

\*

:  
:

( )

(R=-1) ( Mean Stress)

( )

( + )

( SEM)

( - ) .( - )

**Abstract**

This study has aimed to illustrate the effect of one surface hardening method( Nitriding) upon fatigue life time of medium carbon steel alloys . Therefore all tests concerning round bending of fatigue ,have been conducted at ordinary laboratory circumstances , within a mean stress , [ value = 0&stress ratio ,R = -1], as stable and changing stress capacities , were forced in order to know the metal resistance to these stresses under the different dynamic loading .There by to give the safety life time of this metal , nitriding process (liquid & Gas ) was carried out to the metal ,which contributed in improving the fatigue resistance , as the improvement amount was based on the hardened depth , and the fatigue boundary , increases with nitriding layer depth . strength tests, micro and hardening were carried out for the applied heat treatment circumstances ,because these tests are considered to be as criteria and connected with revelant correlation , concerning fatigue tests results .

Actually , micro structure examination has carried often before treatment , where as the micro structure was found before treatment [ ferrit & perlite ] while nitrogen phases were observed to be high with a layer of chrome iron nitrides on the treated service with nitriding , that confirm the nitriding role in structural barriers formation on the service , that acts on stopping towards the crack..

Consequently, the images of (SEM) , regarding the fracture service , have declared a follow up images towards fatigue cracks . This crack is originated under the thick hardened surface.Layer and developes , is a lease plastic region , as it was detected that fatigue life time , increases when loading from (high – low ) at the changing capacity of fatigue tests rather than( Low- High).

أ- )  
 ب- ( :  
 :  
 : 1 (42 Cr M04)  
 :

2 :  
 أ- )  
 ب- )  
 ج- (1) :  
 1 :  
 )

( )  
 (Bending)  
 (stress)  
 (life)  
 ( 650-480C° )  
 )  
 (2) -:

1-4 (3)

(42 Cr M04)

(Die- blocks)  
 (Spindles)  
 .(Pump shafts)  
 : \_\_\_\_\_ .2

(1)

	C%	Si%	Mn%	P%	S%	Cr%	Mo%	Ni%	Cu%	V%
	0.439	0.368	0.810	0.025	0.02	0.99	0.231	0.33	0.16	0.02
	-0.38 0.45	0.40	-0.60 0.90	0.035	0.03	-0.90 1.2	-0.15 0.30	-	-	-

(6.74mm)

2-4

(1000,800,500,320,220) ( 80 (10 mm) cm)  
 2 / ( CNC)

.(Diamond)  
 3-4

:

(R30)

(2)

A	-	
B	B1	30 min
	B2	90
C	-	

( 860C° ) 4-4  
 20min) .(

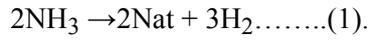
( 600C° )

( Liquid )

: Nitriding)

(

(B)



(580C°)

) NaCN

(%70-60

( 40%- KCN

( 30%)

NH4Cl)(REG1)

: \_\_\_\_\_ 5-4

1-5-4

Roughness inspection

(B)

(Gas Nitriding)

-ب

(C)

NH3

)( 600C

(3)

No.	Specimen	Ra(μ m)	Ri(μ m)
1.	A	0.13	0.96
2.	B1	0.15	1.88
3.	B2	0.16	1.97
4.	C	0.06	1.19

( Instron)

: 2-5-4

(4)

No.	Specimen	Time	Yield Strength MPa	Tensile Strength MPa
1.	A	As recived	1047	1089
2.	B1	30 min	-	1551
3.	B2	90min	-	1672
4.	C	2880min	-	1702

: 3-5-4

( ( Macro )

150kg)

.Hardness)

.1

( Rockwell)

(Frank 147/N150 kg)

$$H_v = 1.854 \frac{P}{d^2} \dots \dots \dots 2)$$

.2

/ :p :  
/ :d  
:Hv ( 2kg)

(5)

Specimen	A	B1	B2	C
HRC	22	48	50	52
H.V	237	486	522	538

Micro Hardness -ب

(Etching)

( 98%) (2%)  
Hv Kg /mm<sup>2</sup>.

