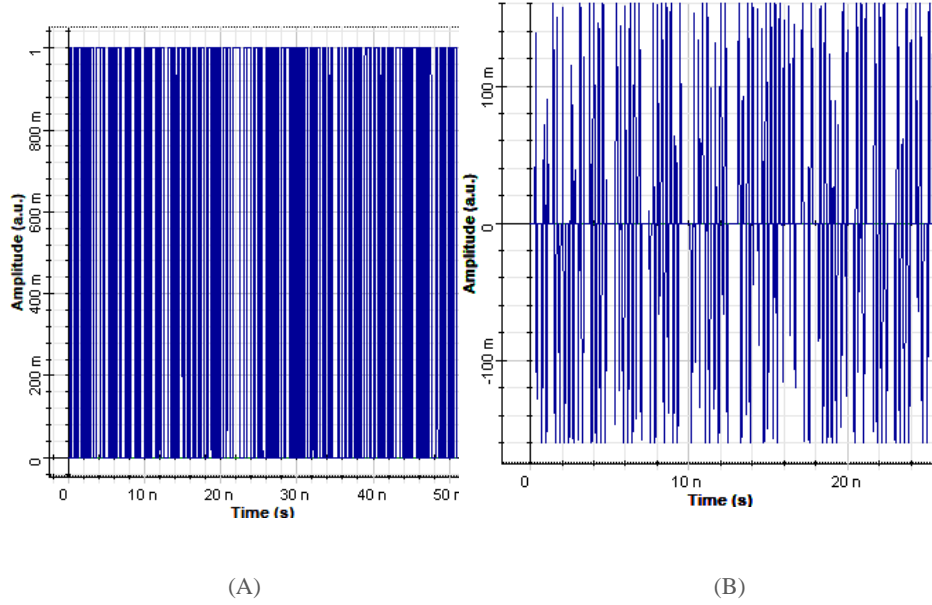


FIG. 9. (A) DIGITAL DATA, (B) MODULATED SIGNAL AFTER AM MODULATOR.

The carrier generator produces a stable sinusoidal signal for modulation, which is combined with an NRZ-AM modulated signal by an electrical adder. A composite waveform is formed that encodes binary information. As the signal moves through the 0° coupler, the phase and amplitude remain as is, ensuring it is ready for further modulation and transmission, as demonstrated in Fig. 10. The CW laser's output spectrum, depicted in Fig. 11, shows a sharp peak at 193.1 THz, indicating stable and precise optical carrier generation. The stability level is crucial for accurate modulation and reliable signal transmission within optical networks.

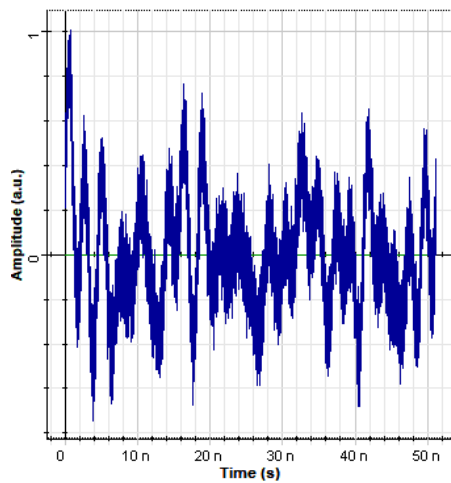


FIG. 10. CARRIER GENERATOR AFTER 0-DEGREE COUPLER.

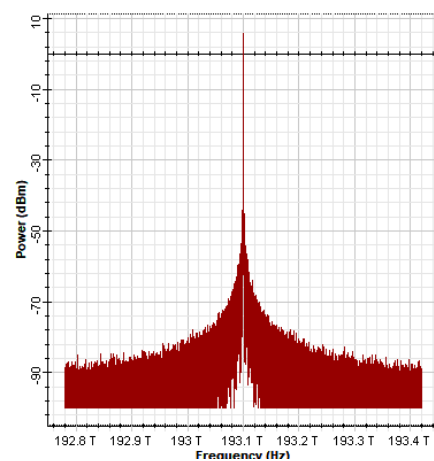


FIG. 11. CW LASER SPECTRUM.

