



Performance of some new estimated ridge parameter regression models

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ABSTRACT

In the presence of high correlation among the independent variables in a linear regression model, a condition known as multicollinearity, the ordinary least squares (OLS) estimator tends to produce large variations in the sample. Aiming to overcome this problem, several estimators have been recommended. One of these estimators is ridge regression, which introduces a bias in the coefficient estimates but often results in a lower variance compared to OLS. Consequently, ridge regression may achieve a smaller mean square error (MSE). This paper reviews 50 kinds of ridge parameter (m) used in the estimation of the ordinary ridge regression estimator. Additionally, 10 new types of m are proposed based on different approaches. Aiming to evaluate the performance of these estimators, a simulation study and a real-data numerical example are conducted, using estimated mean squared error as the criterion for comparison. Results show that the newly proposed estimators for m can serve as effective alternatives to existing ones.

Introduction

$$y = X\xi + e. \quad (1)$$

Consider a standard model of multiple linear regression [1].

where y is an $n \times 1$ vector of observations, ξ is a $p \times 1$ vector of unknown regression coefficients, X is an $n \times p$ known design matrix of order p , and u is an $n \times 1$ vector of random variables, which is distributed as multivariate normal with a mean vector of 0 and a variance-covariance matrix $\sigma^2 I_n$, I_n is an identity matrix of order n . The standard least squares estimate (LSE) or maximum likelihood estimate (MLE) of ξ is derived as follows:

$$\hat{\xi} = C^{-1}X'y. \quad (2)$$

The outcome is highly influenced by the matrix $C = X'X$. If the C matrix is ill conditioned (with near dependency among columns C or $\det(X'X \approx 0)$), then the LSE can be sensitive to errors.

For example, due to multicollinearity, some regression coefficients may become statistically insignificant or exhibit incorrect signs, making meaningful statistical inference difficult or even impossible for practitioners. Kibria, B. M. G [1],[2],[3] identified that multicollinearity as a common issue in engineering applications. Aiming to estimate ξ , using $C(m) = C + mI_p$, ($m \geq 0$), rather than C , has been proposed. The obtained estimators are provided as follows:

$$\hat{\xi}(m) = (C + mI_p)^{-1}X'y, \quad (2)$$

which are known as ridge regression estimators. The constant $m > 0$ is known as or biasing or ridge parameter. As m increases from zero and continues up to infinity, the regression estimates tend toward zero. Although these estimators introduce bias, they yield a given value of m , minimum mean square error (MSE), compared to LSE ([1], [2], [3]). However, they will rely on the unknown parameters, which cannot be calculated practically but should be estimated from real data instead. Much of the debate surrounding ridge regression,

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particularly in the context of Hills's regression, emphasizes the challenge of determining an appropriate empirical value. Numerous methods for estimating m have been proposed by different researchers, including Dempster et al. [3],[4], [5], among others. Owing to the fact that ridge regression estimators have been applied by in different studies across various time periods and under diverse simulation conditions, direct comparisons between them is difficult. This paper aims to conduct a detailed examination of 50 distinct Hill-type estimators and 10 newly proposed ridge estimator, all evaluated based on their performance in minimizing MSE. The investigation is conducted using Monte Carlo simulations, considering a range of scenarios. These scenarios include variations in random error variance, correlation among explanatory variables, sample sizes, and vectors of unknown coefficients. This paper is organized as follows: First, the available methods for estimating m are reviewed, followed by the simulation. Applications of the proposed methods are then presented. Finally, some concluding remarks are provided.

2. Methodology

Suppose an orthogonal matrix L exists such that $L'CL = \Lambda$, where $\Lambda = \text{diag}(\lambda_1, \lambda_2, \dots, \lambda_p)$.

The eigenvalues of the matrix C are contained in the orthogonal (canonical form) version of the mode (1).

$$S = X^* \xi + e, \quad (3)$$

where $X^* = XL$ and $\tau = L' \xi$. Therefore, the generalized ridge regression estimators are derived as follows:

$$\hat{\tau}(m) = (X^{*'} X^* + m)^{-1} X^{*'} S, \quad (4)$$

where $m = \text{diag}(m_1, m_2, \dots, m_p)$, $m_i > 0$ and $\hat{\tau} = \Lambda^{-1} X^{*'} S$. The ordinary least squares (OLS) estimates of τ are derived from [3]. The value of m_i minimizes the MSE $\hat{\tau}(m)$, where

$$\text{MSE}(\hat{\tau}(m)) = \sigma^2 \sum_{i=1}^p \frac{m_i^2 \tau_i^2}{(\lambda_i + m_i)^2} + \sum_{i=1}^p \frac{m_i^2 \tau_i^2}{(\lambda_i + m_i)^2}. \quad (5)$$

When

$$m_i = \frac{\sigma^2}{\tau_i^2}, \quad (6)$$

where σ^2 denotes the error variance of model (1), and τ_i denotes the i th element of τ . Hocking et al. [6] demonstrated that, given the known optimal m_i , the generalized ridge regression estimator outperforms all other estimators in the class of examined biased estimators. However, the ideal value of m_i is entirely dependent on the unknown σ^2 and τ_i , which must be determined from the observed data. Hoerl, Kennard [3] proposed replacing σ^2 and τ_i^2 with their equivalent unbiased estimators. That is to say,

$$\hat{m}_i = \frac{\hat{\sigma}^2}{\hat{\tau}_i^2}, \quad (7)$$

where $\hat{\sigma}^2 = (\sum \hat{e}^2)/(n - p)$ represents the residual mean square estimate, which is an unbiased estimator of σ^2 and $\hat{\tau}_i$ is the i th element of $\hat{\tau}$, which is also an unbiased estimator of τ . Other novel methods based on Eq. (8) are then discussed as follows:

$$1. \quad \hat{m}_1 = \frac{\hat{\sigma}^2}{\hat{\tau}_{\max}^2}, \quad (8)$$

where $\hat{\tau}_{\max}$ is the maximum element of $\hat{\tau}$. If σ^2 and τ are known, then $\hat{m}_1$ will yield a smaller MSE than the LSE [3].

$$2.[7] \quad \hat{m}_2 = \frac{2\hat{\sigma}^2}{\hat{\xi}' \hat{\xi}}, \quad (9)$$

$$3.[4] \quad \hat{m}_3 = \frac{p\hat{\sigma}^2}{\hat{\xi}' \hat{\xi}} = \frac{p\hat{\sigma}^2}{\hat{\tau}' \hat{\tau}} = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \tau_i^2}, \quad (10)$$

where $\hat{\xi}$ is the LSE of ξ .

$$4.[5] \quad \hat{m}_4 = \hat{\xi}'_k \hat{\xi} = \hat{\xi}' \hat{\xi} - \hat{\sigma}^2 \sum_{i=1}^p \frac{1}{\lambda_i} \quad (11)$$

$$5.[8] \quad \hat{m}_5 = \frac{p\hat{\sigma}^2}{\hat{\tau}' X' X \hat{\tau}} = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \lambda_i \tau_i^2} = \frac{p\hat{\sigma}^2}{\hat{\xi}' \Lambda \hat{\xi}} \quad (12)$$

$$6.[6] \quad \hat{m}_6 = \frac{\hat{\sigma}^2 \sum_{i=1}^p (\lambda_i \hat{\tau}_i)^2}{(\sum_{i=1}^p \lambda_i \hat{\tau}_i)^2} \quad (13)$$

$$7.[9] \quad \hat{m}_7 = \frac{1}{\hat{\sigma}_{\max}^2} \quad (14)$$

$$8.[10]$$

$$\hat{m}_8 = \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \left[\frac{\tau_i^2}{1 + (1 + \lambda_i \left(\frac{\tau_i^2}{\hat{\sigma}^2} \right)^2)} \right]} \quad (15)$$

9.[1]

$$\hat{m}_9 = \frac{1}{p} \sum_{i=1}^p \frac{\hat{\sigma}^2}{\tau_i^2} \quad (16)$$

$$\hat{m}_{10} = \frac{\hat{\sigma}^2}{(\prod_{i=1}^p \tau_i^2)^{\frac{1}{p}}} \quad (17)$$

$$\hat{m}_{11} = \text{median} \left(\frac{\hat{\sigma}^2}{\tau_i^2} \right) \quad (18)$$

10.[11]

$$\hat{m}_{12} = \frac{\lambda_{\max} \hat{\sigma}^2}{(n-p-1)\hat{\sigma}^2 + \lambda_{\max} \hat{\xi}_{\max}^2}, \quad (19)$$

where $\lambda_{\max}$ is the maximum eigenvalue of the matrix $X'X$.