) ( (Prufmas chinen 3030 Rating + Messen)  
(100gm)

(Universal camera Microscope  
Reichert MeF2, Nr360974)  
(3)

5-5-4

( case depth)  
.[B1,B2,C][2]  
4-5-4  
(Micro structure examination)

(X- Ray

diffractometer)

: -ا

(4)

.(1000,800,500,320M220,120)

Fatigue test :

6-5-4

(Polising) -ب

(Alomin)

(Rotating Bending)

(Scheneck Punn Rotating

Bending)

(5) ( R=-1)

8-5-2

(2)

( Constant Amplitude test)

(2) (6000 rpm)

( S-N)

(6) (30 cm)

A ( S-N) (B1,B2,C) ( 900 MPa)

-(6) 7-5-4

( ) (6)

Specimen	S-N Curve	Fatigue Limit; $\sigma_f$ (MPa)
A	$\sigma_f = 830N_f^{-0.03}$	450
B1	$\sigma_f = 1138N_f^{-0.053}$	480
B2	$\sigma_f = 1383N_f^{-0.053^2}$	575
C	$\sigma_f = 2124N_f^{-0.093}$	512

(515,530,575) (Variables : Amplitude)

(10000)

(10000)

(50000)

(A,B,C)

(6)

(Block increasing)

(8) (7)

(Block decreasing)

k (A,B,C)

(Mimer Linear Pamage Rule)

i

ni

Ni

$$D1 + D2 \dots + Di+1 + Di = 1 \dots (3)$$

:

$$\sum_{i=1}^k \frac{n_i}{N_i} = 1 \dots (4)$$

(7)

.S-N

		$\sigma_1$	n1	$\sigma_2$	n2	$\sigma_3$	n3	Nexp	)
A1	L-H	515	10000	530	10000	575	50000	150000	(
A2	H-L	575	10000	530	10000	515	50000	240000	
B1	L-H	515	10000	530	10000	575	50000	723000	
B2	H-L	575	10000	530	10000	515	50000	1714000	
C1	L-H	700	10000	725	10000	750	50000	104000	
C2	H-L	750	10000	725	10000	700	50000	296000	

(8)

	L-H	Nexp	N Miner	$\frac{N}{N}$	D-Miner
A1	515-530-575	93000	7788	0.08	4.3
A2	575-530-515	240000	149316	0.58	1.2
B1	515-530-575	723000	187365	0.25	1.2
B2	575-530-515	1014000	1487539	1.4	0.7
C1	700-725-750	208701	39471	0.18	1.8
C2	750-725-700	898101	211660	0.23	21.5

:

(575)N/mm<sup>2</sup> 90min  
 (450) N/mm<sup>2</sup>, 30min ( 42CrM04)  
 ( 90min, 30min) (480N/mm<sup>2</sup>)  
 (512N/mm<sup>2</sup>)  
 (450 N/mm<sup>2</sup>)  
 .[4]

[5.6]

.2 .[7]

.3

.( - )

( 90, 30)min

.4

,0.5min 0.3min  
.[1, 3, 4, 5, 6, 8]

.5

(1089)  
(1551) N/mm2  
(1702 ) (1672)

.[4,5,6,9]

.6

( (7) C,B,A)  
( - )  
( - )

.(6 ,5)

:

" , , , , , [1]

[5]

.1989 , ,

(A,B,C)

"Metal Hand" Desk Edition  
[2]Boyer, H.E and Gall T.L,  
ASM3<sup>rd</sup> edition, 1985.

- ) ( - ) (

[3]Jack DH; "Effect of Process  
Variables on the Fiting  
Resistance of Nitride Steel"  
Heat Treatment Proceeding of  
an International Conference p.  
169-177,1979.

( - )

:

.1

( )  
.Y= K  $\sqrt{t}$

[10]Mikcorite," Heat Treatment of Steel", 2004. Internet.