Fig. 12 shows MZM outputs in a system of 32 channels, which present only for four channels: 193.1 THz, 194 THz, 195 THz, and 196 THz, respectively, that exhibit distinct peaks, signifying stable and robust optical carriers. Well-balanced power distribution and low noise of the system emphasize optimal maintenance of excellent signal integrity and less distortion.

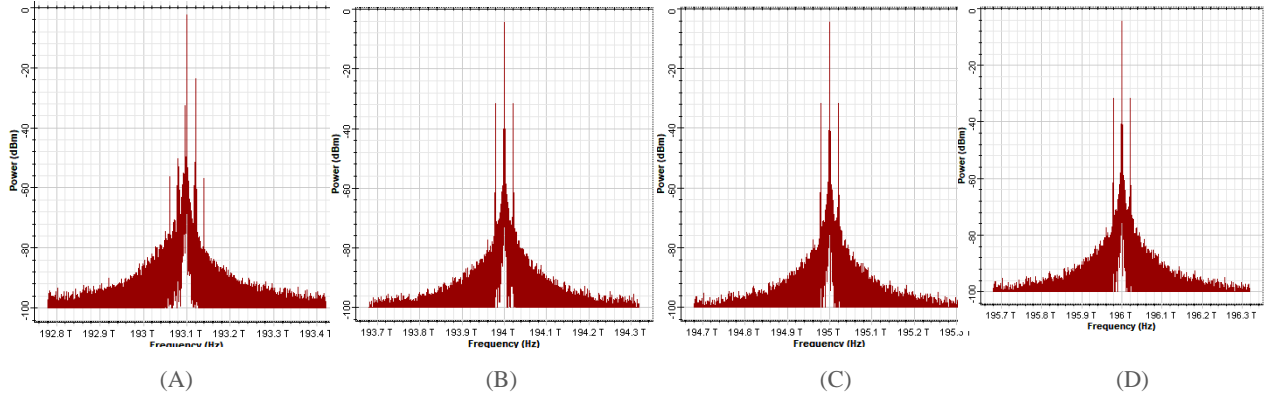


FIG. 12. A-D OUTPUT SPECTRUM OF MZM FOR THE FREQUENCY 193.1THZ, 194THZ, 195THZ AND 196THZ RESPECTIVELY.

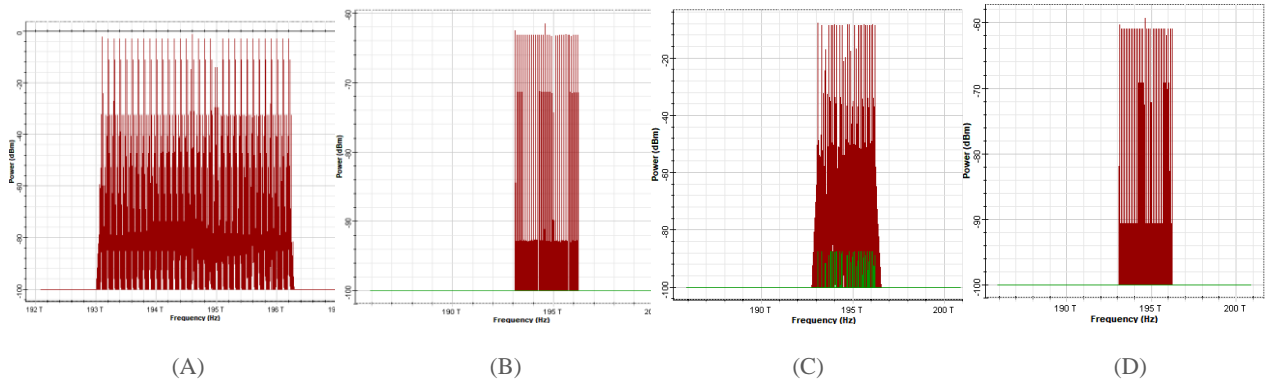


FIG. 13. A-D FREQUENCY SPECTRA OF WDM MUX FOR THE DOWNLINK AND UPLINK RESPECTIVELY.