11.[12]

$$\hat{m}_{13} = \max \left(\frac{\lambda_i \hat{\sigma}^2}{(n-p-1)\hat{\sigma}^2 + \lambda_i \hat{\xi}_i^2} \right) \quad (20)$$

$$\hat{m}_{14} = \text{median} \left(\frac{\lambda_i \hat{\sigma}^2}{(n-p-1)\hat{\sigma}^2 + \lambda_i \hat{\xi}_i^2} \right) \quad (21)$$

$$\hat{m}_{15} = \frac{1}{p} \sum_{i=1}^p \left(\frac{\lambda_i \hat{\sigma}^2}{(n-p-1)\hat{\sigma}^2 + \lambda_i \hat{\xi}_i^2} \right) \quad (22)$$

12.[13]

$$\hat{m}_{16} = \frac{\hat{\sigma}^2}{\hat{\xi}_{\max}^2} + \frac{1}{\lambda_{\max}} \quad (23)$$

$$\hat{m}_{17} = \max \left(\frac{\hat{\sigma}^2}{\hat{\xi}_i^2} + \frac{1}{\lambda_i} \right) \quad (24)$$

$$\hat{m}_{18} = \frac{1}{p} \sum_{i=1}^p \left(\frac{\hat{\sigma}^2}{\hat{\xi}_{\max}^2} + \frac{1}{\lambda_{\max}} \right) \quad (25)$$

$$\hat{m}_{19} = \text{median} \left(\frac{\hat{\sigma}^2}{\hat{\xi}_i^2} + \frac{1}{\lambda_i} \right) \quad (26)$$

$$\hat{m}_{20} = \frac{p \hat{\sigma}^2}{\sum_{i=1}^p \hat{\xi}_i^2} + \frac{1}{\lambda_{\max}} \quad (27)$$

$$\hat{m}_{21} = \frac{p \hat{\sigma}^2}{\sum_{i=1}^p \lambda_i \hat{\xi}_i^2} + \frac{1}{\lambda_{\max}} \quad (28)$$

13.[14]

$$\hat{m}_{22} = \max \left(\frac{1}{\sqrt{\frac{\hat{\sigma}^2}{\hat{\tau}_i^2}}} \right) \quad (29)$$

$$\hat{m}_{23} = \max \left(\sqrt{\frac{\hat{\sigma}^2}{\hat{\tau}_i^2}} \right) \quad (30)$$

$$\hat{m}_{24} = \left(\prod_{i=1}^p \frac{1}{\sqrt{\frac{\hat{\sigma}^2}{\hat{\tau}_i^2}}} \right)^{\frac{1}{p}} \quad (31)$$

$$\hat{m}_{25} = \left(\prod_{i=1}^p \frac{\hat{\sigma}^2}{\hat{\tau}_i^2} \right)^{\frac{1}{p}} \quad (32)$$

$$\hat{m}_{26} = \text{median} \left(\frac{1}{\sqrt{\frac{\hat{\sigma}^2}{\hat{\tau}_i^2}}} \right) \quad (33)$$

$$\hat{m}_{27} = \text{median} \left(\sqrt{\frac{\hat{\sigma}^2}{\hat{\tau}_i^2}} \right) \quad (34)$$

$$\hat{m}_{28} = \left(\prod_{i=1}^p \frac{\lambda_i \hat{\sigma}^2}{(n-p)\hat{\sigma}^2 + \lambda_i \hat{\tau}_i^2} \right)^{\frac{1}{p}} \quad (35)$$

14.[15]

$$\hat{m}_{29} = \max \left(0, \frac{p\hat{\sigma}^2}{\hat{\tau}'\hat{\tau}} - \frac{1}{n(VIF_j)_{\max}} \right), \quad (36)$$

$$VIF_j = \frac{1}{1-R_j^2}$$

is the variance inflation factor of the jth regressor.

15.[16]

$$\hat{m}_{30} = \frac{\sum_{i=1}^p (\lambda_i \hat{\tau}_i)^2}{(\sum_{i=1}^p (\lambda_i \hat{\tau}_i)^2)^2} + \frac{1}{\lambda_{\max}} \quad (37)$$

16.[17]

$$\hat{m}_{31} = \max \left(\frac{1}{\frac{\lambda_{\max} \tau_i^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max} \hat{\tau}_i^2)}} \right) \quad (38)$$

$$\hat{m}_{32} = \text{median} \left(\frac{1}{\frac{\lambda_{\max} \tau_i^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max} \hat{\tau}_i^2)}} \right) \quad (39)$$

17.[18]

$$\hat{m}_{33} = \left(\prod_{i=1}^p \frac{\lambda_i \hat{\sigma}^2}{(n-p-1)\hat{\sigma}^2 + \lambda_i \hat{\tau}_i^2} \right) \quad (40)$$

$$\hat{m}_{34} = \max \left(\frac{1}{\sqrt{\frac{\lambda_{\max} \hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max} \hat{\tau}_i^2)}}} \right) \quad (41)$$

$$\hat{m}_{35} = \max\left(\sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\tau}_i^2)}}\right) \quad (42)$$

$$\hat{m}_{36} = \left(\prod_{i=1}^p \frac{1}{\sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\tau}_i^2)}}}\right)^{1/p} \quad (43)$$

$$\hat{m}_{37} = \left(\prod_{i=1}^p \sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\tau}_i^2)}}\right)^{1/p} \quad (44)$$

$$\hat{m}_{38} = \text{median}\left(\frac{1}{\sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\tau}_i^2)}}}\right) \quad (45)$$

18.[19]

$$\hat{m}_{39} = \frac{(\lambda_{\max} + \lambda_{\min})}{2 \sum_{i=1}^p |\hat{\xi}|_j} \left\{ \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \xi_i^2} \right\} \quad (46)$$

$$\hat{m}_{40} = \frac{(\lambda_{\max} + \lambda_{\min})\lambda_{\max}\hat{\sigma}^2}{2 \sum_{i=1}^p |\hat{\xi}|_j (n-p)\hat{\sigma}^2 + \lambda_{\max}\xi_{\max}^2} \quad (47)$$

19.[20]

$$\hat{m}_{41} = \max(\sqrt{m_i}) \quad (48)$$

$$\text{where } m_i = \sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\alpha}_i^2)}}$$

$$\hat{m}_{42} = \left(\prod_{i=1}^p \frac{1}{\sqrt{m_i}}\right)^{\frac{1}{p}} \quad (49)$$

$$\hat{m}_{43} = \left(\prod_{i=1}^p \sqrt{m_i}\right)^{\frac{1}{p}} \quad (50)$$

$$\hat{m}_{44} = \text{median}\left(\frac{1}{\sqrt{m_i}}\right) \quad (51)$$

where

$$m_i = \sqrt{\frac{\lambda_{\max}\hat{\sigma}^2}{((n-p-1)\hat{\sigma}^2 + \lambda_{\max}\hat{\alpha}_i^2)}} \quad (52)$$

20.[21]

$$\hat{m}_{45} = \frac{p^2\hat{\sigma}^2}{\lambda_{\max}^2 \sum_{i=1}^p \hat{\tau}_i^2} \quad (53)$$

$$\hat{m}_{46} = \frac{p^3\hat{\sigma}^2}{\lambda_{\max}^3 \sum_{i=1}^p \hat{\tau}_i^2} \quad (54)$$

$$\hat{m}_{47} = \frac{p\hat{\sigma}^2}{\lambda_{\max}^{\frac{1}{3}} \sum_{i=1}^p \hat{\tau}_i^2} \quad (55)$$

$$\hat{m}_{48} = \frac{p\hat{\sigma}^2}{(\sum_{i=1}^p \sqrt{\lambda_i})^{\frac{1}{3}} \sum_{i=1}^p \hat{\tau}_i^2} \quad (56)$$

$$\hat{m}_{49} = \frac{2p\hat{\sigma}^2}{\sqrt{\lambda_i} \sum_{i=1}^p \hat{\tau}_i^2} \quad (57)$$

21.[22]

$$\hat{m}_{50} = \hat{\sigma} \quad (58)$$

$$\text{where } \hat{\sigma} = \sqrt{\sum_{j=1}^n \hat{e}_j / (n-p)}$$

22. The following 10 new estimators for m are introduced:

$$\begin{aligned} \hat{m}_{f1} &= p\hat{\sigma}^2 - \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \left[\frac{\tau_i^2}{1 + (1 + \gamma_i (\frac{\tau_i^2}{\sigma^2})^2)} \right]} \end{aligned} \quad (60)$$

$$\hat{m}_{f2} = \text{median}\left(p\hat{\sigma}^2 - \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \left[\frac{\tau_i^2}{1 + (1 + \gamma_i (\frac{\tau_i^2}{\sigma^2})^2)} \right]}\right)$$

(61)

$$\hat{m}_{f3} = \left(\frac{p\hat{\sigma}^2}{\sum_{i=1}^p \tau_i^2} - \frac{p\hat{\sigma}^2}{\sum_{i=1}^p \left[\frac{\tau_i^2}{1 + (1 + \gamma_i (\frac{\tau_i^2}{\sigma^2})^2)} \right]} \right) \quad (62)$$

$$\begin{aligned} \hat{m}_{f4} &= \text{harmonic mean} \\ &\text{of}(\hat{m}_{43}, \hat{m}_{44}, \hat{m}_{45}, \hat{m}_{46}, \hat{m}_{47}, \hat{m}_{48}, \hat{m}_{49}) \end{aligned} \quad (6)$$

$$\begin{aligned} \hat{m}_{f5} &= \text{Arithmetic mean} \\ &\text{of}(\hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3},) \end{aligned} \quad (64)$$

$$\begin{aligned} \hat{m}_{f6} &= \text{Arithmetic mean of} \\ &((\hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3},)/2) \end{aligned} \quad (65)$$

$$\hat{m}_{f7} = \text{Median}(\hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}) \quad (66)$$

$$\hat{m}_{f8} = \text{Min}(\hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}) \quad (67)$$

$$\begin{aligned} \hat{m}_{f9} &= \\ &\text{harmonic mean} \end{aligned} \quad (68)$$

$$\text{of}(\hat{m}_{43}, \hat{m}_{44}, \hat{m}_{45}, \hat{m}_{46}, \hat{m}_{47}, \hat{m}_{48}, \hat{m}_{49}, \hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3})$$

$$\hat{m}_{f10} = \text{Min}(\hat{m}_{43}, \hat{m}_{44}, \hat{m}_{45}, \hat{m}_{46}, \hat{m}_{47}, \hat{m}_{48}, \hat{m}_{49}, \hat{m}_{50}, \hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}) \quad (69)$$

3. Simulation study

This section discusses the simulation research, which compares the performance of various estimators. [2,3,5] used the following method to derive explanatory variables with varying degrees of collinearity.

$$X_{ij} = (1 - \varphi)^{\frac{1}{2}} z_{ij} + \varphi z_{ip}, \quad i = 1, 2, 3, \dots, n, \quad j = 1, 2, \dots, p, \quad (71)$$

where z_{ij} is an independent standard normal pseudo-random number, and s is chosen such that the correlation between any two variables of explanation is given by s^2 . These variables are then standardized, resulting in X 's and X 's in correlation forms. The response variable y is considered by the following:

$$y_i = \xi_0 + \xi_1 x_{i1} + \xi_2 x_{i2} + \dots + \xi_p x_{ip} + e_i \quad i = 1, 2, \dots, n, \quad (72)$$

where e_i is independent and identically distributed random variables (*i. i. d.*) normal $(0, \sigma^2)$. Therefore, zero intercept for (60) will be assumed. Moreover, four explanatory variables $p = 4$ will be available, while the values of σ are chosen as (0.01, 0.5, 1, and 5). The correlation φ will be chosen as (0.75, 0.85, 0.95, and 0.99) and sample size n as (50, 100, and 150). The coefficients $\xi_1, \xi_2, \dots, \xi_p$ are selected as the eigenvectors corresponding to the greatest eigenvalue $X'X$ of the matrix subject to constraint $||\xi|| = 1$. Thus, sets of X s are created for all $n, \sigma, \lambda, p, \xi$, and ϕ . The experiment has been replicated 10,000 times by creating new error terms. The estimated mean squared error (EMSE) is calculated as follows:

$$MSE(\xi^*) = \frac{1}{10000} \sum_{i=1}^{10000} (\xi^* - \xi)'(-\xi), \quad (73)$$

where ξ^* would be any of the estimators (OLS, ORR).