[11]J. W. Martin and Jones; " Residual stress Distribution in Nitrided En 413 steel as Function of case Depth," University of Oxford, Metal Technology.1999.

[4] . ) .1985 , (

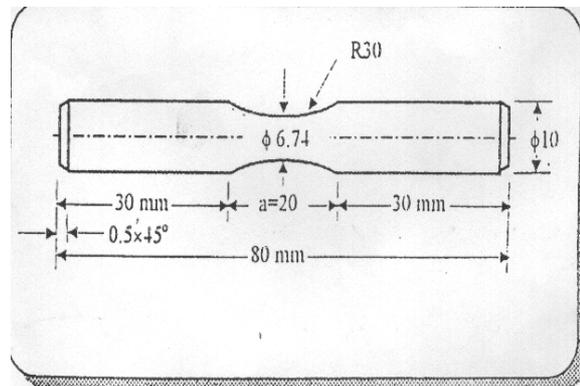
[5] ) -2001 -

[6] ) -2002 -

[7]Technology in the heat treatment of steel Prof. Dr. Inghabil, Dr .H.C Hans-Joachim, Internet 18-7.2002.

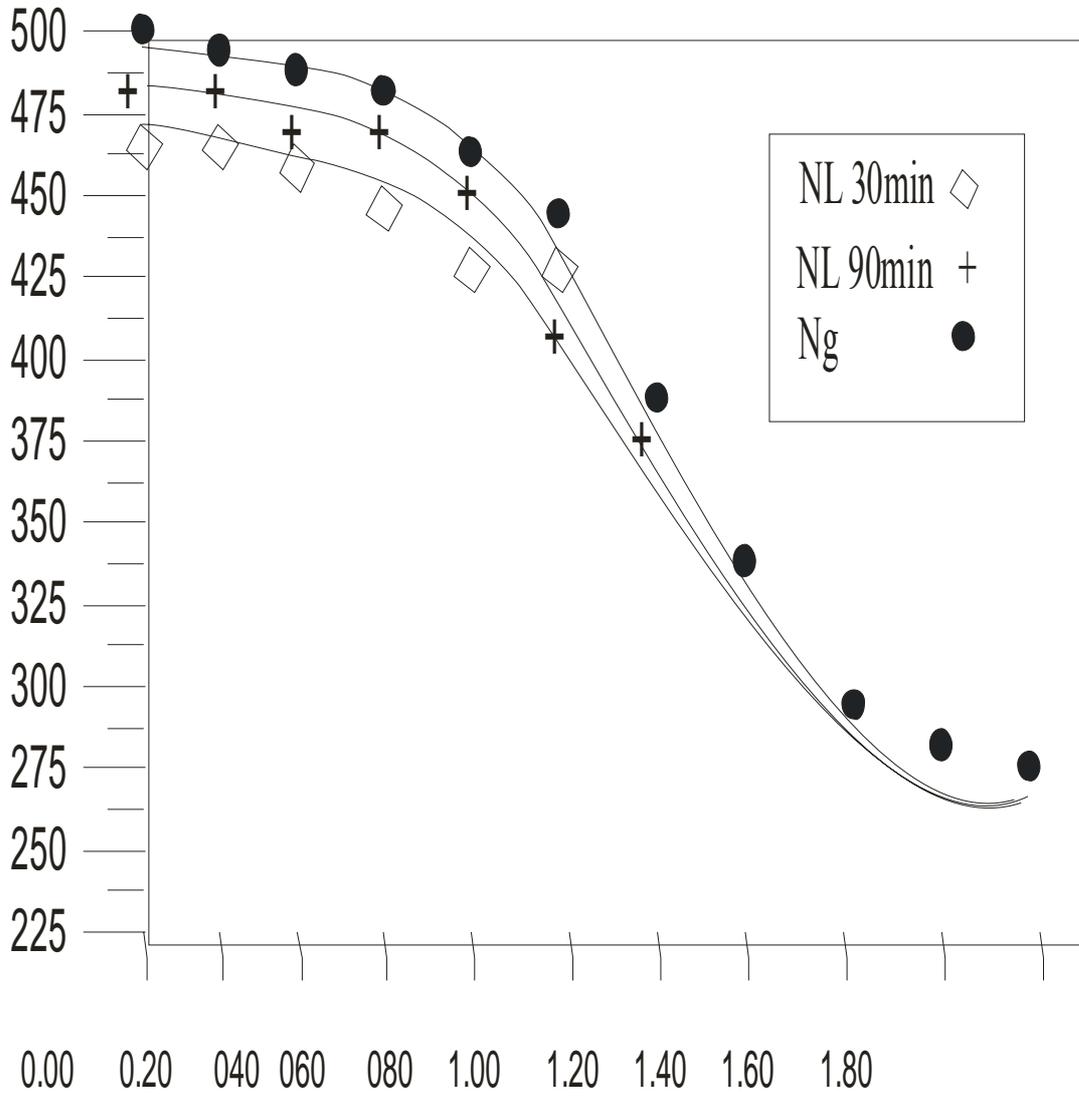
[8]Lakhtin Y, Engineering Physical Metarllurgy, 1977.