The system's proficiency in handling bidirectional communication is illustrated by the frequency spectra for the uplink and downlink components in Fig. 13. Effective WDM channel allocation is highlighted by well-defined peaks in the uplink and downlink transmitter spectra, while the receiver spectra confirm reliable transmission and reception with minimal distortion but with little interference and precise channel separation.

Figs. 14 and 15 distinctly display the spectra of four DEMUX channels from both the downlink and uplink, with clear peaks at their respective frequencies. The clear separation between the channels and the uniform power levels across the spectra demonstrate effective channel isolation that underscores the dependable functionality of the WDM system, reinforcing the reliability of the WDM system in supporting precise bidirectional communication with little interference or crosstalk among channels.

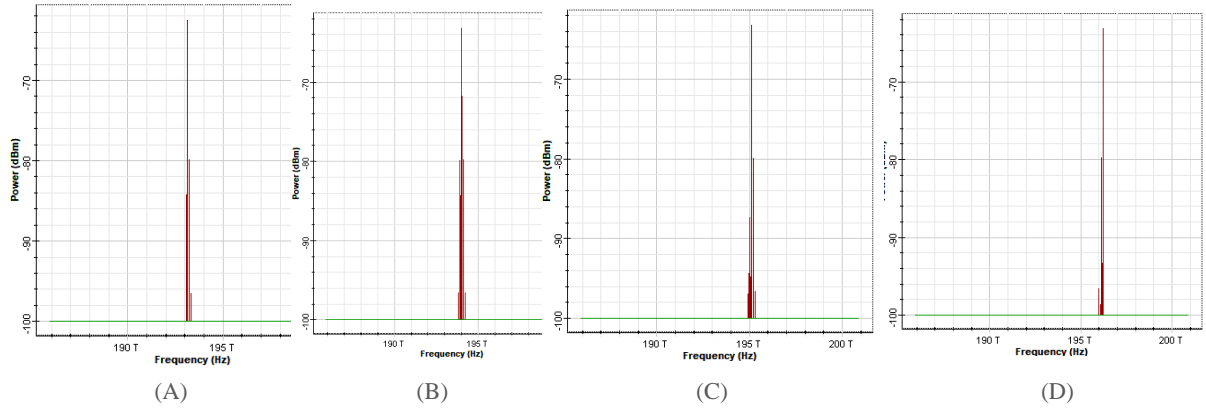


FIG. 14. A-D DOWNLINK DEMUX OUTPUT FOR FREQUENCY 193.1, 194.195, 196THZ RESPECTIVELY.

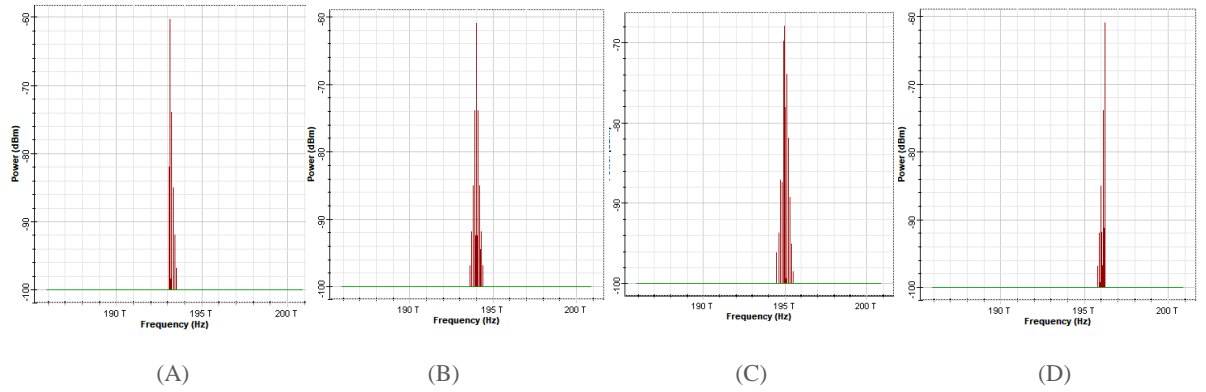


FIG.15. A-D UPLINK DEMUX OUTPUT FOR FREQUENCY 193.1, 194.195, 196THZ RESPECTIVELY.