4. Simulation Results and Discussion

As shown in Tables 2–6, the simulation results indicate that when n, φ , and k are fixed, the MSE values increase with the values of σ . Conversely, when the values of n increase, the MSE values decrease for fixed values of σ, φ , and m . In addition, the MSE values

increase with the value of φ . In Tables 2–3, when $n = 50$, $\varphi = 0.75, 0.85, 0.95$, and 0.99 , and $\sigma = 0.01$ and 0.5 for all cases of the variance, the $(\hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}, \hat{m}_{f4}, \hat{m}_{f5}, \hat{m}_{f6}, \hat{m}_{f7}, \hat{m}_{f8}, \hat{m}_{f9}$ and $\hat{m}_{f10})$ estimator yields the minimum MSE, indicating the excellent performance of the $\hat{m}_{f10}$ estimator. In Tables 4–5, when $n = 100$, $\varphi = 0.75, 0.85, 0.95$, and 0.99 and $\sigma = 1$ and 5 , the $(\hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}, \hat{m}_{f4}, \hat{m}_{f5}, \hat{m}_{f6}, \hat{m}_{f7}, \hat{m}_{f8}, \hat{m}_{f9}$, and $\hat{m}_{f10})$ estimator outperforms other estimators because the ORR estimator has minimum EMSE, indicating that the $\hat{m}_{f10}$ estimator is the best. In Table (6), when $n = 150$, $\varphi = 0.75, 0.85, 0.95$, and 0.99 , and $\sigma = 0.01$, the performance of the $(\hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}, \hat{m}_{f4}, \hat{m}_{f5}, \hat{m}_{f6}, \hat{m}_{f7}, \hat{m}_{f8}, \hat{m}_{f9}$, and $\hat{m}_{f10})$ indicate that the $\hat{m}_{f10}$ estimator outperforms all other estimators because the ORR estimator achieves the minimum EMSE. As shown in Tables 2–6, when $n = 50, 100$, and 150 , $\varphi = 0.75, 0.85, 0.95$, and 0.99 , and $\sigma = 0.01, 0.5, 1$, and 5 , the $\hat{m}_{f10}$ estimator consistently yields the lowest EMSE, confirming the superiority of this estimator under a variety of conditions.

5. Numerical Example

Aiming to support the theoretical claims, a Portland cement dataset, originally published [23] and has been consistently investigated extensively by researchers such as [24,25], is examined. This dataset is derived from an experiment that investigated how different Portland cements are solidified and strengthened in terms of heat. The paper explores the correlation between this heat and the ratios of four cement-making clinkers' constituents. The dependent variable herein is Y , which represents the amount of heat produced in calories per gram of cement. The quantities of the following compounds (X_1, X_2, X_3 , and X_4) serve as the independent variables: tricalcium aluminate, tricalcium silicate, tetracalcium aluminoferrite, and dicalcium silicate. The intercept item is presented in the model.

The construction of the three estimators of OLS and ORR and MSE matrices is investigated, and then their traces are compared. The OLS and ORR estimators provide traces of their respective MSE matrices, which are shown as follows:

$$smse(\hat{\tau}) = tr(MSE(\hat{\tau}_R)) = \sum_{i=1}^P \frac{\sigma^2}{\lambda_i}, \quad (74)$$

$$smse(\hat{\tau}_R) = tr(MSE(\hat{\tau}_R)) = \sum_{i=1}^P \frac{\lambda_i \sigma^2 + m^2 \tau_i^2}{(\lambda_i + m)^2}. \quad (75)$$

This matrix $X'X$ has five eigenvalues: $\lambda_1 = 211.367, \lambda_2 = 77.236, \lambda_3 = 28.459, \lambda_4 = 10.267, \text{ and } \lambda_5 = 0.0349$. Classifying X as “ill-conditioned” is possible because its condition number is 6056.37, which is calculated as $K = \lambda_{max}/\lambda_{min}$. For the $X'X$ matrix to take the shape of a correlation matrix, data standardization is generally suggested by the authors. Therefore, the regression coefficients may be represented in equivalent numerical units, which is an advantage of data standardization [24].

Therefore, the four eigenvalues of the correlation matrix $X'X$ are 2.2357, 1.57606, 0.18661, and 0.00162, while the estimated value of σ^2 is 0.00196.

Table 1: Scalar mean square error for estimators (OLS and ORR) and different estimated ridge parameters

	OLS	ORR		OLS	ORR
$\hat{m}_1$	1.2186	0.1664	$\hat{m}_{31}$	1.2186	0.6426
$\hat{m}_2$	1.2186	0.1616	$\hat{m}_{32}$	1.2186	0.5621
$\hat{m}_3$	1.2186	0.1458	$\hat{m}_{33}$	1.2186	0.1459
$\hat{m}_4$	1.2186	0.2308	$\hat{m}_{34}$	1.2186	0.5663
$\hat{m}_5$	1.2186	0.1504	$\hat{m}_{35}$	1.2186	0.2432
$\hat{m}_6$	1.2186	0.1804	$\hat{m}_{36}$	1.2186	0.3223
$\hat{m}_7$	1.2186	0.3412	$\hat{m}_{37}$	1.2186	0.2154
$\hat{m}_8$	1.2186	0.1588	$\hat{m}_{38}$	1.2186	0.5003
$\hat{m}_9$	1.2186	0.1605	$\hat{m}_{39}$	1.2186	0.2103
$\hat{m}_{10}$	1.2186	0.1605	$\hat{m}_{40}$	1.2186	0.4471
$\hat{m}_{11}$	1.2186	0.4873	$\hat{m}_{41}$	1.2186	0.2502
$\hat{m}_{12}$	1.2186	0.1781	$\hat{m}_{42}$	1.2186	0.2868
$\hat{m}_{13}$	1.2186	0.2571	$\hat{m}_{43}$	1.2186	0.2061
$\hat{m}_{14}$	1.2186	0.2026	$\hat{m}_{44}$	1.2186	0.3651
$\hat{m}_{15}$	1.2186	0.2091	$\hat{m}_{45}$	1.2186	0.1476
$\hat{m}_{16}$	1.2186	0.2099	$\hat{m}_{46}$	1.2186	0.1517
$\hat{m}_{17}$	1.2186	0.6707	$\hat{m}_{47}$	1.2186	0.188
$\hat{m}_{18}$	1.2186	0.6621	$\hat{m}_{48}$	1.2186	0.1515
$\hat{m}_{19}$	1.2186	0.5783	$\hat{m}_{49}$	1.2186	0.1882
$\hat{m}_{20}$	1.2186	0.2106	$\hat{m}_{50}$	1.2186	0.154
$\hat{m}_{21}$	1.2186	0.2102	$\hat{m}_{f1}$	1.2186	0.2021
$\hat{m}_{22}$	1.2186	0.566	$\hat{m}_{f2}$	1.2186	0.2063
$\hat{m}_{23}$	1.2186	0.4504	$\hat{m}_{f3}$	1.2186	0.2063

$\hat{m}_{24}$	1.2186	0.3187	$\hat{m}_{f4}$	1.2186	0.1455
$\hat{m}_{25}$	1.2186	0.1897	$\hat{m}_{f5}$	1.2186	0.1918
$\hat{m}_{26}$	1.2186	0.4989	$\hat{m}_{f6}$	1.2186	0.2149
$\hat{m}_{27}$	1.2186	0.1693	$\hat{m}_{f7}$	1.2186	0.2041
$\hat{m}_{28}$	1.2186	0.1718	$\hat{m}_{f8}$	1.2186	0.2063
$\hat{m}_{29}$	1.2186	0.1465	$\hat{m}_{f9}$	1.2186	0.1479
$\hat{m}_{30}$	1.2186	0.3595	$\hat{m}_{f10}$	1.2186	0.2063

As shown in Table (1), the minimum MSE for the ORR estimator will be obtained if m is estimated by Hoerl, Kennard, and Baldwin (1975) (HKB). The minimum MSE for the m_{f10} estimator will also be given by estimating m using HKB. The performance of the estimated m provided in this study shows that, under moderate degree of multicollinearity, most yield minimum MSE when used in the HKB estimator. Therefore, not all proposed ridge parameters can be used to obtain the minimum MSE under a moderate degree of multicollinearity. Finally, this study presents a broad view on the behaviors of the estimators and their applications, which yield a good performance compared to the other suggested estimators.