[9]Thetring K, Butter worths " Steel& Heat Treatment",1984.

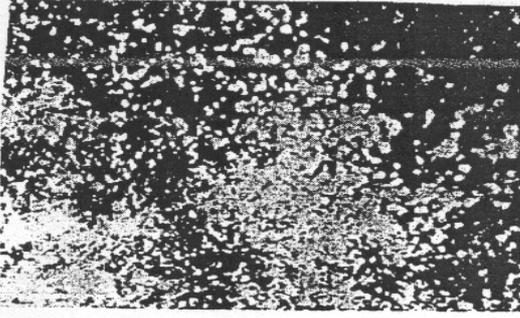


(1)

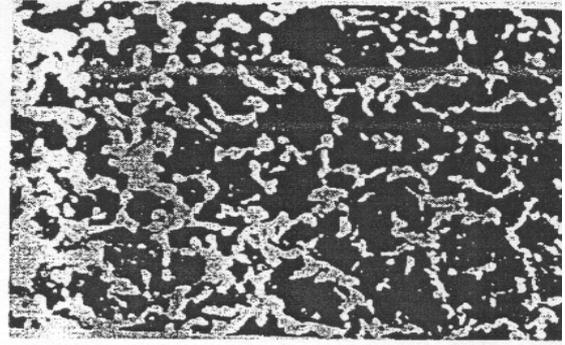
HSM,19Rotating Fatigue Machine



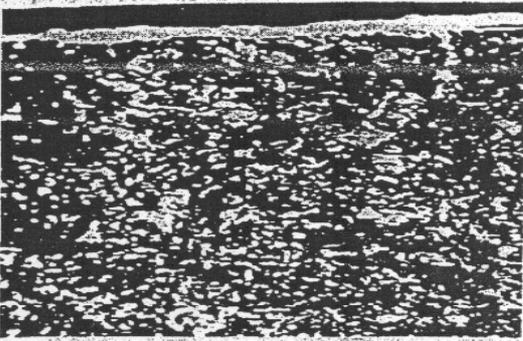
(2)



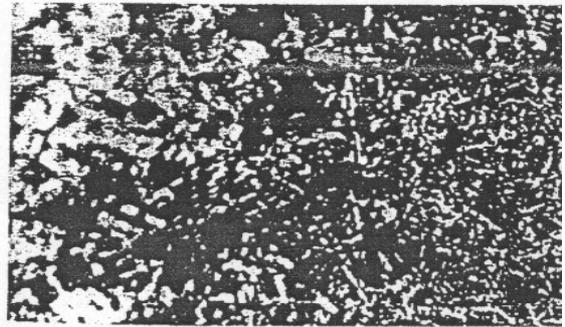
نتردة سائلة بين القلب و السطح  
قوة التكبير 40×10