Table V shows the performance characteristics of the uplink WDM system at both the transmitter and receiver ends. The transmitter side demonstrates uniform signal strength. Across channels with low noise power, obtain elevated SNR and OSNR values (exceeding 50 dB), signifying pristine signal creation and the noise power experiences a slight rise due to transmission effects on the receiver side.

The downlink WDM system's performance at both the transmitter and receiver sides is analyzed in Table VI. Signal power is about -2.69 dBm per channel, with noise power of -35 dBm, leading to SNR values ranging from 28 to 33 dB. OSNR values range from 31 to 35 dB at the transmitter side, which reflects adequate optical signal quality; nevertheless, further noise mitigation could optimize performance. At the receiver, it experiences a slight reduction, somewhat from -4.6 dBm to -6.8 dBm, as a result of anticipated transmission attenuation. The noise power is from -55 to -57 dBm at the receiver, maintaining SNR values above 50 dB and an average OSNR of 52 dB, resulting in excellent signal integrity after transmission. While the system demonstrates strong performance, further noise reduction at the transmitter could enhance proper alignment with the receiver's robust metrics.

TABLE V. UPLINK TRANSMITTER AND RECEIVER SIDE OF WDM ANALYZERS METRICS RESPECTIVELY.

WDM Analyzer						WDM Analyzer					
Frequency (THz)	Signal Power (dBm)	Noise Power (dBm)	SNR (dB)	Noise Power: 0.1nm (dBm)	OSNR (dB)	Frequency (THz)	Signal Power (dBm)	Noise Power (dBm)	SNR (dB)	Noise Power: 0.1nm (dBm)	OSNR (dB)
193.1	-46.52963	-100	53.417037	-100	53.417037	193.1	-46.52963	-100	53.417037	-100	53.417037
193.2	-46.52963	-100	53.417037	-100	53.417037	193.2	-46.52963	-100	53.417037	-100	53.417037
193.3	-46.52963	-100	53.417037	-100	53.417037	193.3	-46.52963	-100	53.417037	-100	53.417037
193.4	-46.52963	-100	53.417037	-100	53.417037	193.4	-46.52963	-100	53.417037	-100	53.417037
193.5	-46.52963	-100	53.417037	-100	53.417037	193.5	-46.52963	-100	53.417037	-100	53.417037
193.6	-46.52963	-100	53.417037	-100	53.417037	193.6	-46.52963	-100	53.417037	-100	53.417037
193.7	-46.52963	-100	53.417037	-100	53.417037	193.7	-46.52963	-100	53.417037	-100	53.417037
193.8	-46.52963	-100	53.417037	-100	53.417037	193.8	-46.52963	-100	53.417037	-100	53.417037
193.9	-46.52963	-100	53.417037	-100	53.417037	193.9	-46.52963	-100	53.417037	-100	53.417037
194	-46.52963	-100	53.417037	-100	53.417037	194	-46.52963	-100	53.417037	-100	53.417037
194.1	-46.52963	-100	53.417037	-100	53.417037	194.1	-46.52963	-100	53.417037	-100	53.417037
194.2	-46.52963	-100	53.417037	-100	53.417037	194.2	-46.52963	-100	53.417037	-100	53.417037
194.3	-46.52963	-100	53.417037	-100	53.417037	194.3	-46.52963	-100	53.417037	-100	53.417037
194.4	-46.52963	-100	53.417037	-100	53.417037	194.4	-46.52963	-100	53.417037	-100	53.417037
194.5	-46.52963	-100	53.417037	-100	53.417037	194.5	-46.52963	-100	53.417037	-100	53.417037
194.6	-46.52963	-100	53.417037	-100	53.417037	194.6	-46.52963	-100	53.417037	-100	53.417037
194.7	-46.52963	-100	53.417037	-100	53.417037	194.7	-46.52963	-100	53.417037	-100	53.417037
194.8	-46.52963	-100	53.417037	-100	53.417037	194.8	-46.52963	-100	53.417037	-100	53.417037
194.9	-46.52963	-100	53.417037	-100	53.417037	194.9	-46.52963	-100	53.417037	-100	53.417037
195	-46.52963	-100	53.417037	-100	53.417037	195	-46.52963	-100	53.417037	-100	53.417037
195.1	-46.52963	-100	53.417037	-100	53.417037	195.1	-46.52963	-100	53.417037	-100	53.417037
195.2	-46.52963	-100	53.417037	-100	53.417037	195.2	-46.52963	-100	53.417037	-100	53.417037
195.3	-46.52963	-100	53.417037	-100	53.417037	195.3	-46.52963	-100	53.417037	-100	53.417037
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195.6	-46.52963	-100	53.417037	-100	53.417037	195.6	-46.52963	-100	53.417037	-100	53.417037
195.7	-46.52963	-100	53.417037	-100	53.417037	195.7	-46.52963	-100	53.417037	-100	53.417037
195.8	-46.52963	-100	53.417037	-100	53.417037	195.8	-46.52963	-100	53.417037	-100	53.417037
195.9	-46.52963	-100	53.417037	-100	53.417037	195.9	-46.52963	-100	53.417037	-100	53.417037
196	-46.52963	-100	53.417037	-100	53.417037	196	-46.52963	-100	53.417037	-100	53.417037
196.1	-46.52963	-100	53.417037	-100	53.417037	196.1	-46.52963	-100	53.417037	-100	53.417037
196.2	-46.52963	-100	53.417037	-100	53.417037	196.2	-46.52963	-100	53.417037	-100	53.417037