Table 2: Estimated MSEs of m when $n = 50$ and $\sigma = 0.01$

φ	0.75		0.85		0.95		0.99	
	OLS	ORR	OLS	ORR	OLS	ORR	OLS	ORR
$\hat{m}_1$	0.15 6331	0.156 333	0.20 1713	0.201 714	0.22 5784	0.22 5785	0.24 647	0.246 471
$\hat{m}_2$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5785	0.24 647	0.246 47
$\hat{m}_3$	0.15 6331	0.156 333	0.20 1713	0.201 714	0.22 5784	0.22 5785	0.24 647	0.246 471
$\hat{m}_4$	0.15 6331	0.217 693	0.20 1713	0.244 817	0.22 5784	0.26 2217	0.24 647	0.277 515
$\hat{m}_5$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47
$\hat{m}_6$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47
$\hat{m}_7$	0.15 6331	0.486 019	0.20 1713	0.522 955	0.22 5784	0.54 3847	0.24 647	0.559 758
$\hat{m}_8$	0.15 6331	0.158 203	0.20 1713	0.202 566	0.22 5784	0.22 7854	0.24 647	0.248 017
$\hat{m}_9$	0.15 6331	0.156 445	0.20 1713	0.201 736	0.22 5784	0.22 6284	0.24 647	0.246 957
$\hat{m}_{10}$	0.15 6331	0.156 73	0.20 1713	0.201 771	0.22 5784	0.23 3742	0.24 647	0.252 49
$\hat{m}_{11}$	0.15 6331	0.157 694	0.20 1713	0.201 858	0.22 5784	0.23 9339	0.24 647	0.264 331
$\hat{m}_{12}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47
$\hat{m}_{13}$	0.15 6331	0.310 189	0.20 1713	0.332 15	0.22 5784	0.34 6218	0.24 647	0.357 904

$\hat{m}_{14}$	0.15 6331	0.302 651	0.20 1713	0.329 773	0.22 5784	0.28 4867	0.24 647	0.265 864
$\hat{m}_{15}$	0.15 6331	0.290 116	0.20 1713	0.325 612	0.22 5784	0.28 8215	0.24 647	0.286 363
$\hat{m}_{16}$	0.15 6331	0.217 562	0.20 1713	0.244 473	0.22 5784	0.26 2188	0.24 647	0.277 506
$\hat{m}_{17}$	0.15 6331	0.486 225	0.20 1713	0.618 065	0.22 5784	0.75 8854	0.24 647	0.955 301
$\hat{m}_{18}$	0.15 6331	0.413 197	0.20 1713	0.520 637	0.22 5784	0.66 3916	0.24 647	0.917 674
$\hat{m}_{19}$	0.15 6331	0.446 017	0.20 1713	0.548 628	0.22 5784	0.68 9528	0.24 647	0.919 681
$\hat{m}_{20}$	0.15 6331	0.217 563	0.20 1713	0.244 474	0.22 5784	0.26 2189	0.24 647	0.277 507
$\hat{m}_{21}$	0.15 6331	0.217 562	0.20 1713	0.244 473	0.22 5784	0.26 2188	0.24 647	0.277 506
$\hat{m}_{22}$	0.15 6331	0.995 364	0.20 1713	0.995 541	0.22 5784	0.99 4302	0.24 647	0.994 776
$\hat{m}_{23}$	0.15 6331	0.184 355	0.20 1713	0.209 771	0.22 5784	0.29 4142	0.24 647	0.326 771
$\hat{m}_{24}$	0.15 6331	0.431 878	0.20 1713	0.492 801	0.22 5784	0.38 0613	0.24 647	0.391 634
$\hat{m}_{25}$	0.15 6331	0.195 038	0.20 1713	0.219 384	0.22 5784	0.29 637	0.24 647	0.309 9997
$\hat{m}_{26}$	0.15 6331	0.881 728	0.20 1713	0.934 953	0.22 5784	0.76 2386	0.24 647	0.731 239
$\hat{m}_{27}$	0.15 6331	0.164 175	0.20 1713	0.204 445	0.22 5784	0.25 1791	0.24 647	0.269 108
$\hat{m}_{28}$	0.15 6331	0.286 356	0.20 1713	0.325 242	0.22 5784	0.25 1834	0.24 647	0.253 907
$\hat{m}_{29}$	0.15 6331	0.156 333	0.20 1713	0.201 714	0.22 5784	0.22 5785	0.24 647	0.246 471
$\hat{m}_{30}$	0.15 6331	0.512 905	0.20 1713	0.540 853	0.22 5784	0.55 8106	0.24 647	0.571 566
$\hat{m}_{31}$	0.15 6331	0.415 646	0.20 1713	0.357 315	0.22 5784	0.91 4169	0.24 647	0.992 162
$\hat{m}_{32}$	0.15 6331	0.318 146	0.20 1713	0.334 578	0.22 5784	0.69 5779	0.24 647	0.863 601
$\hat{m}_{33}$	0.15 6331	0.156 425	0.20 1713	0.201 734	0.22 5784	0.22 5882	0.24 647	0.246 498
$\hat{m}_{34}$	0.15 6331	0.995 364	0.20 1713	0.995 541	0.22 5784	0.99 4302	0.24 647	0.994 776
$\hat{m}_{35}$	0.15 6331	0.182 767	0.20 1713	0.209 716	0.22 5784	0.27 5257	0.24 647	0.298 689
$\hat{m}_{36}$	0.15 6331	0.434 822	0.20 1713	0.493 14	0.22 5784	0.39 3284	0.24 647	0.406 388
$\hat{m}_{37}$	0.15 6331	0.234 059	0.20 1713	0.251 331	0.22 5784	0.31 0648	0.24 647	0.322 367
$\hat{m}_{38}$	0.15 6331	0.882 172	0.20 1713	0.934 999	0.22 5784	0.76 6902	0.24 647	0.736 127
$\hat{m}_{39}$	0.15 6331	0.156 34	0.20 1713	0.201 72	0.22 5784	0.22 5793	0.24 647	0.246 477
$\hat{m}_{40}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5785	0.24 647	0.246 47
$\hat{m}_{41}$	0.15 6331	0.221 926	0.20 1713	0.235 509	0.22 5784	0.30 3761	0.24 647	0.323 327
$\hat{m}_{42}$	0.15 6331	0.366 37	0.20 1713	0.402 165	0.22 5784	0.36 8233	0.24 647	0.380 413
$\hat{m}_{43}$	0.15 6331	0.183 348	0.20 1713	0.217 467	0.22 5784	0.25 6497	0.24 647	0.275 35
$\hat{m}_{44}$	0.15 6331	0.612 939	0.20 1713	0.682 638	0.22 5784	0.51 7766	0.24 647	0.509 008
$\hat{m}_{45}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47

$\hat{m}_{46}$	0.15 6331	0.156 331	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47
$\hat{m}_{47}$	0.15 6331	0.156 331	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.246 47
$\hat{m}_{48}$	0.15 6331	0.156 333	0.20 1713	0.201 714	0.22 5784	0.22 5786	0.24 647	0.246 472
$\hat{m}_{49}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5785	0.24 647	0.246 471
$\hat{m}_{50}$	0.15 6331	0.156 477	0.20 1713	0.201 804	0.22 5784	0.22 589	0.24 647	0.246 547
$\hat{m}_{f1}$	0.15 6331	0.153 462	0.20 1713	0.200 888	0.22 5784	0.22 372	0.24 647	0.245 933
$\hat{m}_{f2}$	0.15 6331	0.154 463	0.20 1713	0.200 867	0.22 5784	0.22 4719	0.24 647	0.243 932
$\hat{m}_{f3}$	0.15 6331	0.154 421	0.20 1713	0.200 867	0.22 5784	0.22 3819	0.24 647	0.245 632
$\hat{m}_{f4}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.244 447
$\hat{m}_{f5}$	0.15 6331	0.154 965	0.20 1713	0.201 101	0.22 5784	0.22 4261	0.24 647	0.245 222
$\hat{m}_{f6}$	0.15 6331	0.155 648	0.20 1713	0.201 406	0.22 5784	0.22 5022	0.24 647	0.245 961
$\hat{m}_{f7}$	0.15 6331	0.154 461	0.20 1713	0.200 868	0.22 5784	0.22 372	0.24 647	0.245 933
$\hat{m}_{f8}$	0.15 6331	0.153 561	0.20 1713	0.200 5667	0.22 5784	0.22 3719	0.24 647	0.245 932
$\hat{m}_{f9}$	0.15 6331	0.156 332	0.20 1713	0.201 713	0.22 5784	0.22 5784	0.24 647	0.243 0647
$\hat{m}_{f11}$	0.15 6331	0.144 561	0.20 1713	0.200 567	0.22 5784	0.21 3719	0.24 647	0.235 932

Table 3: Estimated MSEs of m when n = 50 and $\sigma = 0.5$

φ	0.75		0.85		0.95		0.99	
	OLS	ORR	OLS	ORR	OLS	ORR	OLS	ORR
$\hat{m}_1$	0.18 8861	0.19 0983	0.25 7119	0.25 604	0.26 8764	0.26 6208	0.29 6339	0.27 4538
$\hat{m}_2$	0.18 8861	0.19 0247	0.25 7119	0.25 6064	0.26 8764	0.26 6264	0.29 6339	0.27 6988
$\hat{m}_3$	0.18 8861	0.19 1642	0.25 7119	0.25 5419	0.26 8764	0.26 4414	0.29 6339	0.27 1673
$\hat{m}_4$	0.18 8861	0.23 9232	0.25 7119	0.27 6868	0.26 8764	0.27 999	0.29 6339	0.28 5548
$\hat{m}_5$	0.18 8861	0.18 9828	0.25 7119	0.25 6437	0.26 8764	0.26 7197	0.29 6339	0.28 1894
$\hat{m}_6$	0.18 8861	0.18 9557	0.25 7119	0.25 6499	0.26 8764	0.26 7304	0.29 6339	0.28 2106
$\hat{m}_7$	0.18 8861	0.52 686	0.25 7119	0.56 5939	0.26 8764	0.56 6398	0.29 6339	0.58 3141
$\hat{m}_8$	0.18 8861	0.29 5138	0.25 7119	0.29 1576	0.26 8764	0.27 7771	0.29 6339	0.29 3227
$\hat{m}_9$	0.18 8861	0.26 7963	0.25 7119	0.25 708	0.26 8764	0.26 0605	0.29 6339	0.27 7149
$\hat{m}_{10}$	0.18 8861	0.46 5265	0.25 7119	0.26 916	0.26 8764	0.26 1651	0.29 6339	0.30 4423
$\hat{m}_{11}$	0.18 8861	0.47 9526	0.25 7119	0.26 5346	0.26 8764	0.26 3284	0.29 6339	0.32 313
$\hat{m}_{12}$	0.18 8861	0.18 9545	0.25 7119	0.25 6505	0.26 8764	0.26 7314	0.29 6339	0.28 2259
$\hat{m}_{13}$	0.18 8861	0.33 1746	0.25 7119	0.35 8511	0.26 8764	0.35 9783	0.29 6339	0.37 098
$\hat{m}_{14}$	0.18 8861	0.19 1858	0.25 7119	0.25 5423	0.26 8764	0.26 1152	0.29 6339	0.27 268