برلايت + فرايت قيل إجراء المعاملة  
قوة التكبير 40×10

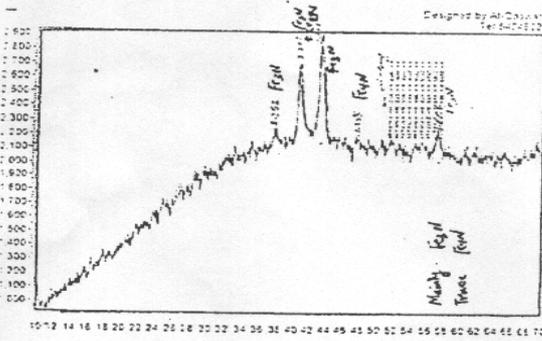


نتردة غازية  
قوة التكبير 40×10

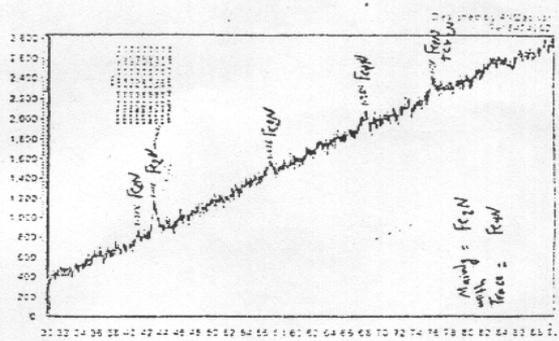


نتردة سائلة بفترة زمنية 90 Min.  
قوة التكبير 40×10

شكل رقم (3) يوضح التركيب المجهرى للعينات قبل وبعد إجراء النتردة

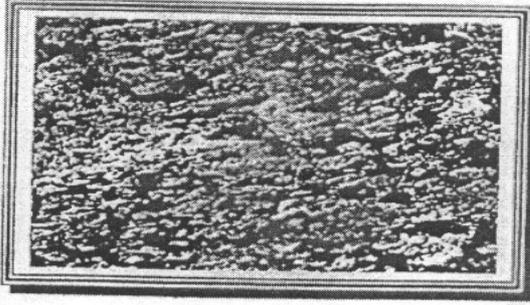


نتردة غازية

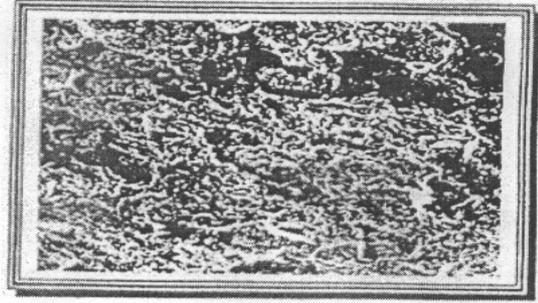