TABLE VI. DOWNLINK TRANSMITTER AND RECEIVER SIDE OF WDM ANALYZERS METRICS RESPECTIVELY.

WDM Analyzer						WDM Analyzer					
Frequency (THz)	Signal Power (dBm)	Noise Power (dBm)	SNR (dB)	Noise Power: 0.1nm (dBm)	OSNR (dB)	Frequency (THz)	Signal Power (dBm)	Noise Power (dBm)	SNR (dB)	Noise Power: 0.1nm (dBm)	OSNR (dB)
193.1	-46.52963	-100	53.417037	-100	53.417037	193.1	-46.52963	-100	53.417037	-100	53.417037
193.2	-46.52963	-100	53.417037	-100	53.417037	193.2	-46.52963	-100	53.417037	-100	53.417037
193.3	-46.52963	-100	53.417037	-100	53.417037	193.3	-46.52963	-100	53.417037	-100	53.417037
193.4	-46.52963	-100	53.417037	-100	53.417037	193.4	-46.52963	-100	53.417037	-100	53.417037
193.5	-46.52963	-100	53.417037	-100	53.417037	193.5	-46.52963	-100	53.417037	-100	53.417037
193.6	-46.52963	-100	53.417037	-100	53.417037	193.6	-46.52963	-100	53.417037	-100	53.417037
193.7	-46.52963	-100	53.417037	-100	53.417037	193.7	-46.52963	-100	53.417037	-100	53.417037
193.8	-46.52963	-100	53.417037	-100	53.417037	193.8	-46.52963	-100	53.417037	-100	53.417037
193.9	-46.52963	-100	53.417037	-100	53.417037	193.9	-46.52963	-100	53.417037	-100	53.417037
194	-46.52963	-100	53.417037	-100	53.417037	194	-46.52963	-100	53.417037	-100	53.417037
194.1	-46.52963	-100	53.417037	-100	53.417037	194.1	-46.52963	-100	53.417037	-100	53.417037
194.2	-46.52963	-100	53.417037	-100	53.417037	194.2	-46.52963	-100	53.417037	-100	53.417037
194.3	-46.52963	-100	53.417037	-100	53.417037	194.3	-46.52963	-100	53.417037	-100	53.417037
194.4	-46.52963	-100	53.417037	-100	53.417037	194.4	-46.52963	-100	53.417037	-100	53.417037
194.5	-46.52963	-100	53.417037	-100	53.417037	194.5	-46.52963	-100	53.417037	-100	53.417037
194.6	-46.52963	-100	53.417037	-100	53.417037	194.6	-46.52963	-100	53.417037	-100	53.417037
194.7	-46.52963	-100	53.417037	-100	53.417037	194.7	-46.52963	-100	53.417037	-100	53.417037
194.8	-46.52963	-100	53.417037	-100	53.417037	194.8	-46.52963	-100	53.417037	-100	53.417037
194.9	-46.52963	-100	53.417037	-100	53.417037	194.9	-46.52963	-100	53.417037	-100	53.417037
195	-46.52963	-100	53.417037	-100	53.417037	195	-46.52963	-100	53.417037	-100	53.417037
195.1	-46.52963	-100	53.417037	-100	53.417037	195.1	-46.52963	-100	53.417037	-100	53.417037
195.2	-46.52963	-100	53.417037	-100	53.417037	195.2	-46.52963	-100	53.417037	-100	53.417037
195.3	-46.52963	-100	53.417037	-100	53.417037	195.3	-46.52963	-100	53.417037	-100	53.417037