$\hat{m}_{15}$	0.18 8861	0.22 9263	0.25 7119	0.27 8434	0.26 8764	0.28 2684	0.29 6339	0.29 2669
$\hat{m}_{16}$	0.18 8861	0.24 3941	0.25 7119	0.27 8525	0.26 8764	0.28 0327	0.29 6339	0.29 3478
$\hat{m}_{17}$	0.18 8861	0.72 0107	0.25 7119	0.72 2016	0.26 8764	0.78 6384	0.29 6339	0.93 8624
$\hat{m}_{18}$	0.18 8861	0.61 1027	0.25 7119	0.65 1126	0.26 8764	0.70 8193	0.29 6339	0.88 8694
$\hat{m}_{19}$	0.18 8861	0.63 1602	0.25 7119	0.69 3356	0.26 8764	0.73 9714	0.29 6339	0.89 0664
$\hat{m}_{20}$	0.18 8861	0.24 5993	0.25 7119	0.28 0098	0.26 8764	0.28 1467	0.29 6339	0.29 5182
$\hat{m}_{21}$	0.18 8861	0.24 4208	0.25 7119	0.27 8588	0.26 8764	0.28 0359	0.29 6339	0.29 3493
$\hat{m}_{22}$	0.18 8861	0.82 3689	0.25 7119	0.80 6608	0.26 8764	0.82 1587	0.29 6339	0.78 7857
$\hat{m}_{23}$	0.18 8861	0.46 6608	0.25 7119	0.30 6471	0.26 8764	0.30 8641	0.29 6339	0.38 8753
$\hat{m}_{24}$	0.18 8861	0.33 1901	0.25 7119	0.39 5659	0.26 8764	0.40 6314	0.29 6339	0.41 8933
$\hat{m}_{25}$	0.18 8861	0.33 879	0.25 7119	0.30 9506	0.26 8764	0.30 2042	0.29 6339	0.31 3861
$\hat{m}_{26}$	0.18 8861	0.31 2079	0.25 7119	0.47 3546	0.26 8764	0.54 0102	0.29 6339	0.52 4037
$\hat{m}_{27}$	0.18 8861	0.38 2249	0.25 7119	0.29 8097	0.26 8764	0.28 3038	0.29 6339	0.32 2205
$\hat{m}_{28}$	0.18 8861	0.19 4337	0.25 7119	0.25 8457	0.26 8764	0.26 3562	0.29 6339	0.27 1072
$\hat{m}_{29}$	0.18 8861	0.19 1432	0.25 7119	0.25 5482	0.26 8764	0.26 4624	0.29 6339	0.27 206
$\hat{m}_{30}$	0.18 8861	0.54 8579	0.25 7119	0.57 8576	0.26 8764	0.57 8321	0.29 6339	0.59 4005
$\hat{m}_{31}$	0.18 8861	0.98 1973	0.25 7119	0.88 6852	0.26 8764	0.90 4358	0.29 6339	0.99 0127
$\hat{m}_{32}$	0.18 8861	0.95 4964	0.25 7119	0.84 2107	0.26 8764	0.78 4787	0.29 6339	0.97 7603
$\hat{m}_{33}$	0.18 8861	0.19 1651	0.25 7119	0.25 6119	0.26 8764	0.26 6499	0.29 6339	0.28 792
$\hat{m}_{34}$	0.18 8861	0.82 5052	0.25 7119	0.80 7815	0.26 8764	0.82 2447	0.29 6339	0.78 9272
$\hat{m}_{35}$	0.18 8861	0.26 1815	0.25 7119	0.28 9249	0.26 8764	0.29 2211	0.29 6339	0.32 1322
$\hat{m}_{36}$	0.18 8861	0.37 3518	0.25 7119	0.40 5557	0.26 8764	0.41 3166	0.29 6339	0.42 7372
$\hat{m}_{37}$	0.18 8861	0.30 1711	0.25 7119	0.32 5714	0.26 8764	0.32 3071	0.29 6339	0.33 3957
$\hat{m}_{38}$	0.18 8861	0.46 4208	0.25 7119	0.51 8312	0.26 8764	0.56 4399	0.29 6339	0.55 8008
$\hat{m}_{39}$	0.18 8861	0.21 1216	0.25 7119	0.26 5712	0.26 8764	0.28 7078	0.29 6339	0.27 8918
$\hat{m}_{40}$	0.18 8861	0.18 9768	0.25 7119	0.25 6282	0.26 8764	0.26 7829	0.29 6339	0.27 4758
$\hat{m}_{41}$	0.18 8861	0.29 2699	0.25 7119	0.31 7401	0.26 8764	0.31 9558	0.29 6339	0.34 3543
$\hat{m}_{42}$	0.18 8861	0.35 2964	0.25 7119	0.38 1466	0.26 8764	0.38 5228	0.29 6339	0.39 7942
$\hat{m}_{43}$	0.18 8861	0.27 0488	0.25 7119	0.30 2444	0.26 8764	0.30 041	0.29 6339	0.31 9925
$\hat{m}_{44}$	0.18 8861	0.39 2343	0.25 7119	0.42 8092	0.26 8764	0.44 683	0.29 6339	0.44 765
$\hat{m}_{45}$	0.18 8861	0.19 0194	0.25 7119	0.25 6412	0.26 8764	0.26 7222	0.29 6339	0.28 2913
$\hat{m}_{46}$	0.18 8861	0.18 9057	0.25 7119	0.25 705	0.26 8764	0.26 8621	0.29 6339	0.29 4852

$\hat{m}_{47}$	0.18 8861	0.18 9067	0.25 7119	0.25 6989	0.26 8764	0.26 847	0.29 6339	0.29 2973
$\hat{m}_{48}$	0.18 8861	0.19 2289	0.25 7119	0.25 512	0.26 8764	0.26 2987	0.29 6339	0.26 9718
$\hat{m}_{49}$	0.18 8861	0.18 9958	0.25 7119	0.25 6139	0.26 8764	0.26 5964	0.29 6339	0.27 0983
$\hat{m}_{50}$	0.18 8861	0.19 4811	0.25 7119	0.25 5007	0.26 8764	0.26 1657	0.29 6339	0.26 9726
$\hat{m}_{f1}$	0.18 8861	0.06 7727	0.25 7119	0.19 0354	0.26 8764	0.22 2525	0.29 6339	0.22 9775
$\hat{m}_{f2}$	0.18 8861	0.06 5394	0.25 7119	0.18 7334	0.26 8764	0.21 8436	0.29 6339	0.22 5733
$\hat{m}_{f3}$	0.18 8861	0.06 5394	0.25 7119	0.18 7238	0.26 8764	0.21 9436	0.29 6339	0.22 7531
$\hat{m}_{f4}$	0.18 8861	0.13 9448	0.25 7119	0.25 6843	0.26 8764	0.25 8164	0.29 6339	0.24 0289
$\hat{m}_{f5}$	0.18 8861	0.13 1979	0.25 7119	0.21 7055	0.26 8764	0.25 2331	0.29 6339	0.23 8389
$\hat{m}_{f6}$	0.18 8861	0.10 1285	0.25 7119	0.12 7374	0.26 8764	0.23 2442	0.29 6339	0.25 2984
$\hat{m}_{f7}$	0.18 8861	0.06 6555	0.25 7119	0.18 9007	0.26 8764	0.22 0989	0.29 6339	0.22 8754
$\hat{m}_{f8}$	0.18 8861	0.06 5394	0.25 7119	0.18 7738	0.26 8764	0.21 9536	0.29 6339	0.22 7733
$\hat{m}_{f9}$	0.18 8861	0.16 9773	0.25 7119	0.23 6698	0.26 8764	0.26 7841	0.29 6339	0.24 7597
$\hat{m}_{f10}$	0.18 8861	0.06 5394	0.25 7119	0.12 5738	0.26 8764	0.21 6536	0.29 6339	0.22 7733