نتردة سائلة

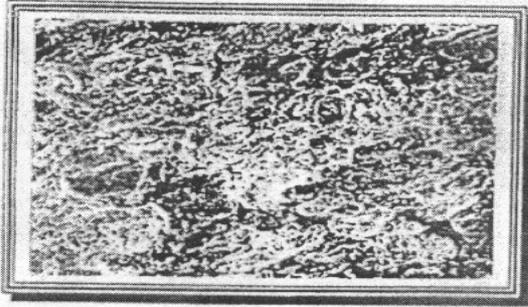
شكل رقم (4) يوضح مخطط تحديد الأطوار



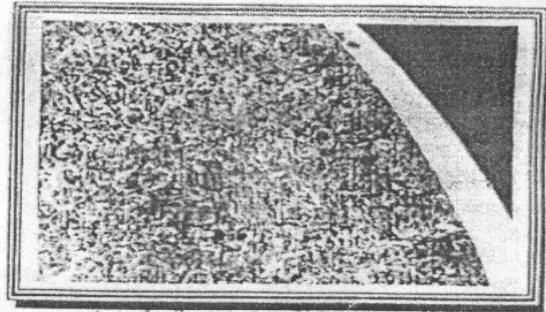
معدن بدون تعامل



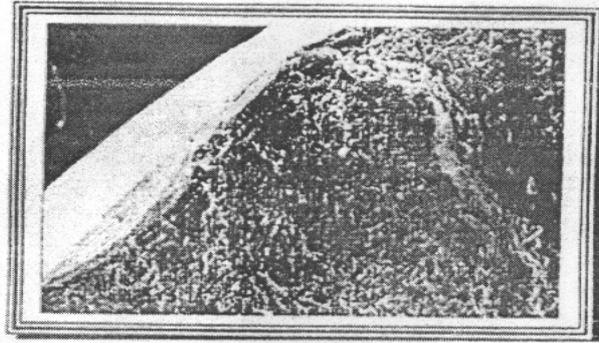
نتردة سائلة (الحمل عالى)



نتردة غازية (الحمل واطن)

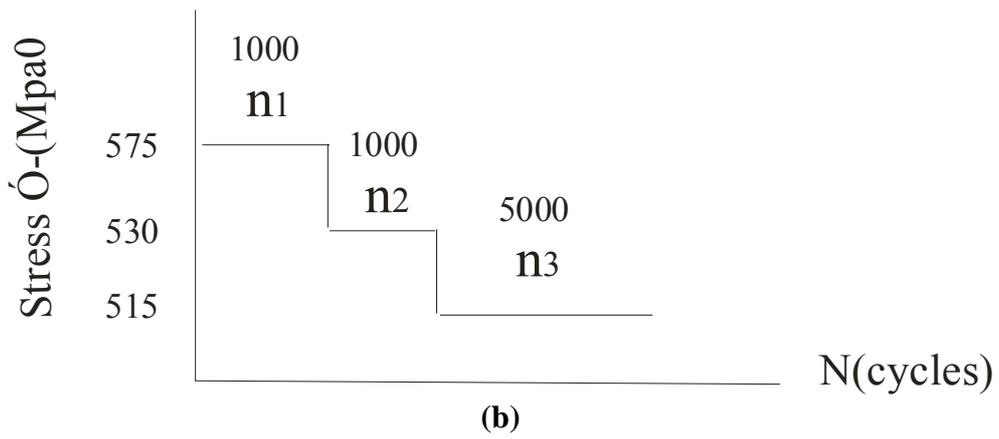
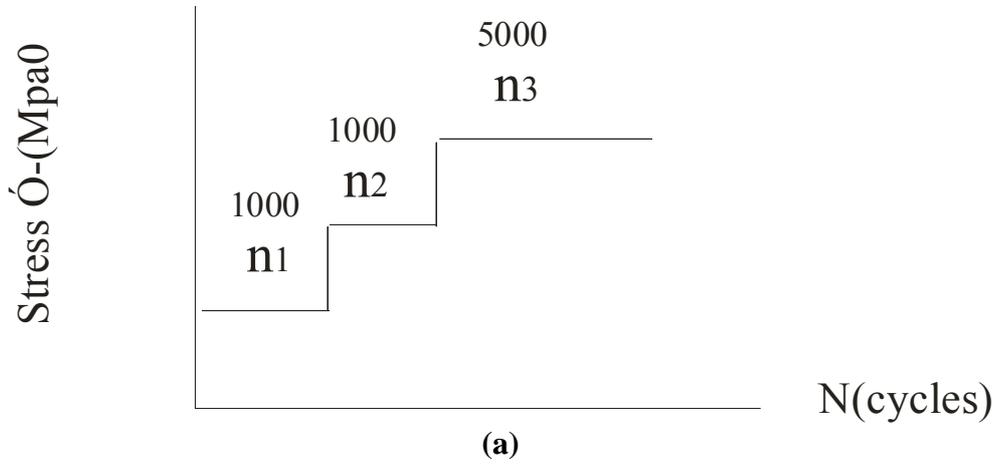


نتردة سائلة (الحمل واطن)



نتردة غازية (الحمل عالى)