195.4	-46.52963	-100	53.417037	-100	53.417037	195.4	-46.52963	-100	53.417037	-100	53.417037
195.5	-46.52963	-100	53.417037	-100	53.417037	195.5	-46.52963	-100	53.417037	-100	53.417037
195.6	-46.52963	-100	53.417037	-100	53.417037	195.6	-46.52963	-100	53.417037	-100	53.417037
195.7	-46.52963	-100	53.417037	-100	53.417037	195.7	-46.52963	-100	53.417037	-100	53.417037
195.8	-46.52963	-100	53.417037	-100	53.417037	195.8	-46.52963	-100	53.417037	-100	53.417037
195.9	-46.52963	-100	53.417037	-100	53.417037	195.9	-46.52963	-100	53.417037	-100	53.417037
196	-46.52963	-100	53.417037	-100	53.417037	196	-46.52963	-100	53.417037	-100	53.417037
196.1	-46.52963	-100	53.417037	-100	53.417037	196.1	-46.52963	-100	53.417037	-100	53.417037
196.2	-46.52963	-100	53.417037	-100	53.417037	196.2	-46.52963	-100	53.417037	-100	53.417037

VI. CONCLUSION

By implementing DWDM and RoF technologies, the proposed relay-based station architecture adeptly addresses critical obstacles in 5G RAN. With the integration of optical technology to sustain continuous SNR and OSNR values exceeding 50 dB over 32 channels, delivering high-quality signal transmission with minimal degradation and clear spectral peaks, efficient reuse of wavelengths, and strong channel separation in the MUX and DEMUX outputs shows it can communicate in both directions with little interference. EDFAs with continuous-wave lasers improve system performance by maintaining dependable optical signal amplification and lowering power loss, thereby facilitating high-speed data transmission over extended distances. The relay architecture effectively provides scalability for increasing network requirements in high-density user traffic. These attributes position the system as a reinforced foundation for enhancing 5G coverage and performance, particularly in high-frequency bands where route loss and interference remain key challenges, and systems with the ability to maintain low-noise power and consistent transmission in both downlink and uplink contexts underscore and prove its dependability and efficiency.

CONFLICT OF INTEREST

Conflict of Interest the authors confirm that no conflicts of interest exist regarding this paper's publication. Salahaddin University-Erbil acknowledges its support for this research through funding for its implementation.

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