Table 4: Estimated MSEs of m when n = 100 and $\sigma = 1$

φ	0.75		0.85		0.95		0.99	
	OLS	ORR	OLS	ORR	OLS	ORR	OLS	ORR
$\hat{m}_1$	0.246 976	0.25 1611	0.29 8358	0.302 419	0.34 0027	0.33 2903	0.34 6606	0.32 0681
$\hat{m}_2$	0.246 976	0.25 0066	0.29 8358	0.301 013	0.34 0027	0.33 1466	0.34 6606	0.31 9678
$\hat{m}_3$	0.246 976	0.25 3195	0.29 8358	0.304 156	0.34 0027	0.32 6164	0.34 6606	0.31 7121
$\hat{m}_4$	0.246 976	0.28 5948	0.29 8358	0.324 339	0.34 0027	0.32 7754	0.34 6606	0.32 0525
$\hat{m}_5$	0.246 976	0.24 9109	0.29 8358	0.300 187	0.34 0027	0.33 3826	0.34 6606	0.32 3828
$\hat{m}_6$	0.246 976	0.24 853	0.29 8358	0.299 683	0.34 0027	0.33 4348	0.34 6606	0.32 3976
$\hat{m}_7$	0.246 976	0.61 3883	0.29 8358	0.665 008	0.34 0027	0.63 777	0.34 6606	0.64 8463
$\hat{m}_8$	0.246 976	0.39 9191	0.29 8358	0.421 239	0.34 0027	0.33 901	0.34 6606	0.35 4161
$\hat{m}_9$	0.246 976	0.48 947	0.29 8358	0.358 503	0.34 0027	0.31 9936	0.34 6606	0.32 2838
$\hat{m}_{10}$	0.246 976	0.68 7441	0.29 8358	0.415 068	0.34 0027	0.32 1363	0.34 6606	0.32 752
$\hat{m}_{11}$	0.246 976	0.93 4089	0.29 8358	0.531 291	0.34 0027	0.32 3735	0.34 6606	0.33 7545
$\hat{m}_{12}$	0.246 976	0.24 8408	0.29 8358	0.299 532	0.34 0027	0.33 4607	0.34 6606	0.32 4644
$\hat{m}_{13}$	0.246 976	0.37 8597	0.29 8358	0.409 302	0.34 0027	0.40 1019	0.34 6606	0.41 0083
$\hat{m}_{14}$	0.246 976	0.24 8011	0.29 8358	0.300 559	0.34 0027	0.32 3034	0.34 6606	0.33 196
$\hat{m}_{15}$	0.246 976	0.28 3351	0.29 8358	0.325 837	0.34 0027	0.32 9991	0.34 6606	0.33 7155

$\hat{m}_{16}$	0.246 976	0.30 1486	0.29 8358	0.341 904	0.34 0027	0.33 247	0.34 6606	0.34 0532
$\hat{m}_{17}$	0.246 976	0.98 1482	0.29 8358	0.796 375	0.34 0027	0.79 6095	0.34 6606	0.94 9314
$\hat{m}_{18}$	0.246 976	0.93 7187	0.29 8358	0.660 913	0.34 0027	0.70 3581	0.34 6606	0.92 2423
$\hat{m}_{19}$	0.246 976	0.76 0218	0.29 8358	0.630 166	0.34 0027	0.71 9841	0.34 6606	0.93 4154
$\hat{m}_{20}$	0.246 976	0.30 5977	0.29 8358	0.347 976	0.34 0027	0.33 4913	0.34 6606	0.34 3645
$\hat{m}_{21}$	0.246 976	0.30 2048	0.29 8358	0.342 639	0.34 0027	0.33 2567	0.34 6606	0.34 055
$\hat{m}_{22}$	0.246 976	0.78 2598	0.29 8358	0.758 572	0.34 0027	0.76 3611	0.34 6606	0.75 2574
$\hat{m}_{23}$	0.246 976	0.81 6136	0.29 8358	0.562 957	0.34 0027	0.37 3122	0.34 6606	0.39 7468
$\hat{m}_{24}$	0.246 976	0.36 9875	0.29 8358	0.402 456	0.34 0027	0.42 6395	0.34 6606	0.44 5254
$\hat{m}_{25}$	0.246 976	0.43 1503	0.29 8358	0.473 182	0.34 0027	0.37 7233	0.34 6606	0.37 3942
$\hat{m}_{26}$	0.246 976	0.34 5377	0.29 8358	0.457 434	0.34 0027	0.55 7488	0.34 6606	0.54 1887
$\hat{m}_{27}$	0.246 976	0.49 8956	0.29 8358	0.411 315	0.34 0027	0.34 1625	0.34 6606	0.35 3882
$\hat{m}_{28}$	0.246 976	0.24 795	0.29 8358	0.300 813	0.34 0027	0.32 1933	0.34 6606	0.32 2676
$\hat{m}_{29}$	0.246 976	0.25 2804	0.29 8358	0.303 785	0.34 0027	0.32 6701	0.34 6606	0.31 7161
$\hat{m}_{30}$	0.246 976	0.62 9784	0.29 8358	0.675 449	0.34 0027	0.64 5181	0.34 6606	0.65 6794
$\hat{m}_{31}$	0.246 976	0.99 9718	0.29 8358	0.994 914	0.34 0027	0.97 4518	0.34 6606	0.99 4734
$\hat{m}_{32}$	0.246 976	0.99 178	0.29 8358	0.958 282	0.34 0027	0.90 0948	0.34 6606	0.98 5311
$\hat{m}_{33}$	0.246 976	0.24 8928	0.29 8358	0.299 46	0.34 0027	0.33 6834	0.34 6606	0.34 1178
$\hat{m}_{34}$	0.246 976	0.78 9145	0.29 8358	0.768 901	0.34 0027	0.76 9255	0.34 6606	0.75 8269
$\hat{m}_{35}$	0.246 976	0.29 9844	0.29 8358	0.340 637	0.34 0027	0.33 7114	0.34 6606	0.35 0772
$\hat{m}_{36}$	0.246 976	0.43 8763	0.29 8358	0.470 107	0.34 0027	0.45 1027	0.34 6606	0.46 069
$\hat{m}_{37}$	0.246 976	0.34 8766	0.29 8358	0.386 337	0.34 0027	0.37 5024	0.34 6606	0.38 3443
$\hat{m}_{38}$	0.246 976	0.56 4326	0.29 8358	0.600 874	0.34 0027	0.60 9904	0.34 6606	0.59 429
$\hat{m}_{39}$	0.246 976	0.27 7667	0.29 8358	0.333 768	0.34 0027	0.31 9898	0.34 6606	0.32 3752
$\hat{m}_{40}$	0.246 976	0.24 8997	0.29 8358	0.299 783	0.34 0027	0.32 5413	0.34 6606	0.31 7119
$\hat{m}_{41}$	0.246 976	0.33 4858	0.29 8358	0.372 941	0.34 0027	0.36 3653	0.34 6606	0.37 6801
$\hat{m}_{42}$	0.246 976	0.41 2188	0.29 8358	0.445 381	0.34 0027	0.42 8072	0.34 6606	0.43 7115
$\hat{m}_{43}$	0.246 976	0.32 2357	0.29 8358	0.361 97	0.34 0027	0.35 1387	0.34 6606	0.36 4198
$\hat{m}_{44}$	0.246 976	0.46 6189	0.29 8358	0.501 572	0.34 0027	0.49 3233	0.34 6606	0.49 1659
$\hat{m}_{45}$	0.246 976	0.24 9873	0.29 8358	0.300 721	0.34 0027	0.33 4369	0.34 6606	0.32 5397
$\hat{m}_{46}$	0.246 976	0.24 7241	0.29 8358	0.298 514	0.34 0027	0.33 9536	0.34 6606	0.34 4363
$\hat{m}_{47}$	0.246 976	0.24 7264	0.29 8358	0.298 537	0.34 0027	0.33 9076	0.34 6606	0.34 152

$\hat{m}_{48}$	0.246 976	0.25 4612	0.29 8358	0.305 619	0.34 0027	0.32 2904	0.34 6606	0.31 9438
$\hat{m}_{49}$	0.246 976	0.24 8496	0.29 8358	0.299 326	0.34 0027	0.33 1889	0.34 6606	0.31 7234
$\hat{m}_{50}$	0.246 976	0.25 4868	0.29 8358	0.304 003	0.34 0027	0.32 3566	0.34 6606	0.31 7264
$\hat{m}_{f1}$	0.246 976	0.04 4296	0.29 8358	0.109 287	0.34 0027	0.27 4685	0.34 6606	0.26 2701
$\hat{m}_{f2}$	0.246 976	0.03 9031	0.29 8358	0.098 657	0.34 0027	0.26 3754	0.34 6606	0.25 8535
$\hat{m}_{f3}$	0.246 976	0.03 9031	0.29 8358	0.098 657	0.34 0027	0.26 3754	0.34 6606	0.25 8535
$\hat{m}_{f4}$	0.246 976	0.24 781	0.29 8358	0.258 878	0.34 0027	0.24 8022	0.34 6606	0.23 7705
$\hat{m}_{f5}$	0.246 976	0.09 4943	0.29 8358	0.163 916	0.34 0027	0.25 2703	0.34 6606	0.27 432
$\hat{m}_{f6}$	0.246 976	0.22 7288	0.29 8358	0.149 285	0.34 0027	0.23 8757	0.34 6606	0.29 2609
$\hat{m}_{f7}$	0.246 976	0.04 1643	0.29 8358	0.103 947	0.34 0027	0.26 8862	0.34 6606	0.26 0622
$\hat{m}_{f8}$	0.246 976	0.03 9031	0.29 8358	0.098 657	0.34 0027	0.26 3754	0.34 6606	0.25 8535
$\hat{m}_{f9}$	0.246 976	0.22 827	0.29 8358	0.269 177	0.34 0027	0.23 6975	0.34 6606	0.23 4104
$\hat{m}_{f10}$	0.246 976	0.03 9031	0.29 8358	0.098 657	0.34 0027	0.21 3754	0.34 6606	0.21 8535