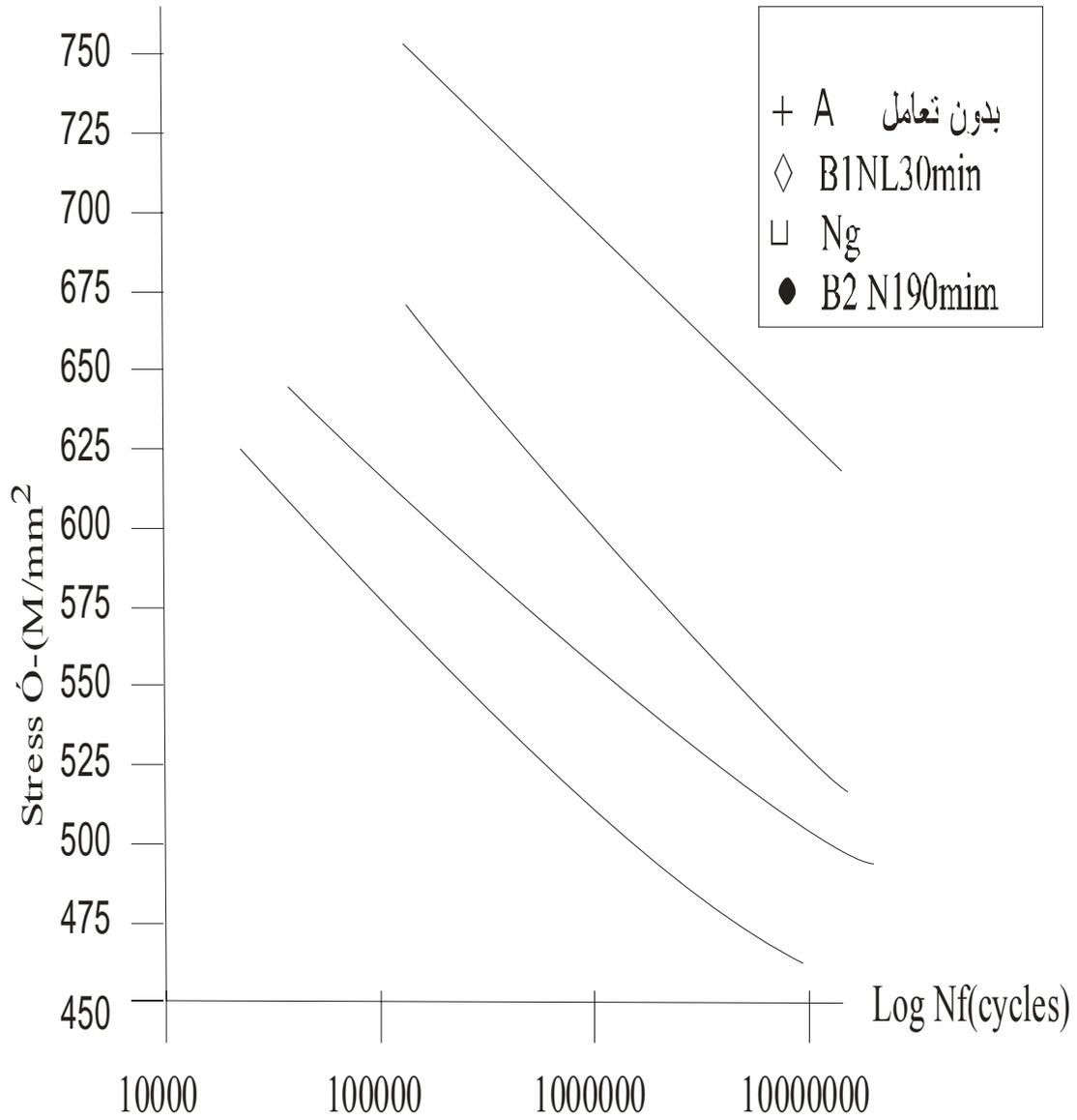
شكل (5) يوضح مقاطع سطح الكسر ونشوء الشق.



(b)

(a)

(6)



(S-N) (7)