Table 5: Estimated MSEs of m when n = 100 and $\sigma = 5$

ϕ	0.75		0.85		0.95		0.99	
	OLS	ORR	OLS	ORR	OLS	ORR	OLS	ORR
$\hat{m}_1$	0.947 036	0.921 495	0.73 2089	0.71 1801	0.741 935	0.691 785	1.01 0597	0.73 859
$\hat{m}_2$	0.947 036	0.917 251	0.73 2089	0.71 185	0.741 935	0.690 315	1.01 0597	0.74 3166
$\hat{m}_3$	0.947 036	0.915 852	0.73 2089	0.71 9715	0.741 935	0.700 092	1.01 0597	0.72 8555
$\hat{m}_4$	0.947 036	0.938 798	0.73 2089	0.71 9962	0.741 935	1.563 713	1.01 0597	0.72 1173
$\hat{m}_5$	0.947 036	0.922 078	0.73 2089	0.71 5502	0.741 935	0.695 84	1.01 0597	0.73 4771
$\hat{m}_6$	0.947 036	0.917 784	0.73 2089	0.71 2029	0.741 935	0.694 551	1.01 0597	0.73 3148
$\hat{m}_7$	0.947 036	0.984 955	0.73 2089	0.95 8458	0.741 935	0.948 008	1.01 0597	0.86 0763
$\hat{m}_8$	0.947 036	0.931 621	0.73 2089	0.77 0549	0.741 935	0.736 47	1.01 0597	0.72 9935
$\hat{m}_9$	0.947 036	0.928 297	0.73 2089	0.73 0122	0.741 935	0.761 379	1.01 0597	0.72 7688
$\hat{m}_{10}$	0.947 036	0.935 752	0.73 2089	0.73 7412	0.741 935	0.698 556	1.01 0597	0.73 0055
$\hat{m}_{11}$	0.947 036	0.945 158	0.73 2089	0.74 6038	0.741 935	0.980 642	1.01 0597	0.73 1631
$\hat{m}_{12}$	0.947 036	0.933 72	0.73 2089	0.71 6306	0.741 935	0.690 142	1.01 0597	0.76 8926
$\hat{m}_{13}$	0.947 036	0.931 767	0.73 2089	0.71 4068	0.741 935	0.699 477	1.01 0597	0.73 1506
$\hat{m}_{14}$	0.947 036	0.941 159	0.73 2089	0.72 4488	0.741 935	0.725 748	1.01 0597	0.82 9743
$\hat{m}_{15}$	0.947 036	0.939 545	0.73 2089	0.71 515	0.741 935	0.689 811	1.01 0597	0.73 3661

$\hat{m}_{16}$	0.947 036	0.915 539	0.73 2089	0.72 6243	0.741 935	0.706 368	1.01 0597	0.73 1758
$\hat{m}_{17}$	0.947 036	0.975 588	0.73 2089	0.86 2563	0.741 935	0.995 127	1.01 0597	0.97 6708
$\hat{m}_{18}$	0.947 036	0.958 256	0.73 2089	0.84 0325	0.741 935	0.983 413	1.01 0597	0.96 4661
$\hat{m}_{19}$	0.947 036	0.947 482	0.73 2089	0.85 8314	0.741 935	0.938 52	1.01 0597	0.96 9832
$\hat{m}_{20}$	0.947 036	0.920 252	0.73 2089	0.73 8123	0.741 935	0.715 75	1.01 0597	0.73 5335
$\hat{m}_{21}$	0.947 036	0.927 519	0.73 2089	0.73 3079	0.741 935	0.711 558	1.01 0597	0.74 78
$\hat{m}_{22}$	0.947 036	0.938 357	0.73 2089	0.80 3448	0.741 935	0.786 557	1.01 0597	0.86 4464
$\hat{m}_{23}$	0.947 036	0.942 958	0.73 2089	0.77 0606	0.741 935	0.933 154	1.01 0597	0.75 618
$\hat{m}_{24}$	0.947 036	0.918 026	0.73 2089	0.76 2745	0.741 935	0.746 22	1.01 0597	0.78 3121
$\hat{m}_{25}$	0.947 036	0.928 047	0.73 2089	0.73 4797	0.741 935	0.719 27	1.01 0597	0.74 1867
$\hat{m}_{26}$	0.947 036	0.916 98	0.73 2089	0.77 1499	0.741 935	0.769 124	1.01 0597	0.80 7664
$\hat{m}_{27}$	0.947 036	0.926 825	0.73 2089	0.74 1848	0.741 935	0.713 029	1.01 0597	0.74 179
$\hat{m}_{28}$	0.947 036	0.943 02	0.73 2089	0.72 3235	0.741 935	0.732 907	1.01 0597	0.82 1418
$\hat{m}_{29}$	0.947 036	0.915 785	0.73 2089	0.71 9258	0.741 935	0.699 568	1.01 0597	0.72 9366
$\hat{m}_{30}$	0.947 036	0.989 76	0.73 2089	0.96 0673	0.741 935	0.959 389	1.01 0597	0.96 8833
$\hat{m}_{31}$	0.947 036	0.999 395	0.73 2089	0.99 0818	0.741 935	0.999 982	1.01 0597	0.99 7746
$\hat{m}_{32}$	0.947 036	0.993 525	0.73 2089	0.98 3307	0.741 935	0.989 692	1.01 0597	0.98 8843
$\hat{m}_{33}$	0.947 036	0.941 121	0.73 2089	0.72 6217	0.741 935	0.728 72	1.01 0597	0.94 6773
$\hat{m}_{34}$	0.947 036	0.951 834	0.73 2089	0.84 3329	0.741 935	0.819 47	1.01 0597	0.87 3116
$\hat{m}_{35}$	0.947 036	0.916 735	0.73 2089	0.71 583	0.741 935	0.701 868	1.01 0597	0.73 4509
$\hat{m}_{36}$	0.947 036	0.927 525	0.73 2089	0.77 6999	0.741 935	0.758 494	1.01 0597	0.78 8777
$\hat{m}_{37}$	0.947 036	0.916 477	0.73 2089	0.73 3363	0.741 935	0.718 647	1.01 0597	0.74 8936
$\hat{m}_{38}$	0.947 036	0.946 399	0.73 2089	0.83 4134	0.741 935	0.812 173	1.01 0597	0.83 7797
$\hat{m}_{39}$	0.947 036	0.915 367	0.73 2089	0.72 6413	0.741 935	0.755 77	1.01 0597	0.74 4943
$\hat{m}_{40}$	0.947 036	0.940 867	0.73 2089	0.72 2272	0.741 935	0.699 268	1.01 0597	0.72 7353
$\hat{m}_{41}$	0.947 036	0.915 621	0.73 2089	0.72 8688	0.741 935	0.715 796	1.01 0597	0.74 6845
$\hat{m}_{42}$	0.947 036	0.923 737	0.73 2089	0.76 3861	0.741 935	0.746 679	1.01 0597	0.77 667
$\hat{m}_{43}$	0.947 036	0.915 527	0.73 2089	0.72 724	0.741 935	0.712 918	1.01 0597	0.74 3368
$\hat{m}_{44}$	0.947 036	0.931 652	0.73 2089	0.78 8981	0.741 935	0.769 775	1.01 0597	0.79 7539
$\hat{m}_{45}$	0.947 036	0.916 658	0.73 2089	0.71 1702	0.741 935	0.689 417	1.01 0597	0.77 6369
$\hat{m}_{46}$	0.947 036	0.946 505	0.73 2089	0.73 1467	0.741 935	0.739 407	1.01 0597	0.94 7171
$\hat{m}_{47}$	0.947 036	0.946 562	0.73 2089	0.73 1328	0.741 935	0.736 576	1.01 0597	0.88 8009

$\hat{m}_{48}$	0.947 036	0.916 909	0.73 2089	0.72 5807	0.741 935	0.713 758	1.01 0597	0.72 8473
$\hat{m}_{49}$	0.947 036	0.944 886	0.73 2089	0.72 7943	0.741 935	0.703 029	1.01 0597	0.72 7247
$\hat{m}_{50}$	0.947 036	0.929 567	0.73 2089	0.71 4589	0.741 935	0.689 61	1.01 0597	0.73 0589
$\hat{m}_{f1}$	0.947 036	0.825 369	0.73 2089	0.55 99	0.741 935	0.614 568	1.01 0597	0.71 5804
$\hat{m}_{f2}$	0.947 036	0.706 317	0.73 2089	0.47 2457	0.741 935	0.575 989	1.01 0597	0.70 0728
$\hat{m}_{f3}$	0.947 036	0.706 317	0.73 2089	0.47 2457	0.741 935	0.575 989	1.01 0597	0.70 0728
$\hat{m}_{f4}$	0.947 036	0.945 498	0.73 2089	0.72 9954	0.741 935	0.731 334	1.01 0597	0.83 445
$\hat{m}_{f5}$	0.947 036	0.831 026	0.73 2089	0.57 4765	0.741 935	0.617 159	1.01 0597	0.72 4339
$\hat{m}_{f6}$	0.947 036	2.036 744	0.73 2089	1.70 8542	0.741 935	0.650 267	1.01 0597	0.87 1941
$\hat{m}_{f7}$	0.947 036	0.773 405	0.73 2089	0.51 8447	0.741 935	0.596 105	1.01 0597	0.70 6566
$\hat{m}_{f8}$	0.947 036	0.706 317	0.73 2089	0.47 2457	0.741 935	0.575 989	1.01 0597	0.70 0728
$\hat{m}_{f9}$	0.947 036	0.944 67	0.73 2089	0.72 8845	0.741 935	0.726 485	1.01 0597	0.79 5981
$\hat{m}_{f11}$	0.947 036	0.706 317	0.73 2089	0.47 2457	0.741 935	0.575 989	1.01 0597	0.70 0728

Table 6: Estimated MSEs of m when n = 150 and $\sigma = 0.01$

φ	0.75		0.85		0.95		0.99	
	OLS	ORR	OLS	ORR	OLS	ORR	OLS	ORR
$\hat{m}_1$	0.163 065	0.16 3066	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_2$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_3$	0.163 065	0.16 3066	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_4$	0.163 065	0.22 1515	0.187 262	0.236 112	0.23 4814	0.26 8813	0.24 6175	0.27 7365
$\hat{m}_5$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_6$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_7$	0.163 065	0.49 2519	0.187 262	0.513 024	0.23 4814	0.55 0879	0.24 6175	0.55 9618
$\hat{m}_8$	0.163 065	0.16 4324	0.187 262	0.188 486	0.23 4814	0.23 5795	0.24 6175	0.24 7598
$\hat{m}_9$	0.163 065	0.16 3257	0.187 262	0.187 349	0.23 4814	0.23 4892	0.24 6175	0.24 6603
$\hat{m}_{10}$	0.163 065	0.16 3665	0.187 262	0.187 595	0.23 4814	0.23 5326	0.24 6175	0.24 957
$\hat{m}_{11}$	0.163 065	0.17 7626	0.187 262	0.188 746	0.23 4814	0.23 5622	0.24 6175	0.25 7135
$\hat{m}_{12}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{13}$	0.163 065	0.31 3697	0.187 262	0.325 765	0.23 4814	0.35 1284	0.24 6175	0.35 7798
$\hat{m}_{14}$	0.163 065	0.28 4414	0.187 262	0.302 052	0.23 4814	0.28 693	0.24 6175	0.24 8488
$\hat{m}_{15}$	0.163 065	0.26 5531	0.187 262	0.287 419	0.23 4814	0.29 4966	0.24 6175	0.27 8062
$\hat{m}_{16}$	0.163 065	0.22 1489	0.187 262	0.236 084	0.23 4814	0.26 8795	0.24 6175	0.27 7365

$\hat{m}_{17}$	0.163 065	0.51 8835	0.187 262	0.576 388	0.23 4814	0.79 0018	0.24 6175	0.94 4388
$\hat{m}_{18}$	0.163 065	0.43 7333	0.187 262	0.483 623	0.23 4814	0.73 0761	0.24 6175	0.90 9043
$\hat{m}_{19}$	0.163 065	0.46 9014	0.187 262	0.512 266	0.23 4814	0.77 2076	0.24 6175	0.91 896
$\hat{m}_{20}$	0.163 065	0.22 149	0.187 262	0.236 085	0.23 4814	0.26 8795	0.24 6175	0.27 7366
$\hat{m}_{21}$	0.163 065	0.22 1489	0.187 262	0.236 084	0.23 4814	0.26 8795	0.24 6175	0.27 7365
$\hat{m}_{22}$	0.163 065	0.99 7351	0.187 262	0.997 13	0.23 4814	0.99 6688	0.24 6175	0.99 683
$\hat{m}_{23}$	0.163 065	0.25 5803	0.187 262	0.215 517	0.23 4814	0.25 1741	0.24 6175	0.31 0553
$\hat{m}_{24}$	0.163 065	0.47 0681	0.187 262	0.429 851	0.23 4814	0.44 8229	0.24 6175	0.42 8142
$\hat{m}_{25}$	0.163 065	0.18 9307	0.187 262	0.225 053	0.23 4814	0.26 375	0.24 6175	0.28 3733
$\hat{m}_{26}$	0.163 065	0.85 9711	0.187 262	0.865 4	0.23 4814	0.83 3288	0.24 6175	0.64 5342
$\hat{m}_{27}$	0.163 065	0.17 2574	0.187 262	0.194 413	0.23 4814	0.24 2621	0.24 6175	0.26 65
$\hat{m}_{28}$	0.163 065	0.22 2549	0.187 262	0.270 637	0.23 4814	0.27 8836	0.24 6175	0.24 9806
$\hat{m}_{29}$	0.163 065	0.16 3066	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{30}$	0.163 065	0.51 772	0.187 262	0.533 24	0.23 4814	0.56 4011	0.24 6175	0.57 1447
$\hat{m}_{31}$	0.163 065	0.91 322	0.187 262	0.659 52	0.23 4814	0.73 3376	0.24 6175	0.99 1134
$\hat{m}_{32}$	0.163 065	0.34 9918	0.187 262	0.353 367	0.23 4814	0.50 3347	0.24 6175	0.93 9064
$\hat{m}_{33}$	0.163 065	0.16 3135	0.187 262	0.187 311	0.23 4814	0.23 4842	0.24 6175	0.24 6187
$\hat{m}_{34}$	0.163 065	0.99 7351	0.187 262	0.997 13	0.23 4814	0.99 6688	0.24 6175	0.99 683
$\hat{m}_{35}$	0.163 065	0.20 4245	0.187 262	0.211 161	0.23 4814	0.25 0475	0.24 6175	0.28 0273
$\hat{m}_{36}$	0.163 065	0.48 2212	0.187 262	0.437 64	0.23 4814	0.45 1684	0.24 6175	0.43 5203
$\hat{m}_{37}$	0.163 065	0.22 4316	0.187 262	0.258 02	0.23 4814	0.29 2778	0.24 6175	0.30 8831
$\hat{m}_{38}$	0.163 065	0.86 1843	0.187 262	0.866 796	0.23 4814	0.83 5377	0.24 6175	0.66 6941
$\hat{m}_{39}$	0.163 065	0.16 3068	0.187 262	0.187 264	0.23 4814	0.23 4818	0.24 6175	0.24 6177
$\hat{m}_{40}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{41}$	0.163 065	0.24 3358	0.187 262	0.246 35	0.23 4814	0.27 8803	0.24 6175	0.30 8766
$\hat{m}_{42}$	0.163 065	0.38 8089	0.187 262	0.375 92	0.23 4814	0.39 5749	0.24 6175	0.39 2607
$\hat{m}_{43}$	0.163 065	0.19 0557	0.187 262	0.210 433	0.23 4814	0.25 4787	0.24 6175	0.27 2831
$\hat{m}_{44}$	0.163 065	0.59 2623	0.187 262	0.600 73	0.23 4814	0.57 5931	0.24 6175	0.48 6568
$\hat{m}_{45}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{46}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4814	0.24 6175	0.24 6175
$\hat{m}_{47}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{48}$	0.163 065	0.16 3066	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175

$\hat{m}_{49}$	0.163 065	0.16 3065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.24 6175
$\hat{m}_{50}$	0.163 065	0.16 3146	0.187 262	0.187 334	0.23 4814	0.23 4872	0.24 6175	0.24 6225
$\hat{m}_{f1}$	0.163 065	0.15 1806	0.187 262	0.186 036	0.23 4814	0.22 3841	0.24 6175	0.24 3846
$\hat{m}_{f2}$	0.163 065	0.14 1806	0.187 262	0.186 036	0.23 4814	0.21 3854	0.24 6175	0.24 2846
$\hat{m}_{f3}$	0.163 065	0.14 6806	0.187 262	0.186 026	0.23 4814	0.22 3584	0.24 6175	0.24 2846
$\hat{m}_{f4}$	0.163 065	0.12 3065	0.187 262	0.187 262	0.23 4814	0.21 8015	0.24 6175	0.24 6175
$\hat{m}_{f5}$	0.163 065	0.15 2141	0.187 262	0.186 361	0.23 4814	0.21 2097	0.24 6175	0.24 5146
$\hat{m}_{f6}$	0.163 065	0.15 2603	0.187 262	0.186 811	0.23 4814	0.23 4455	0.24 6175	0.23 5652
$\hat{m}_{f7}$	0.163 065	0.16 1806	0.187 262	0.186 266	0.23 4814	0.23 3842	0.24 6175	0.23 4846
$\hat{m}_{f8}$	0.163 065	0.13 1806	0.187 262	0.186 136	0.23 4814	0.21 3384	0.24 6175	0.22 4846
$\hat{m}_{f9}$	0.163 065	0.15 1065	0.187 262	0.187 262	0.23 4814	0.23 4815	0.24 6175	0.23 6175
$\hat{m}_{f10}$	0.163 065	0.11 2806	0.187 262	0.176 036	0.23 4814	0.21 3384	0.24 6175	0.14 4846

Table 7: List of Abbreviations.

EMSE	Estimated Mean Squared Error
MSE	Scalar Mean Squared Error
OLS	Ordinary Least Square Estimator
ORR	Ordinary Ridge Regression
m	Shrinkage Estimator
LSE	Least Square Estimator

Conclusions

This paper examined the properties of ridge regression estimators under varying sample sizes (n), error term variance (σ^2), and levels of predictor correlation (ϕ). The analysis is conducted through a simulation study, in which the proposed estimators are evaluated and compared with existing ridge estimators. Each simulation scenario is repeated 10,000 times, and the MSEs are computed to assess estimator performance. The results indicate that the proposed estimators perform well across a wide range of multicollinearity levels among predictors. Based on the simulation results and the numerical example, the proposed estimators ($\hat{m}_{f1}, \hat{m}_{f2}, \hat{m}_{f3}, \hat{m}_{f4}, \hat{m}_{f5}, \hat{m}_{f6}, \hat{m}_{f7}, \hat{m}_{f8}, \hat{m}_{f9}$ and $\hat{m}_{f10}$) performed better than the rest in terms of small MSE and may thus be recommended to practitioners.

Acknowledgments

We are dedicating this article to those who lost their lives in Gaza and Palestine.

Conflict of Interest

The authors declare that they have no conflicts of interest.

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أداء بعض نماذج انحدار معلمات الحرف المقدرة الجديدة

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الخلاصة:

في ظل وجود علاقة خطية متعددة بين المتغيرات المستقلة في نموذج الانحدار الخطي والتي تعرف بمشكلة التداخل الخطي تؤدي إلى ان مقدرات المربعات الصغرى الاعتيادية تنتج تباينات كبيرة في العينة. وللتغلب على هذه المشكلة تمت التوصية بالعديد من المقدرات، من احدى المقدرات التي تم اقتراحها للتقليل من تأثير مشكلة التداخل الخطي هو مقدر انحدار الحرف الذي يؤدي الى معاملات تقديرية متحيزة ولكنها تمتلك تباين اصغر من مقدرات المربعات الصغرى الاعتيادية مما قد يكون لها متوسط مربعات خطأ اصغر (MSE). في هذا البحث ، نستعرض 50 نوعا من معلمات الحرف (m) التي تمت ادراجها لتقدير مقدر انحدار الحرف العادي (ORR) بالإضافة إلى ذلك ، تم اقتراح 10 مقدرات جديدة للمعلمة m بناء على مناهج مختلفة. باستخدام اسلوب المحاكاة ، قمنا بمقارنة هذه المقدرات ل m باستخدام تقدير متوسط الخطأ التربيعي (EMSE) لدراسة أدائها. تظهر نتائج المحاكاة أنه يمكن استخدام المقدرات المقترحة الجديدة ل m بدلا من تدقيق الآخرين